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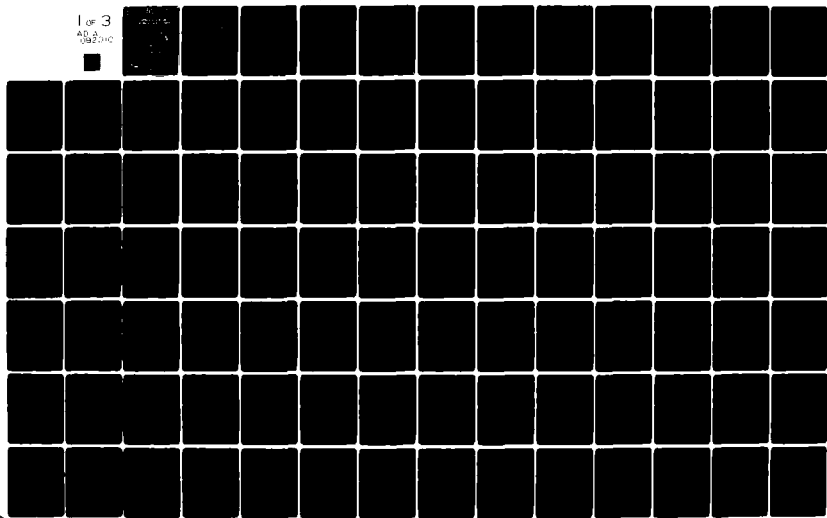
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OPTIMIZATION AT 16 KBPS**

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<p>This report describes the design of a 16 Kb/s Split-Band Adaptive Predictive Coder (SBAPC) whose high quality processed speech compares favorably with that of the Continuously Variable Slope Deltamodulator (CVSD) in both back-to-back and simulated tactical situations. Operations of this algorithm include the partitioning of the input frequency band evenly into two subbands and the encoding of the subband waveform using Adaptive Predictive Coding (APC). The results of our investigation on</p> <p>(Cont'd)</p>		

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→ quadrature mirror filters, tradeoffs between various APC parameters, noise shaping techniques, and adaptive bit allocations are presented. This report also gives a detailed discussion on the utilization of noise suppression techniques in reducing stationary background noise and forward error-correcting codes in maintaining the SBAPC performance at  $10^{-2}$  channel error rate.

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## SECTION I

### SUMMARY

#### 1.1 Summary of the Program

Under the fifteen-month Speech Algorithm Optimization at 16 Kb/s Contract (DCA 100-79-C-0038), GTE developed a FORTRAN simulation of the Split-Band Adaptive Predictive Coder (SBAPC) which yielded high quality speech outputs at 16 Kb/s. This software was designed to run on a PDP-11 computer with the FORTRAN IV-PLUS compiler.

The study has resulted in a number of significant accomplishments for developing speech processing algorithm at 16 Kb/s. Among them, the most important ones are:

- 1) the development of the high quality 16 Kb/s Split-Band APC algorithm which includes:
  - i) the design of Quadrature Mirror Filters (QMF)
  - ii) the tradeoffs between APC parameters
  - iii) comparisons of Atal and Makhoul's noise shaping techniques
  - iv) adaptive allocation of bits between the subbands
- 2) the incorporation of McAuley's noise suppression scheme in the SBAPC which yields intelligible speech even in a noisy background of -6 dB signal-to-noise ratio
- 3) the design of forward error correction codes that maintain the performance of the Split-Band APC algorithm in the presence of  $10^{-2}$  channel error rate.

This Speech Algorithm Optimization at 16 Kb/s Contract was partly motivated by the fact that high quality communications at 16 Kb/s represent one of the government's long-term goals. Moreover, the Continuously Variable Slope Deltamodulation (CVSD) scheme presently employed by the 16 Kb/s Tenley terminals does not produce quality outputs that satisfy all communication needs. The performance of these Tenley terminals, when in tandem with the STU-2's, is further compromised by the interactions of CVSD's granular and slope-overloading characteristics with the buzzy quality of the 2.4 Kb/s Linear Predictive Coder (LPC). Consequently, an improved speech encoding scheme is needed for future 16 Kb/s terminals. Studies in the past had resulted in algorithms that yielded much improved speech quality over CVSD at 16 Kb/s. An existence proof is given by the Adaptive Predictive Coder with Adaptive Quantization (APCQ) developed for DCA by GTE Sylvania under Contract No. DCA-100-76-C-0002. However, though these algorithms may yield outputs that compare favorably with CVSD in the back-to-back mode, yet the latter has been proven time after time to be one of the most robust algorithms under extremely adverse conditions. As a result, the 16 Kb/s CVSD technique still finds utility in the high noise environment of flight decks and the high error surroundings of mobile radios.

In this study, a 16 Kb/s Split-Band Adaptive Predictive Coder (SBAPC) has been investigated and our results indicate that the technique can indeed produce much improved speech quality over that of CVSD. Specifications of the 16 Kb/s SBAPC system is shown in Table 1-1. Basically, the algorithm calls for the splitting of the input frequency band using 32-tap Quadrature Mirror Filters (QMF) followed by the adaptive predictive coding (APC) of the subband waveforms. The windowing and the optimization techniques have been applied to the design of QMF's. Both procedures have

<u>PARAMETER</u>	<u>SPECIFICATION</u>
Input Bandwidth	0-3200 Hz
Sampling Rate	6400 Hz
Frame Rate	44.444/sec.
Number of Samples/Frame	144
Number of Samples Overlapped/Frame	18
Bits/Frame	360
Low Band Residual Energy	5
High Band Residual Energy	5
Low Band Pitch	6
Low Band Pitch Gain	4
Low Band PARCOR 1	5
2	5
3	3
4	3
High Band PARCOR 1	4
2	4
3	3
4	3
Residual Error Signals	216
Parity Bits (Error Correction)	90
SYNC	4
Number of Error Control Blocks/Frame	5
Error Control Technique	(63,45) BCH

TABLE 1-1: OPTIMIZED SBAPC SYSTEM SPECIFICATION



yielded QMF's that perform the bandsplitting and reconstruction with relatively little distortions. Frequency response and S/Q plots of the unquantized SBAPC system employing these filters have indicated that the QMF designed using the optimization technique is a slightly better one. For the low-band where pitch and first formant are present, our tradeoff analysis has shown that the APC with a first order pitch loop and a fourth order prediction loop is capable of preserving these perceptually important parameters. For the high-band where most unvoiced sounds, e.g., fricatives occur, a simple fourth-order prediction loop can be employed without hurting the overall quality. To account for the fluctuations of the distribution of energies between the high and low bands from frame to frame, a bit allocation scheme has been devised to dynamically alter the quantizer bit assignment. With the average assignment of 1.5 bits per sample, an improvement of 1 dB S/Q has been realized with the adaptive method. To further improve the speech quality, noise shaping algorithms have been incorporated in the SBAPC. In particular, the performance of Atal's and Makhoul's noise shaping techniques have been compared. Though the S/Q yielded by the two methods are roughly the same, Makhoul's second order all-zero shaping filter has resulted in higher quality speech.

Cognizant of the fact that CVSD yields intelligible speech under tactical situations, the performance of the SBAPC system has also been studied in the presence of background noise, channel errors and in tandem with LPC. In a low-noise office environment, the SBAPC yields high quality processed speech similar to that of the back-to-back mode. For high-noise surroundings (e.g., S/N = -6 dB), the algorithm still results in highly intelligible speech, but the noisy background makes it very annoying to listen to. To improve this, a noise reduction technique has been de-

signed which works as a pre-processor to the SBAPC system. Depending on the signal-to-noise ratio of the additive noise, a suppression factor can be pre-determined to reduce its level. The integrated SBAPC algorithm with the pre-processor has yielded highly intelligible speech without much of the annoying background noise at  $S/N = -6$  dB. Also, the SBAPC system has been found to be extremely sensitive to channel errors. Degradations in processed speech become noticeable at the bit error rate (BER) of  $5 \times 10^{-4}$  and the system yields unintelligible speech at  $10^{-2}$  BER. As expected, the side information which contains the quantized pitch, PARCOR coefficients etc. is more sensitive to channel errors than the low and high band residual signals. In fact, one or two errors occurring on the side information can result in a frame of erroneous data. Furthermore, the pitch loop in the SBAPC algorithm compounds the effect by propagating these errors over several frames. In this study, forward error correcting codes have been found to be a viable solution to maintain the system performance over a high error rate channel. Particularly, five blocks of (63,45) BCH codes have been incorporated in the 16 Kb/s SBAPC scheme, and the overall system is robust to channel error rates as high as  $10^{-2}$ . When in connection with LPC, the SBAPC algorithm has yielded more intelligible speech than the CVSD/LPC tandem.

Informal listening tests indicate that the SBAPC system yields much higher speech quality than that of CVSD in a back-to-back mode. Also, when compared to the 16 Kb/s adaptive transform coder (ATC) (a discussion is included in Appendix F), the SBAPC processed speech is slightly low-passed, but its smooth quality is much preferred over that of ATC with the noticeable "dish-washing" background noise. Furthermore, the SBAPC system has

performed well in simulated tactical situations. Based on the results obtained in this study, further work should be performed to refine the algorithm and implement it in real-time.

## SECTION II

### ALGORITHM DEVELOPMENT

#### 2.1 Introduction

The Split-Band APC technique is basically a combination of two speech coding methods, namely, the Adaptive Predictive Coding (APC) and Subband coding (SBC). The APC method is well known for its efficiency in processing speech waveforms in the time domain whereas the SBC is one of the simplest techniques in encoding speech in the frequency domain. By combining these two techniques together, the SBAPC algorithm yields high quality processed outputs without much additional complexity. In practice, the SBAPC technique calls for the partitioning of the input frequency band into two even subbands using Finite-Impulse-Response (FIR) filters followed by the application of different quantizations to the two subbands. Since the pitch and the first formant are located at the low frequency band, more detailed description of this band's waveform preserves these perceptually important parameters which can result in higher speech quality. On the other hand, the upper frequency band at which the unvoiced sounds, such as fricatives, are situated can be encoded less precisely without hurting the overall processed speech quality. Consequently, the SBAPC algorithm represents one of the most efficient methods in speech coding.

The block diagram of a Split-Band APC system is shown in Figure 2.1.1. Bandpass filters are utilized to split the input speech frequency band into two. Then each subband signal, after resampling at its Nyquist rate, is encoded using APC. At the receiver, the digital data is decoded using APC. After up-sampling, the original subband signals are created and the difference between them forms a replica of the original

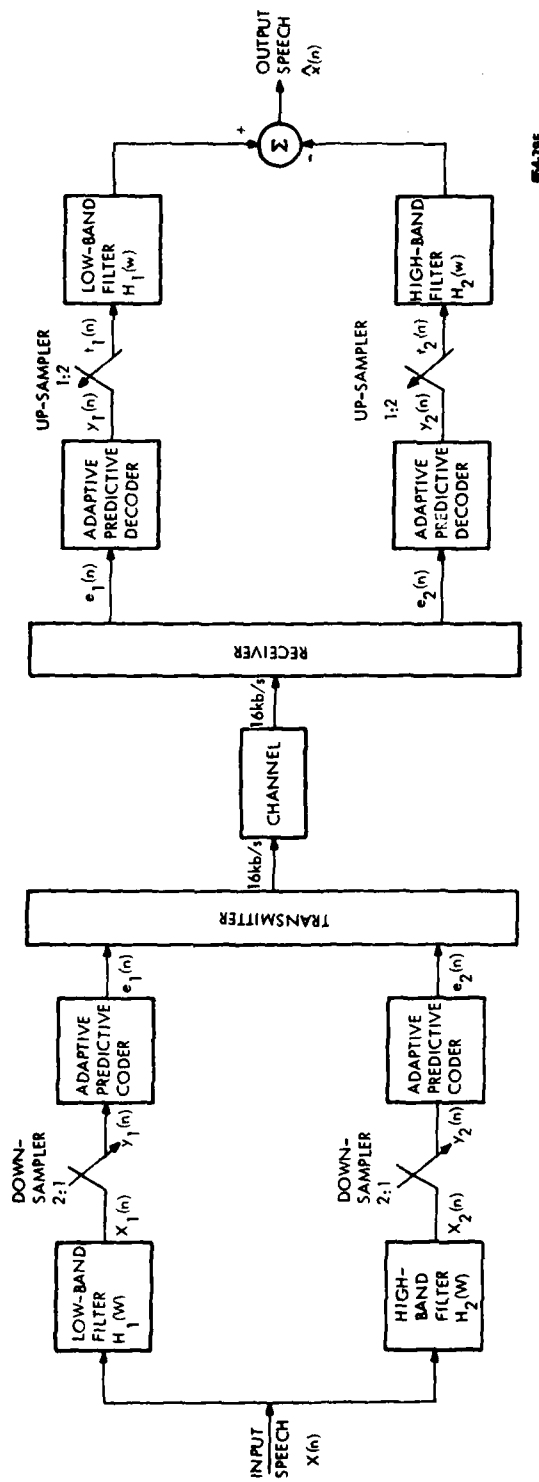


FIGURE 2.1.1: BLOCK DIAGRAM OF THE SPLIT-BAND APC TECHNIQUE

signal. The two subband signals, derived from splitting the original signal band, appear essentially as waveforms with non-flat spectral densities and contain a considerable amount of sample-to-sample correlations within each individual band. For these correlated signals, the APC technique, which attempts to minimize the rms error of the coded signal, is an efficient method of encoding the speech waveform into digital form. In fact, operations of the APC algorithm include the prediction of the past history of the waveform and the coding of the residual error signal formed by subtracting the estimate from the input speech. In this algorithm, efficient encoding is achieved because quantization is only applied to the residual error signal and prediction parameters which have significantly less dynamic range and sample-to-sample correlation as compared to the original signal. Moreover, the distortion from the quantization of the residual signal is the major source of speech degradation. In general, the power of the quantization noise is proportional to the power of the residual error signal. Thus, accurate prediction is essential to the minimization of this quantization error. Although small quantization error does not always mean small distortion perceptually, it generally leads to the production of a high quality synthesized speech. The following sections will discuss the design of a special class of split-band filters known as Quadrature Mirror Filters, the encoding of both low and high bands using APC coders, noise shaping algorithms, and the quantization of the residual waveforms.

## 2.2 Design of Quadrature Mirror Filters

A straightforward way of achieving band splitting is to perform band-pass filtering with the translation of the resulting signal spectrum to DC. This spectral translation can be accomplished in a variety of ways and with varying cost factors concerning efficiency, spectral distortion, and ease of implementation. The most common method is via integer-band sampling where the original signal, after filtering into several frequency bands of bandwidths  $f_i$  using FIR filters, is resampled at  $2f_i$ . To minimize distortions introduced by the band-splitting process alone, filter characteristics such as flat passband response, high stop-band attenuation, and short transition region are extremely desirable. To satisfy the above requirements, the FIR filters required is often of large order, thus increasing the amount of processing tremendously.

Recently, Quadrature Mirror Filters (QMF) have been successfully applied to the split-band or subband coding of speech signals [1, 2]. It has been shown that these QMF's can assure the perfect band-splitting and reconstruction of the input signals regardless of the filter length. For the sake of completeness, a discussion of the theory of QMF is included in Appendix A. It illustrates the fact that if the half-band filters satisfy constraints as defined in Eqs. (A-17 to A-19), no spectral distortion is introduced in the band-splitting and reconstruction processes. However, a filter that fulfills exactly all the QMF constraints is useless for a split-band coding scheme. To illustrate this, rewriting Eq. (A-13) in the Appendix A yields:

$$\hat{X}(Z) = 1/2[H_1^2(Z) - H_2^2(Z)]X(Z) \quad (2-1)$$

where  $\hat{X}(Z)$ ,  $X(Z)$ ,  $H_1(Z)$ ,  $H_2(Z)$  are the Z-transforms of the output, the input, the lowband filter, the highband filter, respectively. Defining the transfer function of the overall QMF structure as  $H_{QMF}$ , its Z-transform is given by:

$$H_{QMF}(Z) = 1/2[H_1^2(Z) - H_2^2(Z)] \quad (2-2)$$

Equivalently, its impulse response is shown as:

$$h_{QMF}(n) = 1/2(h_1(n) \otimes h_1(n) - h_2(n) \otimes h_2(n)) \quad (2-3)$$

where  $\otimes$  denotes the convolution operation. If  $h_1(n)$  is represented by its even and odd parts,

$$h_1(n) = h_{1e}(n) + h_{1o}(n) \quad (2-4)$$

$h_2(n)$  defined as

$$h_2(n) = (-1)^n h_1(n) \quad n = 0, 1, \dots, N-1 \quad (2-5)$$

can be written as:

$$h_2(n) = h_{1e}(n) - h_{1o}(n) \quad (2-6)$$

Substituting Eqs. (2-4) and (2-6) into Eq. (2-3),  $h_{QMF}$  becomes:

$$h_{QMF}(n) = 2 h_{1e}(n) \otimes h_{1o}(n) \quad (2-7)$$

As dictated by the QMF constraints, the perfect bandsplitting and reconstruction requires  $H_{QMF}(Z) = 1$  which means:

$$h_{QMF}(n) = \begin{cases} 1 & ; n=0 \\ 0 & ; n \neq 0 \end{cases} \quad (2-8)$$

From Eq. (2-7), this is only valid if the filter  $h_1(n)$  has two non-zero and identical tap values. Hence, a true QMF can indeed be designed, but



its two tap values generally do not yield sharp cutoff characteristics. Moreover, split-band coding techniques really do not offer any advantages over the full-band schemes unless the subbands have distinctly different frequency characteristics. This implies that the split-band filter should be a higher order one which has a faster roll-off in addition to meeting most of the requirements as stated in Eq. (A-17) to (A-19) of Appendix A.

In general, the half-band filters  $h_1(n)$ , are difficult to design when using conventional computer-aided design algorithms in order to satisfy all the QMF constraints. Of all well-known classes of digital filter design techniques, the McClellan-Parks algorithm is the most popular [3]. This algorithm, which uses the Remez exchange procedure, introduces several extremes in both pass and stopband regions. Although excellent stopband rejections can be achieved, the ripples cannot be . . . guaranteed to combine in such a way that Eq. (A-19) is satisfied. In addition, since the 3-dB point cannot be designed easily to be at the half-band frequency, symmetry requirements are not easily attained. To minimize the interaction between the passband and the stopband of the SBAPC system, design techniques that yield lowpass filters with a smooth passband response which fall off sharply after the 3-dB point and which have high stopband rejection have to be investigated.

#### 2.2.1 The Windowing Technique

One simple approach to design lowpass filters that possess the above characteristics is to use the windowing technique. Depending on the type of windows utilized, short transition regions can be realized with a relatively low filter order. To illustrate the method, let's start with the frequency response of an ideal lowpass filter given as [3]:

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\alpha} & ; |\omega| < \omega_c \\ 0 & ; \text{o.w.} \end{cases} \quad (2-9)$$

where  $\alpha$  is the delay of the filter and  $\omega_c$  is the cutoff frequency in radians. Then the impulse response of the ideal filter is given by the inverse Fourier transform of  $H_d(e^{j\omega})$  as:

$$h_d(n) = \begin{cases} \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega(n-\alpha)} d\omega & ; n = \alpha \\ \sin \frac{\omega_c(n-\alpha)}{\pi(n-\alpha)} & ; n \neq \alpha \end{cases} \quad (2-10)$$

In order to design a finite-impulse-response filter with a zero phase delay, a window function  $W(n)$  is applied to  $h_d(n)$  as follows:

$$h(n) = h_d(n) W(n) \quad (2-11)$$

and  $\alpha$  is selected as

$$\alpha = \frac{N-1}{2} \quad (2-12)$$

where  $N$  is the desired filter length.

There has been considerable research done on the design of digital filters with various window functions  $W(n)$ . For these windows, the tradeoffs between different filter parameters, such as the passband response, transition region, stopband rejection, etc., have been well documented [4]. Among them, the Hanning window which results in filters with a

large stopband rejection and a short transition region with relatively low filter order can be applied to designing QMF.

In this case, the window function  $W(n)$  given as:

$$W(n) = \frac{1}{2} \left( 1 - \cos\left(\frac{2\pi n}{N-1}\right) \right); \quad 0 \leq n \leq N-1 \quad (2-13)$$

is multiplied with  $h_d(n)$  as depicted in Eq. (2-10). In order to satisfy the QMF constraints,  $N$  has to be even and  $w_c$  has to be determined experimentally to cutoff at the half-band frequency. Since the two end-points of the Hanning window are zeros, a window length of  $(N+2)$  points is employed to design a  $N$ th order QMF.

Frequency responses of a 60-tap and a 32-tap QMF designed using the Hanning window are shown in Figures 2.2.1 and 2.2.3. Both filters exhibit flat passband responses of less than 0.07 dB ripple, large stopband rejections in excess of 50 dB and cutoff frequencies at the half-band point (1600 Hz). Though the 32-tap filter has twice the transition bandwidth (400 Hz) as compared to the 60-tap one, the utility of the shorter filter in the SBAPC algorithm represents a good compromise between complexity and performance. Employing these filters, the frequency responses of unquantized SBAPC systems are shown in Figures 2.2.2 and 2.2.4. Both graphs depict a uniform response of less than 0.4 dB ripple which further substantiate the fact that these Hanning filters satisfy most of the QMF constraints and they do not introduce much distortion in the band-splitting and reconstruction process.

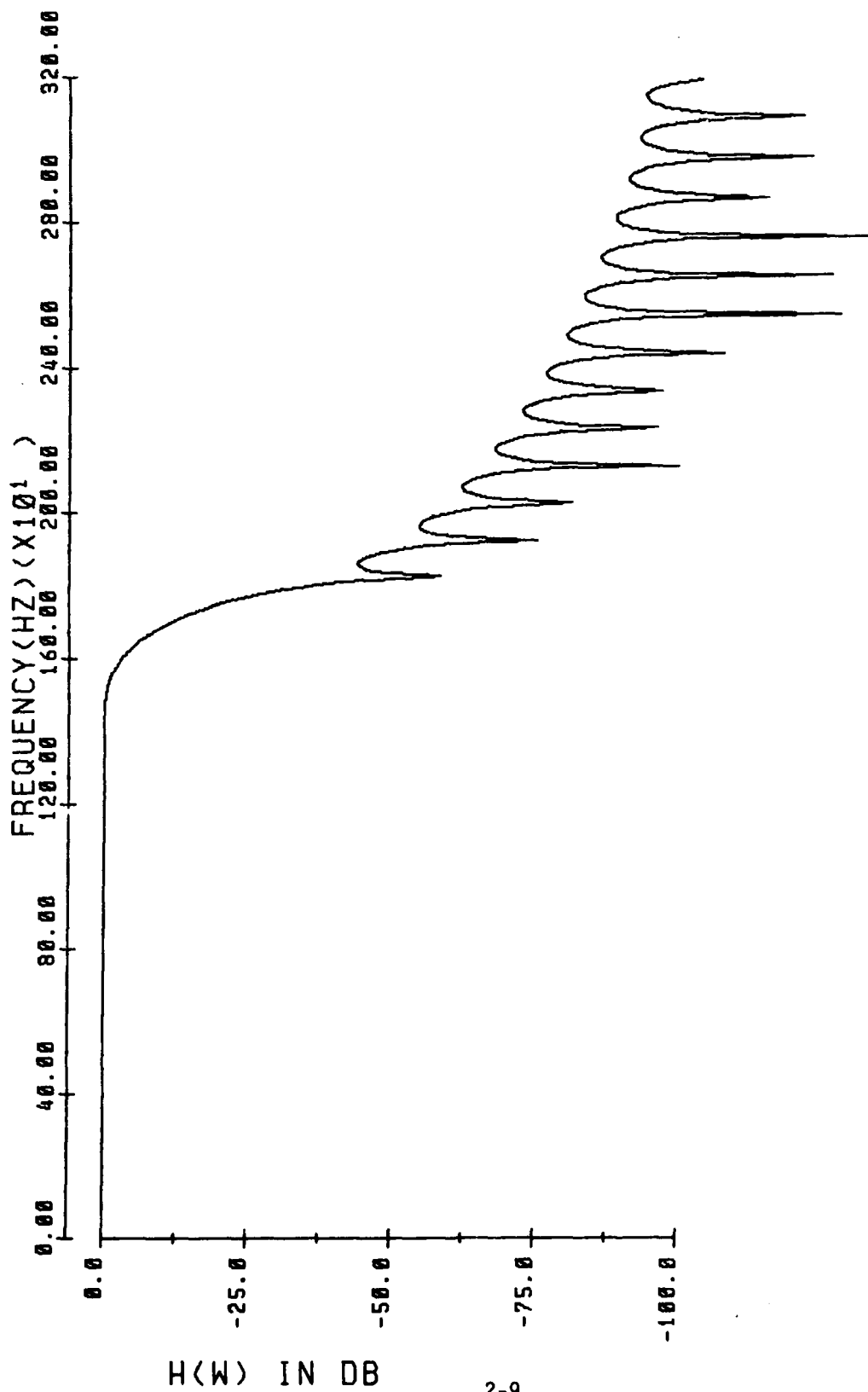
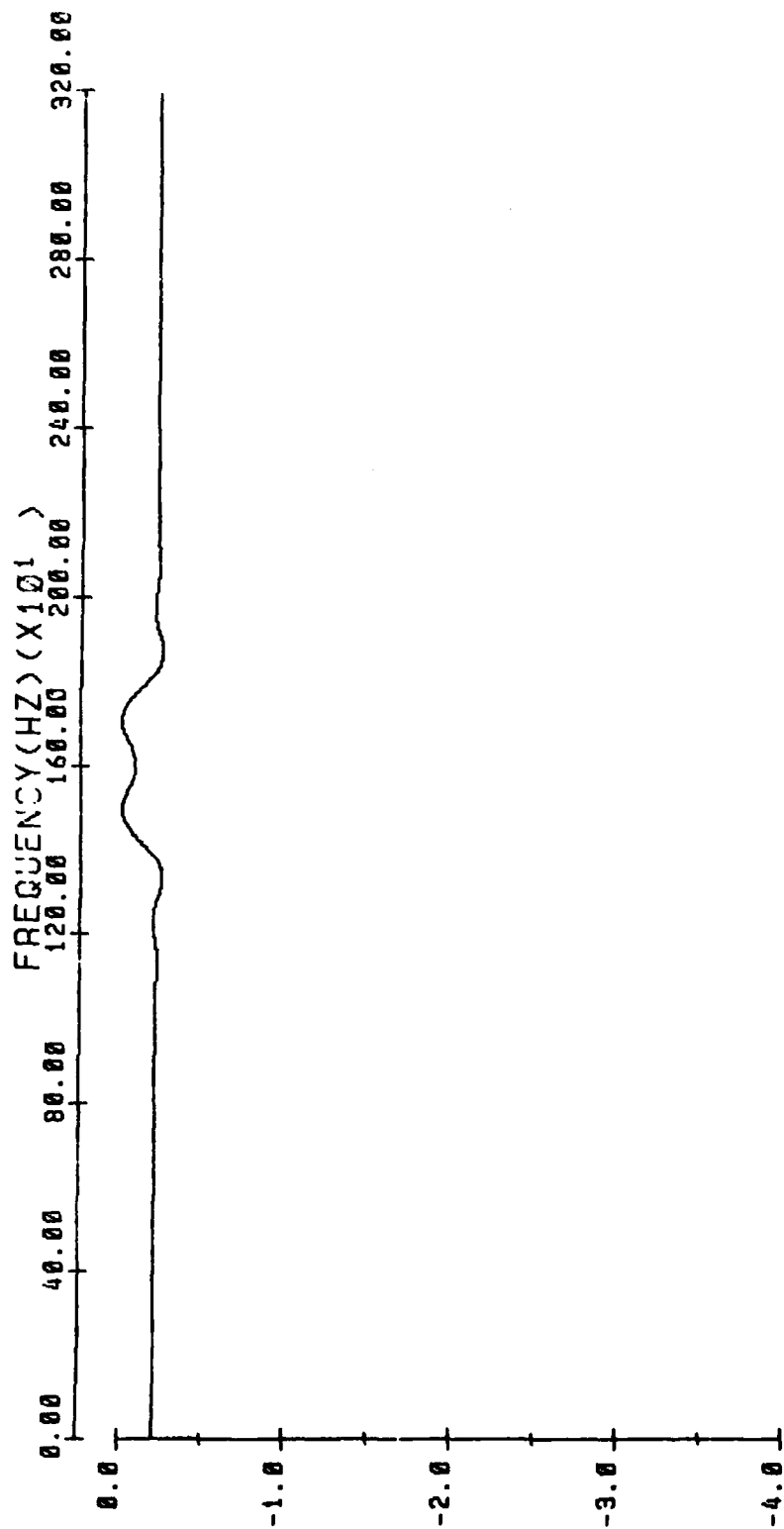


FIGURE 2.2.1: MAGNITUDE RESPONSE OF A 60-TAP QMF DESIGNED USING THE HANNING WINDOW METHOD



H( $\omega$ ) IN DB

2-10

FIGURE 2.2.2: MAGNITUDE RESPONSE OF AN UNQUANTIZED SBAPC SYSTEM  
WITH THE 60-TAP QMF

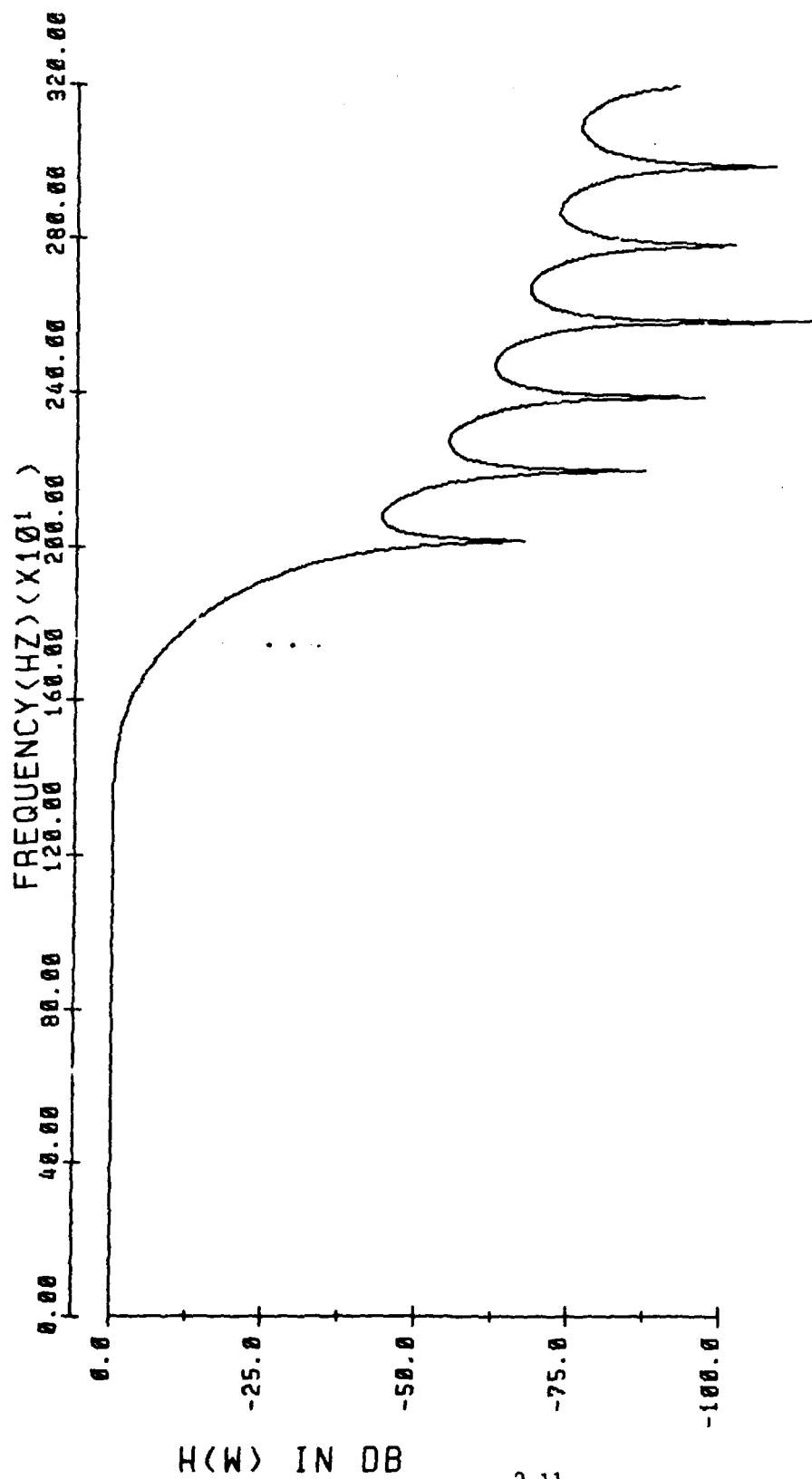


FIGURE 2.2.3: MAGNITUDE RESPONSE OF A 32-TAP QMF DESIGNED USING THE HANNING WINDOW METHOD

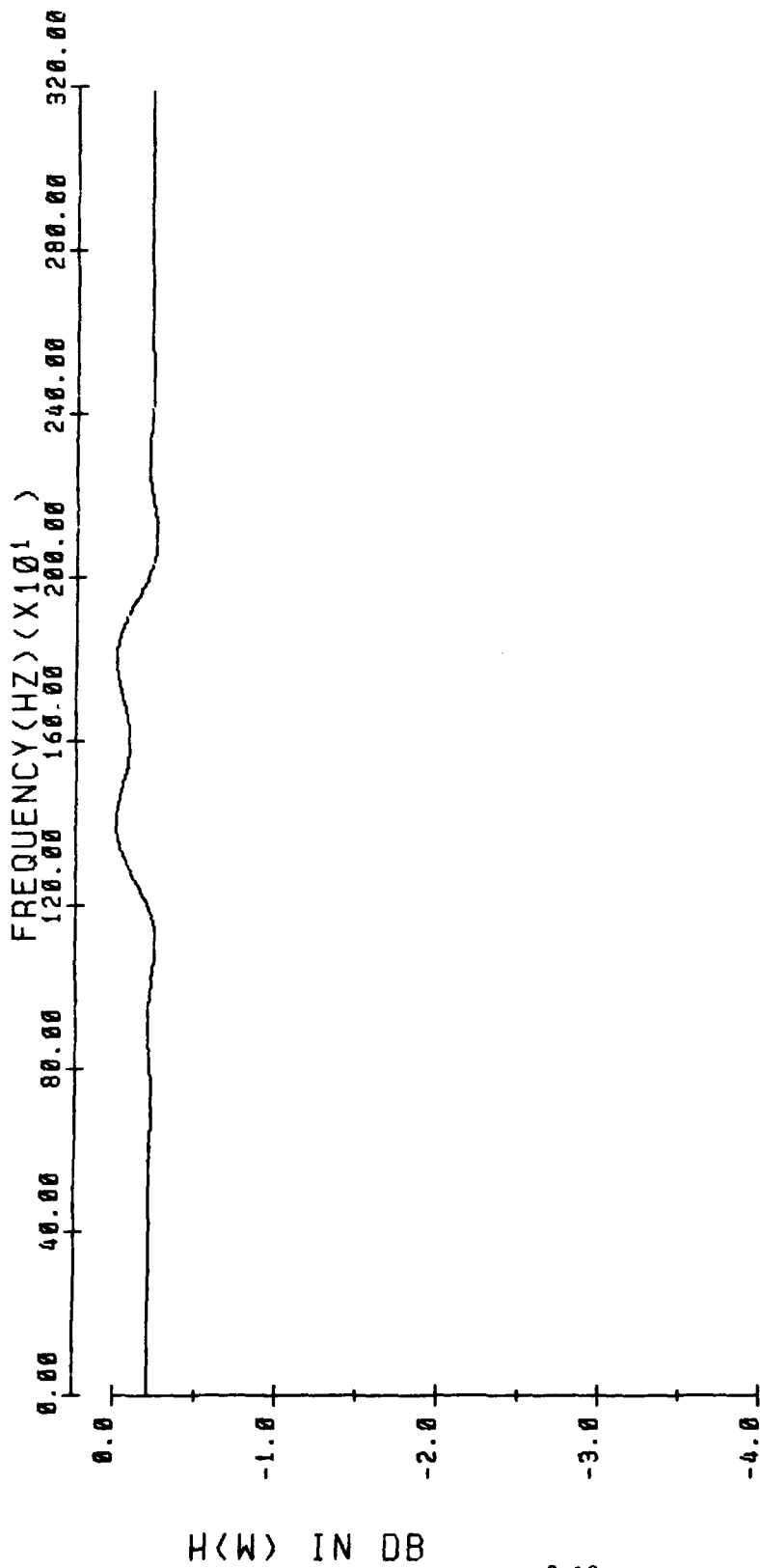


FIGURE 2.2.4: MAGNITUDE RESPONSE OF THE UNQUANTIZED SBAPC SYSTEM  
WITH THE 32-TAP QMF

### 2.2.2 The Optimization Technique

As discussed in Section 2.2.1, the Hanning window is a very simple technique to design filters that perform like QMF's. Though the magnitude response of the unquantized SBAPC system that utilizes these filters still exhibits a 0.4 dB "hump," it is nevertheless a good starting point in designing true QMF's. Recently, an optimization procedure has been proposed which results in QMF through the minimization of a performance index defined as [5]:

$$E = E_r + \alpha E_s(f_{SB}) \quad (2-14)$$

where  $\alpha$ ,  $f_{SB}$  are the weighting, the frequency of the stopband;  $E_r$  is the ripple energy given as:

$$E_r = 2 \sum_{w=0}^{\pi/2} (H_1^2(w) + H_1^2(\pi-w) - 1) \quad (2-15)$$

and  $E_s$  is the out-of-band energy given as:

$$E_s(f_{SB}) = \sum_{w=f_{SB}}^{\pi} H_1^2(w) \quad (2-16)$$

Utilizing the filter coefficients obtained through the Hanning window scheme as a starting point, an iterative search algorithm is formulated in locating the local minimum of  $E$ . QMF's designed using this method have been tabulated and an example of a 32-tap filter is included in Table 2-1. The magnitude response of the filter and the unquantized SBAPC system employing this filter are shown in Figure 2.2.5 and Figure 2.2.6, respectively. As compared to the 32-tap Hanning filter as depicted in Figures 2.2.3 and 2.2.4, the new filter is greatly improved in the sense that it exhibits a flatter unquantized SBAPC sys-



$h_1(0) = +0.69105790E-03 = h_1(31)$   
 $h_1(1) = -0.14037930E-02 = h_1(30)$   
 $h_1(2) = -0.12683030E-02 = h_1(29)$   
 $h_1(3) = +0.42341950E-02 = h_1(28)$   
 $h_1(4) = +0.14142460E-02 = h_1(27)$   
 $h_1(5) = -0.94583180E-02 = h_1(26)$   
 $h_1(6) = -0.13038590E-03 = h_1(25)$   
 $h_1(7) = +0.17981450E-01 = h_1(24)$   
 $h_1(8) = -0.41874830E-02 = h_1(23)$   
 $h_1(9) = -0.31238620E-01 = h_1(22)$   
 $h_1(10) = +0.14568440E-01 = h_1(21)$   
 $h_1(11) = +0.52947450E-01 = h_1(20)$   
 $h_1(12) = -0.39348780E-01 = h_1(19)$   
 $h_1(13) = -0.99802430E-01 = h_1(18)$   
 $h_1(14) = +0.12855790E+00 = h_1(17)$   
 $h_1(15) = +0.46640530E+00 = h_1(16)$

TABLE 2-1: TABULATION OF THE 32-  
 TAP QMF DESIGNED USING  
 THE OPTIMIZATION METHOD

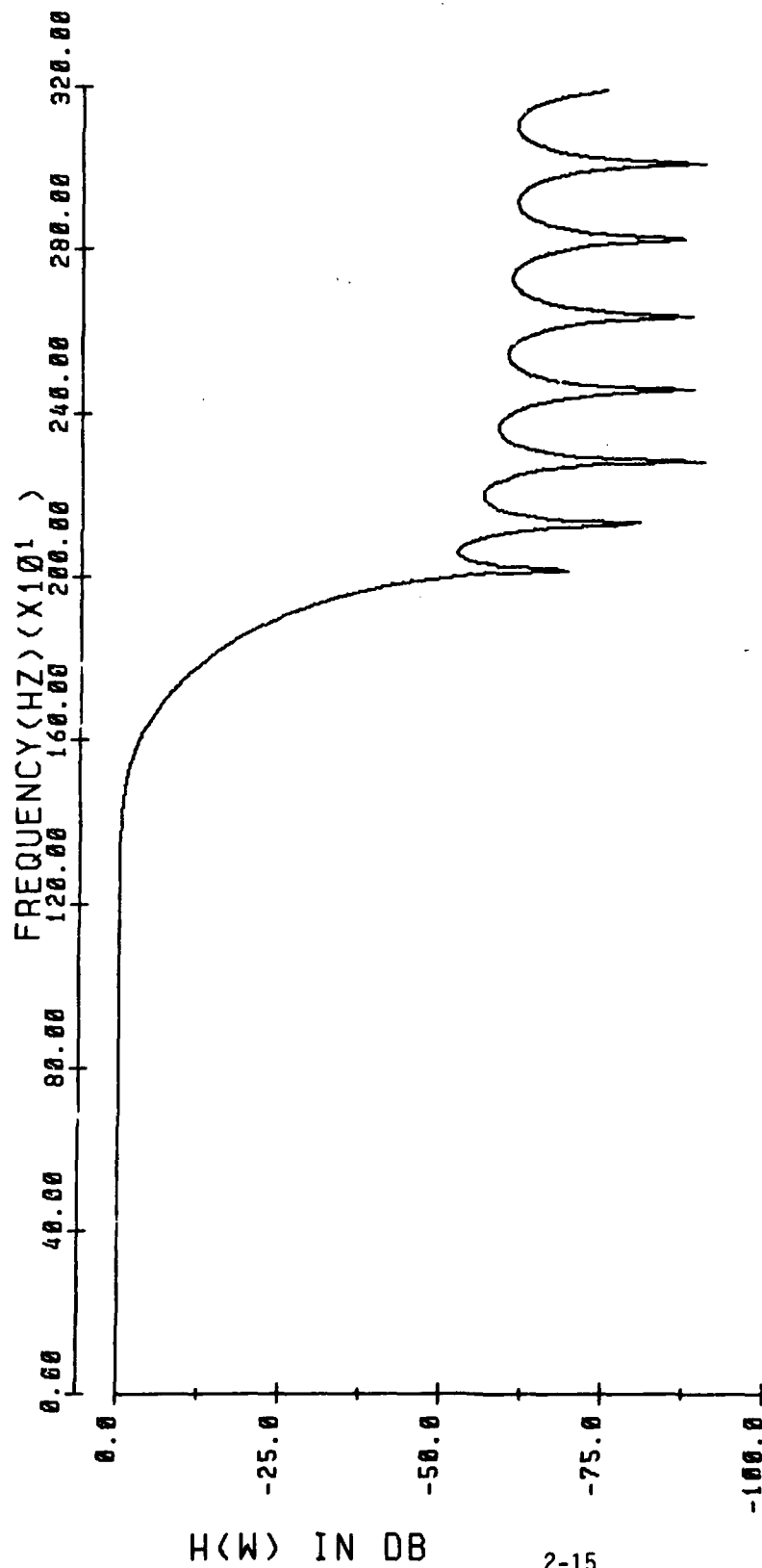


FIGURE 2.2.5: MAGNITUDE RESPONSE OF A 32-TAP QMF DESIGNED USING THE OPTIMIZATION PROCEDURE

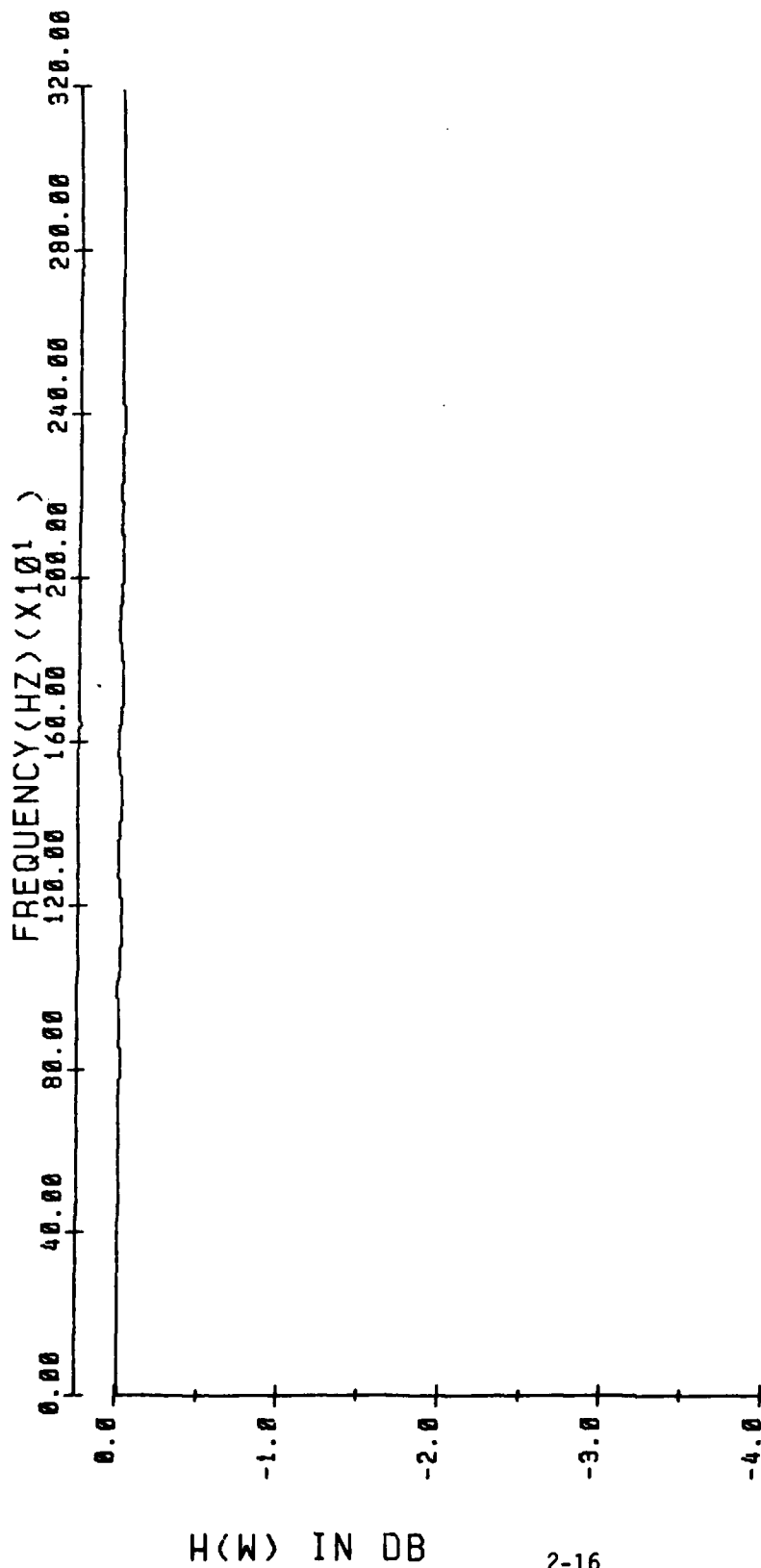


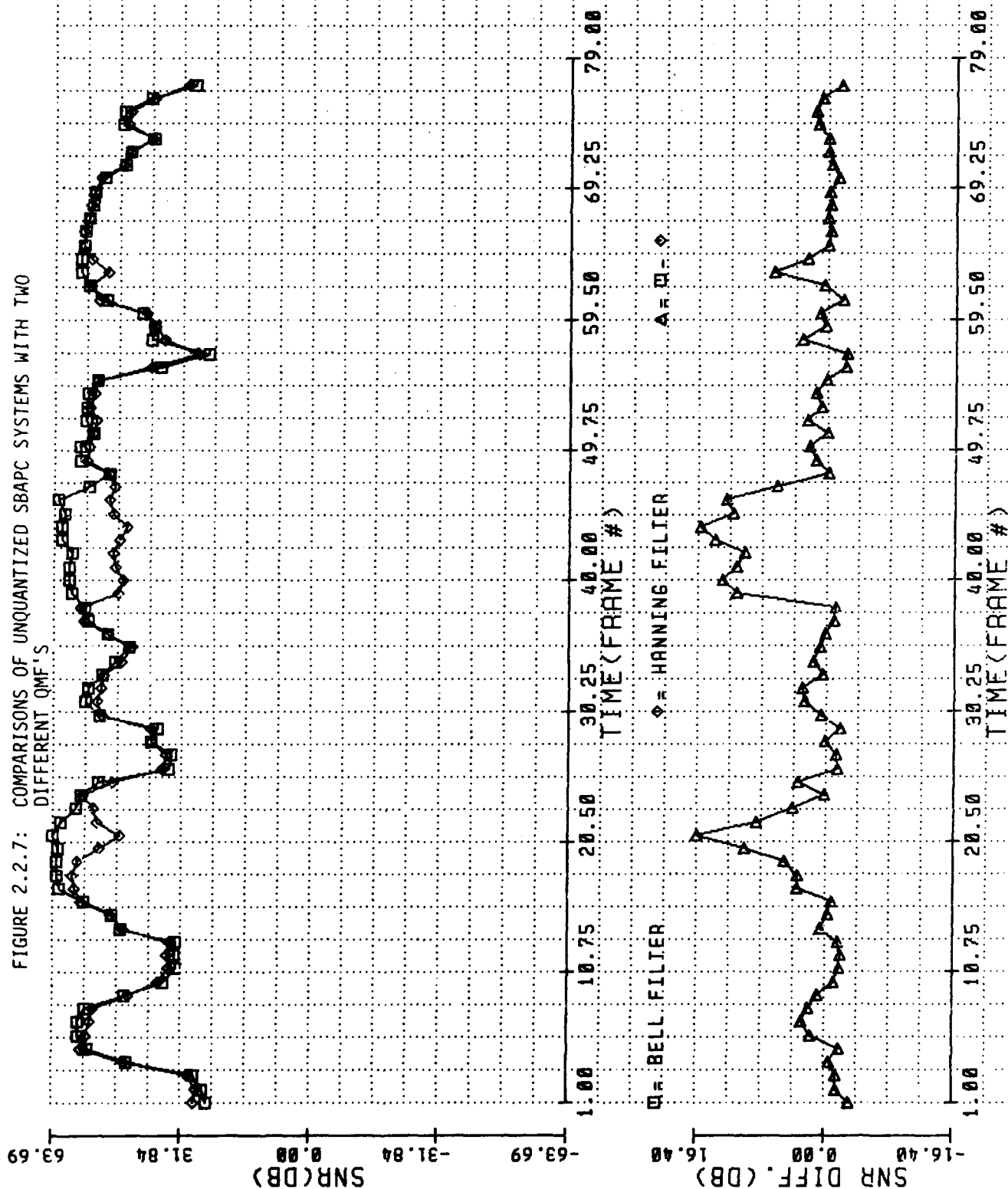
FIGURE 2.2.6: MAGNITUDE RESPONSE OF AN UNQUANTIZED SBAPC SYSTEM  
WITH THE 32-TAP QMF DESIGNED USING THE OPTIMIZATION  
TECHNIQUE

tem response without sacrificing much transition bandwidth and stopband rejection. Though informal listening tests conducted on the unquantized SBAPC processed sentences with the two 32-tap QMF's indicate no audible differences, S/N ratio plots of these systems, as depicted in Figure 2.2.7, show that the new filter consistently out-performs the Hanning filter especially during voiced regions. As a result, the 32-tap filter designed using the optimization procedure is employed in the subsequent studies.

### 2.3 Adaptive Predictive Coding of Split-Band Signals

APC algorithms have been extensively studied and reported on in the literature [6] - [8]. Most systems differ from one to another in the manner of parameter extractions and the design of quantizers with various level of complexity. In this section, the design of adaptive predictive coders, which minimizes the power of quantization error or maximizes the signal-to-quantization noise (S/Q), will be considered.

FIGURE 2.2.7: COMPARISONS OF UNQUANTIZED SBAPC SYSTEMS WITH TWO DIFFERENT QMF'S



### 2.3.1 Adaptive Predictive Coder with one Loop

The APC system with one loop is shown in Figure 2.3.1. In this scheme, the estimate of the present speech sample is assumed to be

$$\hat{s}_n = \sum_{i=1}^P a_i s_{n-i} + b_1 s_{n-M+1} + b_2 s_{n-M} + b_3 s_{n-M-1} \quad (2-17)$$

where M represent the number of speech samples in one pitch period and P is the predictor order in the prediction loop. Here, we consider a 3rd order pitch predictor, although a first order pitch predictor is common in conventional APC systems. The difference between the input speech sample  $s_n$  and the estimate  $\hat{s}_n$  can be expressed as:

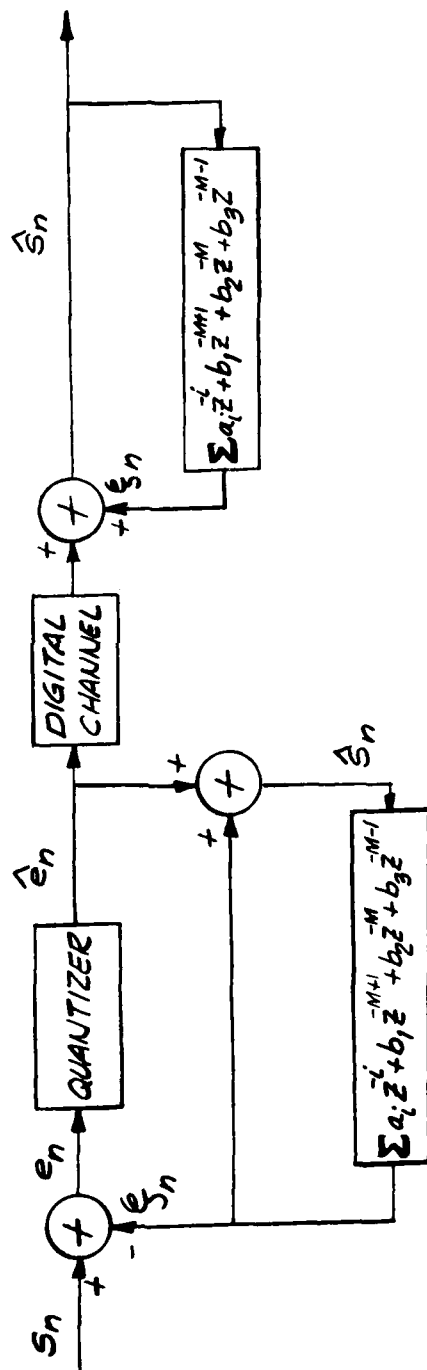
$$e_n = s_n - \hat{s}_n \quad (2-18)$$

The total squared error may be shown as:

$$\begin{aligned} E &= \sum_{n=1}^L e_n^2 \\ &= \sum_{n=1}^L \left[ s_n - \left( \sum_{i=1}^P a_i s_{n-i} + b_1 s_{n-M+1} + b_2 s_{n-M} + b_3 s_{n-M-1} \right) \right]^2 \end{aligned} \quad (2-19)$$

where L is the number of samples within a frame. In order to minimize the total squared error, E is differentiated with respect to  $\{a_i, b_i\}$  and setting the results to zeros, yields:

$$\underline{Ra} = \underline{c} \quad (2-20)$$



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FIGURE 2.3.1 BLOCK DIAGRAM OF AN APC SYSTEM WITH ONE LOOP

where  $R$  is an autocorrelation matrix;  $\underline{a}$  and  $\underline{c}$  are column vectors defined as:

$$\underline{a} = \begin{bmatrix} a_1 \\ \cdot \\ \cdot \\ \cdot \\ a_p \\ b_1 \\ b_2 \\ b_3 \end{bmatrix} \quad (2-21)$$

and

$$\underline{c} = \begin{bmatrix} r_1 \\ \cdot \\ \cdot \\ \cdot \\ r_p \\ r_M \\ r_{M+1} \\ r_{M+2} \end{bmatrix} \quad (2-22)$$

where  $r_i$  is the autocorrelation coefficient of the input speech  $s_n$  with that of a delay  $i$ . Let the column vector  $\underline{d}$  be

$$\underline{d} = \begin{bmatrix} 1 \\ 2 \\ \cdot \\ \cdot \\ \cdot \\ p \\ M-1 \\ M \\ M+1 \end{bmatrix} \quad (2-23)$$



then the elements of the autocorrelation matrix, R, can be expressed as

$$r_{ij} = r_{|d_i - d_j|} \quad (2-24)$$

$$r_{|d_i - d_j|} = \frac{1}{L - |d_i - d_j|} \sum_{n=1}^{L - |d_i - d_j|} s_n s_{n + |d_i - d_j|}$$

In this APC scheme, the autocorrelation coefficients  $\{r_i\}$  are needed to define the vector  $\underline{c}$  in eq.(2-22) and the autocorrelation matrix R in eq.(2-24). Since the number of the required autocorrelation coefficients is large, their calculation can be best made via the fast Fourier transform technique. Then the calculation of  $\{a_i, b_i\}$  can be performed from eq.(2-20) by multiplying the inverse of the matrix R with  $\underline{c}$  as follows:

$$\underline{a} = R^{-1} \underline{c} \quad (2-25)$$

The values of the column vector  $\underline{a}$  will be used for the computation of the residual signal.

### 2.3.2 Adaptive Predictive Coder with two Loops

The block diagram of a two-loop APC system is shown in Figure 2.3.2. In this scheme, the predictor loops are divided into  $P_1$  and  $P_2$ . Acknowledging the fact that speech signals are often quasi-periodic with period  $M$ , the loop  $P_1$  can be used to reduce the redundancy. In particular, if a 3rd order pitch predictor is utilized, the present sample may be estimated as:

$$s_n = \beta_1 s_{n-M+1} + \beta_2 s_{n-M} + \beta_3 s_{n-M-1} \quad (2-26)$$

where  $\beta_i$ 's are the pitch prediction coefficients. Third order pitch predictor is best used to compensate the effects of the quantization error in estimating the pitch period. Let the residual error be

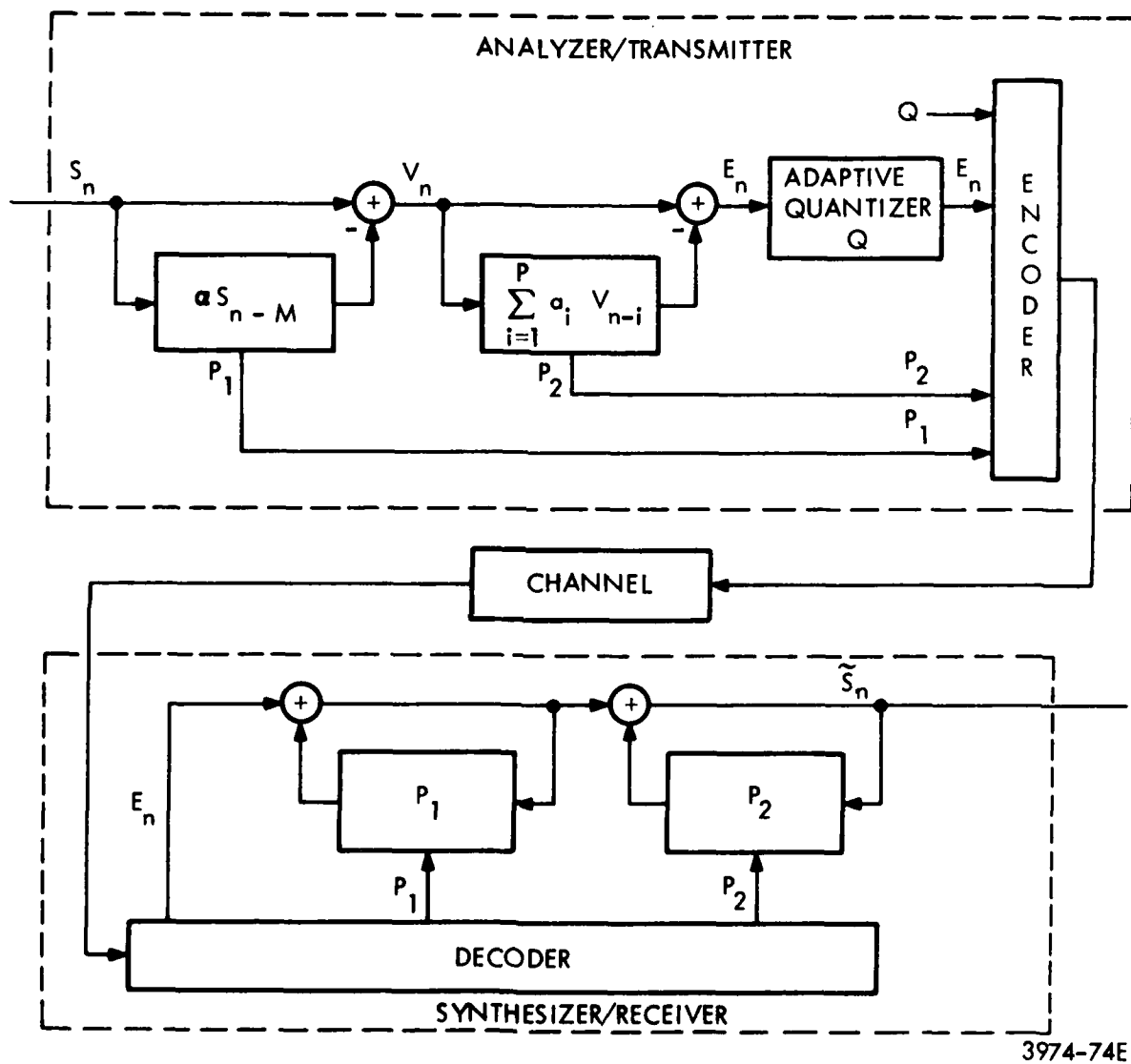
$$v_n = s_n - \hat{s}_n \quad (2-27)$$

$$= s_n - \beta_1 s_{n-M+1} - \beta_2 s_{n-M} - \beta_3 s_{n-M-1}$$

Then, the total squared error may be expressed as:

$$E = \sum_{n=1}^L v_n^2 \quad (2-28)$$

where  $L$  is the number of samples within a frame. In order to minimize the total squared error, differentiating  $E$  with respect to  $\beta_i$  and setting the results to zeros, yield:



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FIGURE 2.3.2: BLOCK DIAGRAM OF AN ADAPTIVE PREDICTIVE CODER WITH TWO LOOPS

$$\begin{bmatrix} \gamma_{11} & \gamma_{12} & \gamma_{13} \\ \gamma_{21} & \gamma_{22} & \gamma_{23} \\ \gamma_{31} & \gamma_{32} & \gamma_{33} \end{bmatrix} \begin{bmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \end{bmatrix} = \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} \quad (2-29)$$

where

$$\alpha_i = \sum_{n=1}^L S_n S_{n-M+2-i}, \quad i = 1, 2, 3 \quad (2-30)$$

and

$$r_{ij} = \sum_{n=1}^L S_{n-M+2-i} S_{n-M+2-j}, \quad i, j = 1, 2, 3 \quad (2-31)$$

For quasi-periodic inputs, such as vowels, the magnitude of  $\beta_i$  is large while the magnitude of  $\beta_j$  is near zero for noise-like consonants.

The reduced waveform still contains sufficient redundancy such that a second predictor loop can further reduce the output signal energy, especially if the speech is not periodic or if the pitch period is estimated incorrectly. This second predictor uses a weighted sum of  $P$  past samples of the speech waveform to form the estimate as

$$\hat{v}_n = \sum_{i=1}^P a_i v_{n-i} \quad (2-32)$$

where  $P$  is the order of the predictor and  $\{a_i\}$ 's are chosen to minimize the total squared error

$$U = \sum_{n=1}^L (v_n - \hat{v}_n)^2 \quad (2-33)$$

The predictor coefficients can be obtained by inverting the following matrix equation:

$$\phi \underline{a} = \underline{c} \quad (2-34)$$

where the  $(i^{th}, j^{th})$  element of  $\phi$  is given as:

$$\phi_{ij} = \sum_{n=1}^L v_{n-i} v_{n-j} \quad (2-35)$$

and the  $i^{th}$  element of  $\underline{c}$  is shown as:

$$c_i = \sum_{n=1}^L v_n v_{n-i} \quad (2-36)$$

If we window the reduced waveform so that it is zero outside the frame interval  $1 \leq n \leq L$  (stationary assumption), eq.(2-34) is reduced to the autocorrelation normal equation;

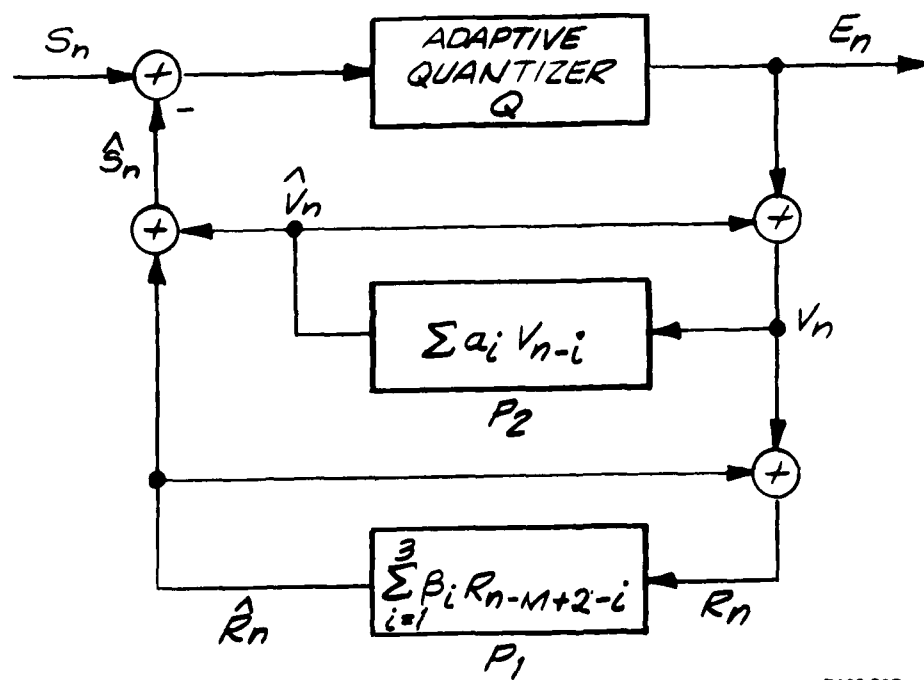
$$\begin{aligned} \phi_{ij} &= \sum_{n=1}^{L-|i-j|} v_n v_{n-|i-j|} \\ &= \gamma_{|i-j|} \end{aligned} \quad (2-37)$$

and

$$\begin{bmatrix} \gamma_0 & \gamma_1 & . & . & . & \gamma_{p-1} \\ \gamma_1 & \gamma_0 & . & . & . & \gamma_{p-2} \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ \gamma_{p-1} & \gamma_{p-2} & . & . & . & \gamma_0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ . \\ . \\ . \\ a_p \end{bmatrix} = \begin{bmatrix} \gamma_1 \\ \gamma_2 \\ . \\ . \\ . \\ \gamma_p \end{bmatrix} \quad (2-38)$$

This is a symmetric Toeplitz matrix because the elements along the principal diagonal and those that are parallel to the diagonal are identical. Efficient solutions exist that result in  $a_i$ 's that minimize the mean squared energy  $U$  in the difference signal. In addition, because the elements of the matrix arise from an autocorrelation function, the stationary matrix solution for the  $a_i$ 's will yield a stable filter during synthesis, with the recursive filters shown in Figure 2.3.3. Unfortunately, the  $a_i$ 's are not good transmission parameters because quantization or errors in transmission can cause the poles of the receiver filter given by  $1/(1-P_1)(1-P_2)$  to move outside the unit circle in the Z-plane, resulting in unstable waveforms. Consequently, auxiliary parameters called Partial Correlation (PARCOR) coefficients  $K_i$  (which are the negatives of reflection coefficients) are calculated from the  $a_i$ 's, and as long as these PARCOR coefficients have magnitudes less than unity, system stability is assured.

In the actual APC algorithm, instead of quantizing the error signal as depicted in Figure 2.3.2, the analyzer is re-formulated with the quantizer placed inside the filtering loop as shown in Figure 2.3.3. In the absence of the quantizer, this configuration has the same transfer function  $(1-P_1)(1-P_2)$  as that of Figure 2.3.2. However, with this new formu-



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FIGURE 2.3.3 RECONFIGURATION OF THE ANALYZER OF A TWO-LOOP APC TO MINIMIZE THE EFFECT OF QUANTIZATION

lation, it can be shown that the accumulation of quantization errors is eliminated. To illustrate this, the synthesized sample  $R_n$  is rewritten as follows:

$$R_n = V_n + \hat{R}_n \quad (2-39)$$

$$= V_n + \hat{S}_n - \hat{V}_n$$

$$= E_n + \hat{S}_n$$

Also,  $E_n$  is given by:

$$E_n = S_n - \hat{S}_n + q_n \quad (2-40)$$

where  $q_n$  is the quantization noise generated at the  $n$ th sample. Substituting eq.(2-40) into (2-39), the following is obtained:

$$R_n = S_n + q_n \quad (2-41)$$

From eq.(2-41), it is clear that the APC synthesized outputs are exactly equal to the inputs except for the quantizing noise  $q_n$ . In the case of the APC system with the quantizer outside the predictor loop, the synthesized output  $R_n$  is given by:

$$R_n = S_n + \tilde{q}_n \quad (2-42)$$



where  $\tilde{q}_n$  is defined as the output obtained when the quantizer noise  $q_n$  is fed into the inverse APC filter

$$\tilde{q}_n = q_n + \sum a_i \tilde{q}_{n-i} \quad (2-43)$$

With the APC system shown in Figure 2.3.2, the synthesized output is an estimate of the input signal plus quantization noise which is an accumulation of previous errors. Hence, with the use of the system shown in Figure 2.3.3, this accumulation effect can be totally avoided.

After computing the pitch gain  $\beta_i$ , the period  $M$ , and the PARCOR coefficient  $K_i$ , the analyzer digitally filters the speech and quantizes the error signal. Then the  $K_i$ ,  $\beta_i$ ,  $M$ , the quantized error sequence  $e_n$ , are quantized and sent to the receiver where the predictor coefficients are regenerated iteratively by computing:

$$a_j^{(i)} = a_j^{(i-1)} - a_{i-j}^{(i-1)} * K_i \quad j = 1, 2, 3, \dots, i-1 \quad (2-44)$$

$$a_i^{(i)} = K_i \quad i = 1, 2, 3, \dots, p \quad (2-45)$$

where  $a_j^{(i)}$  represents  $a_j$  on the  $i$ th iteration.

The synthesizer then creates an output time waveform that is both intelligible and pleasing to listen to. Moreover, this output is reasonably insensitive to errors in pitch extraction, because the P2 predictor on the reduced waveform and the quantization of the error signal can partially compensate for wrong pitch values used in the first predictor P1. In fact,

if the pitch period is incorrectly doubled, as it often happens in practice, then predictions made by the first loop P1 are generated from those that are two periods before, and this is not a serious error. If incorrect values for M are chosen, different values of  $\beta_i$  and PARCOR coefficients are also computed to compensate in part for this error. Finally, the error signal, though coarsely quantized, carries considerable information about the true pitch, should this pitch be incorrectly measured. Thus, the APC processed speech does not show severe degradation even in noisy acoustic environments and with many speakers where accurate pitch extraction is difficult.

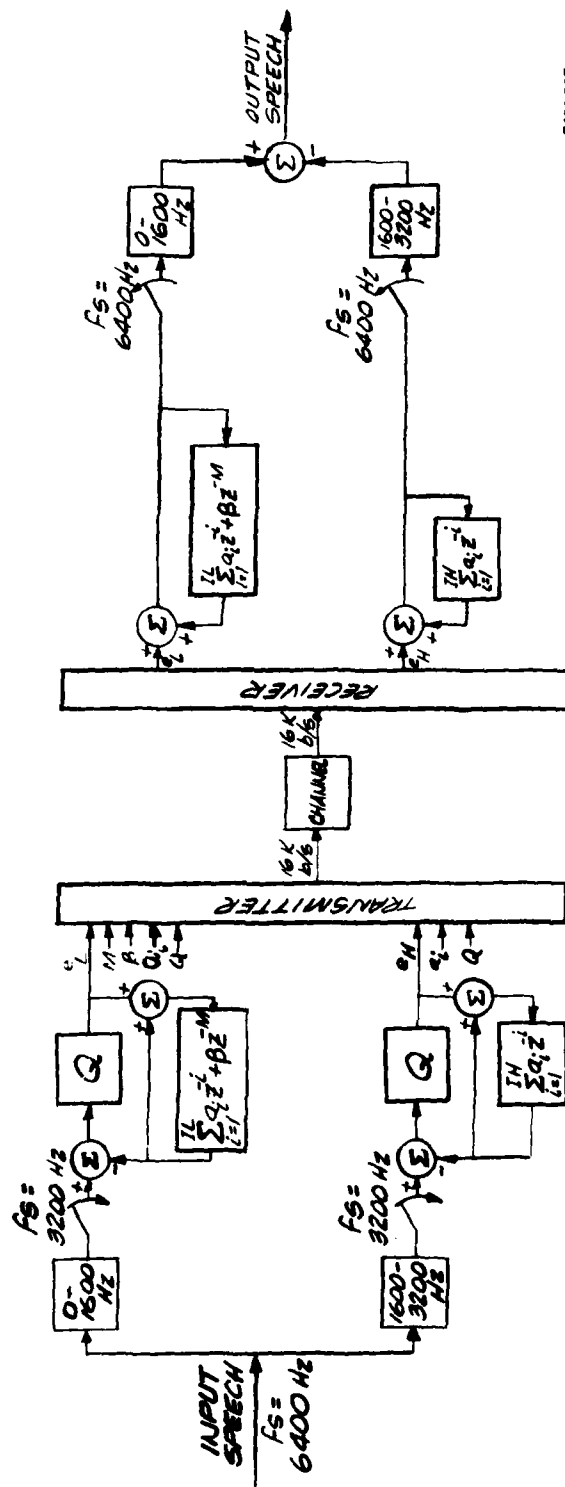
### 2.3.3 Tradeoff Analysis of SBAPC Systems

There are several parameters that affect the performance of a SBAPC system for a given transmission data rate, and they are: the sampling rate, the frame size or duration, the number of prediction loops, the order of the short-term predictors, the order of the pitch predictor, quantizer characteristics, bit allocations between side information parameters and residual error signals, and bit allocations between low and high band signals. In this study, a tradeoff analysis has been performed between the number of prediction loops, the order of the short-term predictor, and the order of pitch predictors in each band. Other factors relating to the performance of the SBAPC system have been fixed at values given by: sampling rate = 6400 Hz, frame size or duration = 22.5 msec, number of bits for encoding low-band error signal = 3, and number of bits for encoding high band error signal = 2. These configurations lead to a data rate slightly higher than 16 KBPS. Laplacian quantizers [9, 10] were used for the quantization of low and high band error signals until the new quantizer was developed from the actual distribution of the error signal's amplitudes. Quantizations were not applied to the parameters of side information, since the first objective of this tradeoff analysis was to determine the number of loops and the order of the predictor in each loop. The quantizations, bit allocations to the side information, the residual error signals, and forward error correcting code will be considered in the later sections.

#### 2.3.3.1 The Performance of the SBAPC System with one Loop

The block diagram of a SBAPC system with one loop is shown in Figure 2.3.4. In this scheme, only short-term predictors are considered in the high band prediction loop, since the signals of the high band often contain little information of pitch. The performance in terms of the signal-to-quantization noise ratio (S/Q) is tabulated in Table 2.2. In this experiment, the data rate used for encoding the error signal is 16 Kb/s. While the total data with side information is higher than 16 Kb/s, the purpose is to study the tradeoffs between the pitch predictor and various predictor orders of the high and low bands. As it is noted from this table, the signal-to-quantization noise ratio (S/Q) is high (about 20 dB). Consequently, the quality of the synthesized speech is very high. The performance of this scheme is better with a larger order of short-term predictors.

A typical S/Q plot of the 1-loop SBAPC systems with and without the pitch predictor are shown in Figure 2.3.5. As it is noted from this figure, the performance is insensitive with respect to the presence of the pitch predictor. Only one pitch related predictor is considered in the evaluation of performance since the system is often unstable for large order ( $\geq 2$ ) of pitch related predictors. Also, the S/Q from Table 2.2 indicates that small number of prediction coefficients ( $\approx 4$ ) is preferable since the performance does not improve significantly when more than 4 prediction coefficients are used.



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FIGURE 2.3.4 BLOCK DIAGRAM OF THE SBAPC SYSTEM WITH ONE LOOP

LB Order \ HB Order	2	4	6
4	20.14 dB <sup>+</sup>	20.43 <sup>+</sup>	20.47 <sup>+</sup>
	19.83 *	20.12 *	20.17 *
6	20.37 +	20.66 <sup>+</sup>	20.70 <sup>+</sup>
	20.19 *	20.48 *	20.53 *
8	20.55 +	20.87	20.92 <sup>+</sup>
	20.31 *	20.61 *	20.65 *

<sup>+</sup> with one pitch predictor  
\* with no pitch predictor

HB = High Band

LB = Low Band

Table 2.2: Signal-to-Quantization Noise Ratios of the SBAPC System with one loop at 16 KBPS

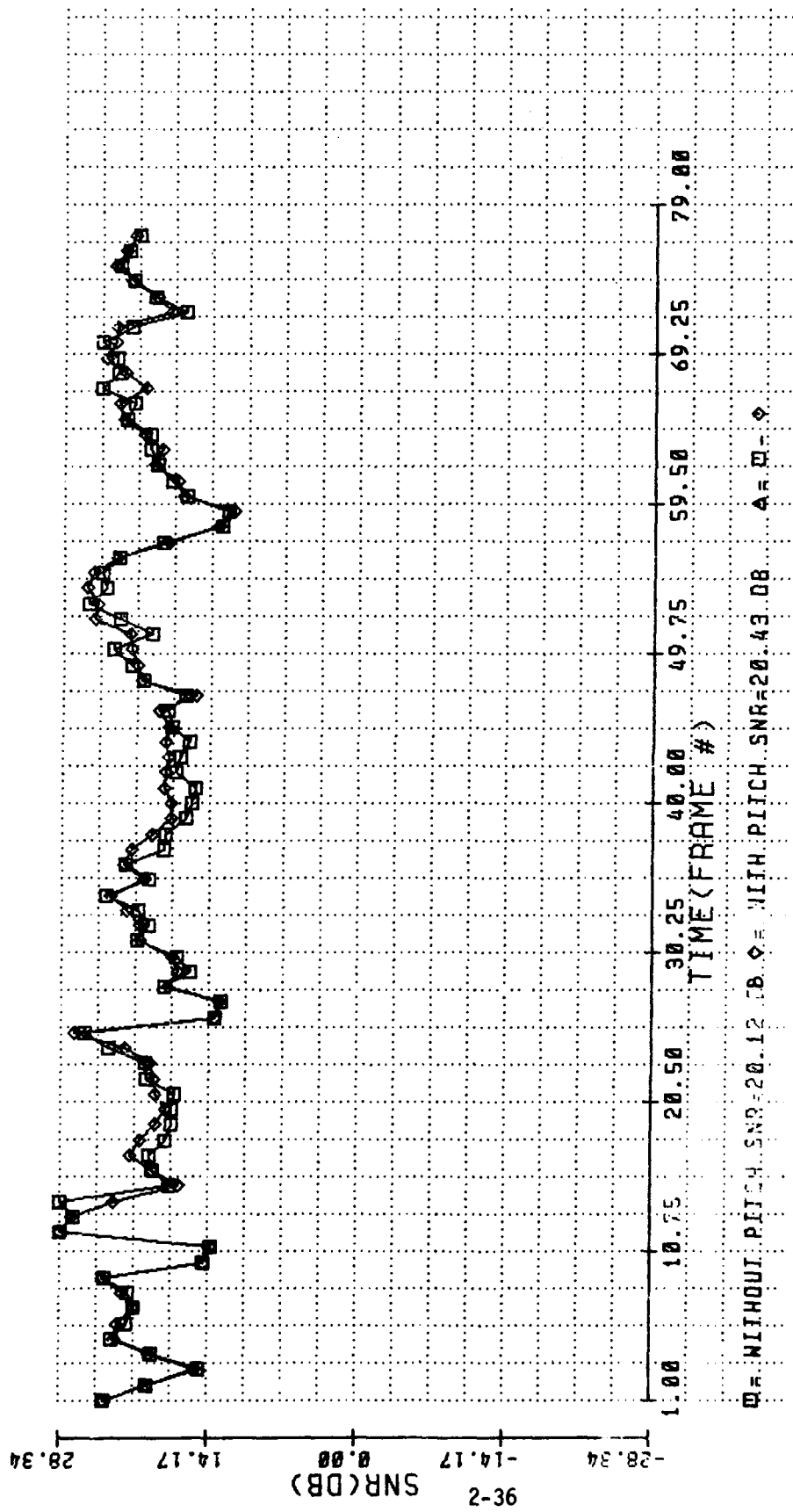


FIGURE 2.3.5: A SIGNAL-TO-QUANTIZATION NOISE RATIO PLOT OF THE 16 KBPS SBAPC SYSTEM WITH ONE LOOP

### 2.3.3.2 The Performance of a SBAPC System with two Loops

The block diagram of a SBAPC system with two loops is shown in Figure 2.3.6. In this scheme, only short-term predictors (one loop) are considered in the high band since signals of the high band after downsampling often contain little information about pitch. The performance in terms of S/Q are tabulated in Table 2.3 with the order of predictors as a variable. The S/Q of the SBAPC system with two loops increases as the order of the low-band predictors increases as shown in Table 2.3. However, the improvement is not that dramatic with the increase in higher band predictors. The SBAPC system with one loop (when the pitch information is not used) performs as well as this scheme for unvoiced frames. However, the SBPAC system with two loops always performs better than the system with one loop for voiced speech. In this scheme, the first order pitch loop results in an increase of 2-3 dB of S/Q over the scheme with no pitch predictor. An additional increase of 1-2 dB of S/Q may be obtained if three pitch predictors are used, but the system is sometimes unstable at low data rates. At 16 KBPS, these distortions are not noticeable in informal listening tests. As the data rate decreases to 9.6 KBPS, the lowering in S/Q becomes more perceptible. Especially noticeable is the hissing noise at high frequencies when no pitch loop was used. This noise degrades much of the speech quality at data rates below 9.6 KBPS.





LB Order \ HB Order	2	4	6
4	22.25 dB <sup>+</sup>	22.59 <sup>+</sup>	22.66 <sup>+</sup>
	23.46 *	23.77 *	23.83 *
6	22.49 <sup>+</sup>	22.86 <sup>+</sup>	22.94 <sup>+</sup>
	23.58 *	23.91 *	23.97 *
8	22.81 <sup>+</sup>	23.19 <sup>+</sup>	23.26 <sup>+</sup>
	23.72 *	24.04 *	24.11 *

<sup>+</sup> with one pitch predictor

\* with three pitch predictors

Table 2.3 Signal-to Quantization Noise Ratio of a  
SBAPC System with two loops at 16 KBPS

## 2.4 The Shaping of Quantization Noise in SBAPC Systems

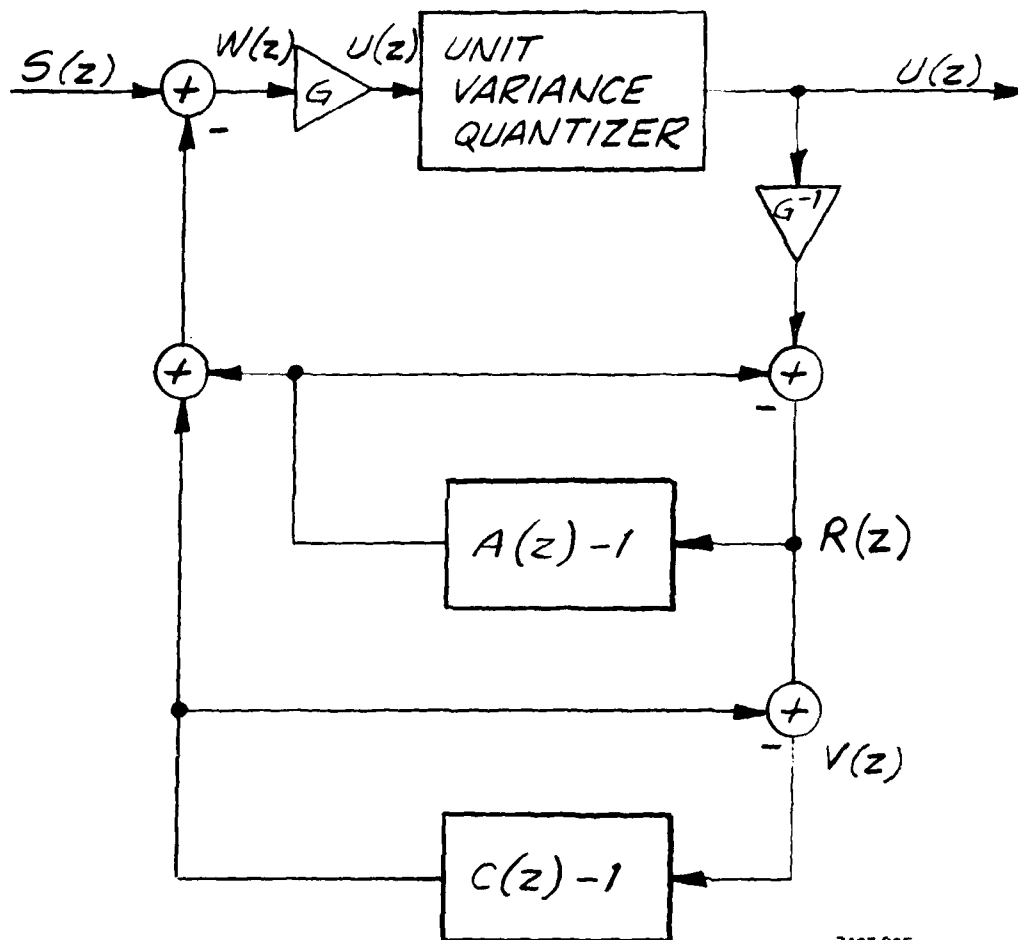
The split-band adaptive predictive coding technique has been proven to be an efficient method for encoding speech signals at 16 Kbps. Though the SBAPC system attempts to minimize the rms value of the error signals in the coded speech, low amplitude quantization error, however, does not always ensure perceptually small distortion in the processed speech. It has been suggested that higher quality speech can be obtained by the adjustment of the noise spectral shape without changing the rms value of the error signals. In the next section, two techniques of noise shaping will be considered [11, 12]. The first method, proposed by Makhoul, changes the flat spectrum of the quantization noise to resemble that of the input speech, whereas the second technique, originated by Atal, attempts to flatten the noise spectrum. Though the objective of both techniques is to enhance the quality of the synthesized speech without additional overhead bits; the complexity, stability of the algorithms, and the flexibility of the noise spectral shaping are quite different.

### 2.4.1 Makhoul's Noise Shaping Technique

The transmitter portion of the basic APC system is shown in Figure 2.4.1. In this figure,  $S(z)$  represents the  $z$  transformation of the input speech  $s_n$ ,  $n=1, \dots, L$  where  $L$  is the number of samples in one frame interval.  $C(z)$  represents the transfer function of the pitch prediction loop which is given by:

$$C(z) = 1 - \alpha z^{-M} \quad (2-46)$$

where  $M$  is the number of speech samples in one pitch period and  $\alpha$  is the pitch gain parameter.  $\alpha$  is computed in order to minimize the total



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FIGURE 2.4.1 BLOCK DIAGRAM OF APC SYSTEM

$$\text{squared error } E = \sum_{n=1}^L (S_n - S_{n-M})^2 \quad (2-47)$$

and it can be expressed as:

$$\alpha = \frac{\sum_{n=1}^L S_n S_{n-M}}{\sum_{n=1}^L S_{n-M}^2} \quad (2-48)$$

The transfer function of the short-term prediction can be written as:

$$A(z) = 1 + \sum_{k=1}^P a_k z^{-k} \quad (2-49)$$

where  $\{a_k\}$ 's are the linear prediction coefficients.  $\hat{W}(z)$  represents the z transform of the APC residual signal which includes the effects of the quantization noise  $Q(z)$ ; i.e.,

$$Q(z) = \hat{W}(z) - W(z) \quad (2-50)$$

where  $W(z)$  is the z transform of the APC residual signal only.  $U(z)$  is the residual error signal with unit variance and can be written as:

$$U(z) = G W(z) \quad (2-51)$$

where  $G$  is a normalization gain factor. The spectrum of  $W(z)$  is assumed to be flat which is a reasonable assumption, since the residual error appears to be highly uncorrelated. Thus, the input of the quantizer is assumed to be white and has unit variance. At the receiver,  $U(z)$ , after multiplying  $G^{-1}$ , is sent through the all-pole linear prediction filter  $1/A(z)$ , and the pitch prediction filter  $1/C(z)$ . The output signal at the re-

ceiver is exactly equal to the signal  $V(z)$  for voiced speech or  $R(z)$  for unvoiced speech, provided the digital data transmission is error-free.

The main idea in noise shaping is to employ a linear filter and modify the quantization noise according to a pre-determined perceptual criterion. For simplicity reasons, the analysis will be conducted without the pitch loop. In this manner, the reconstructed signal  $R(Z)$  is given by:

$$R(Z) = S(Z) + B(Z)Q(Z) \quad (2-52)$$

where  $B(Z)$  is the  $z$ -transform of the shaping filter. Since  $R(Z)$ , as shown in Figure 2.4.1, is also equal to:

$$R(Z) = \frac{\hat{W}(Z)}{A(Z)} = (W(Z) + Q(Z))/A(Z) \quad (2-53)$$

Equating Eq. (2-53) with (2-52), the result becomes:

$$W(Z) = A(Z)S(Z) + [A(Z)B(Z) - 1]Q(Z) \quad (2-54)$$

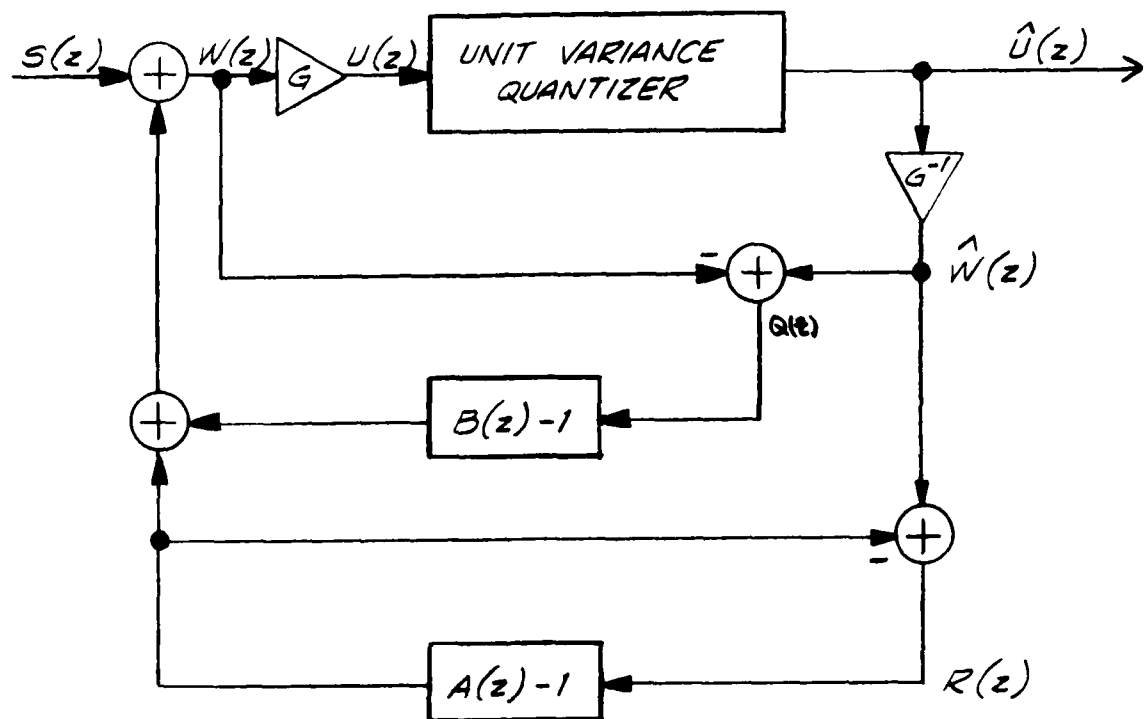
Adding and subtracting  $S(Z) + B(Z)Q(Z)$ , Eq. (2-54), can be rewritten as:

$$W(Z) = S(Z) + (B(Z) - 1)Q(Z) + (A(Z) - 1)(S(Z) + B(Z)Q(Z)) \quad (2-55)$$

Substituting Eqs. (2-52) and (2-53) into (2-55), the following is obtained:

$$W(Z) = S(Z) + (B(Z) - 1)Q(Z) + (A(Z) - 1)(W(Z)/A(Z)) \quad (2-56)$$

The noise shaping algorithm, as illustrated in Eq. (2-56) is depicted in Figure 2.4.2.



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FIGURE 2.4.2 BLOCK DIAGRAM OF THE APC SYSTEM WITH NOISE SHAPING

In this study, the simple and stable second order all-zero filter is employed as  $B(Z)$ . Its transfer function, given as  $B(Z) = \sum_{i=0}^2 b_i z^{-i}$ , is estimated from the original transfer function of the predictor coefficients  $A(Z)$  as follows:

$$\rho_i = \sum_{k=0}^{P-|i|} a(k) a(k + |i|) \quad 0 \leq i \leq 2 \quad (2-57)$$

where  $P$  is the order of the filter  $A(Z)$ . The coefficients  $b_n$  are computed from the set of linear normal equations:

$$\sum_{n=1}^2 b_n \rho_{i-n} = -\rho_i \quad 1 \leq i \leq 2 \quad (2-58)$$

and this results in:

$$\begin{aligned} b_0 &= 1 \\ b_1 &= \rho_1(\rho_2 - \rho_0)/(\rho_0^2 - \rho_1^2) \\ b_2 &= (\rho_1^2 - \rho_0\rho_2)/(\rho_0^2 - \rho_1^2) \end{aligned} \quad (2-59)$$

To study the effect of noise shaping on the SBAPC system, the 2nd order all-zero filter, as given in Eq. (2-59), has been incorporated. In particular, the performance of the combined system at the data rate 8 Kbps (quantization of error signal only, excluding side information) has been investigated. The results in terms of S/Q are tabulated in Table 2.4 for the SBAPC system with and without noise shaping on each band. As it is noted in Table 2.4, maximum signal-to-quantization noise ratio is achieved with the absence of noise shaping on both bands, but the output speech obtained without noise shaping exhibits a rough quality together with some disturbing



noise shaping	number of pitch predictor 1	number of pitch predictor 3
lowband: yes highband: yes	14.38 dB	15.55 dB
lowband: yes highband: no	14.43 dB	15.59 dB
lowband: no highband: no	15.43 dB	16.84 dB

Table 2.4 SIGNAL TO NOISE RATIO OF SBAPC  
SYSTEM WITH MAKHOUL'S NOISE  
SHAPING AT 8 KBPS

background noise. However, these noises disappear when noise shaping is applied. Informal listening tests further suggest that noise shaping in the high band does not enhance the subjective speech quality for male speakers. However, more careful listening tests reveal that the "beeping" noise which occurs frequently with female speakers at low data rates (e.g., 8 Kb/s) is reduced when noise shaping is applied to both high and low bands. For higher data rate systems (>16 Kb/s), noise shaping is not really helpful.

#### 2.4.2 Atal's Noise Shaping Technique

The block diagram of a generalized adaptive predictive coder with adjustable noise spectrum is shown in Figure 2.4.3. In this figure, the speech samples  $\{s_n\}$  pass through the inverse linear prediction filter,  $1 - A(z)$ , where

$$A(z) = \sum_{k=1}^m a_k z^{-k} \quad (2-60)$$

and  $m$  is the order of the filter and  $\{a_k\}$ 's are the linear prediction filter coefficients. The output of the filter may be expressed as

$$d_n = s_n - \sum_{k=1}^m a_k s_{n-k} \quad (2-61)$$

Then  $d_n$  is fed into the quantizer loop. For the sake of simplicity, the pitch loop is ignored. Then, the quantizer noise  $\delta_n$  defined as the difference between the quantizer output  $\hat{q}_n$  and the quantizer input  $q_n$  may be expressed as

$$\delta_n = \hat{q}_n - q_n \quad (2-62)$$



The quantizer noise  $\delta_n$  is fed into the noise shaping filter  $F(z)$ , and the output of this filter  $f_n$  is subtracted from  $d_n$  to yield the quantization noise as:

$$\begin{aligned} q_n &= d_n - f_n \\ &= s_n - \sum_{k=1}^m a_k s_{n-k} - \sum_{k=1}^{m'} b_k \delta_{n-k} \end{aligned} \quad (2-63)$$

where  $m'$  is the order of the feedback loop noise shaping filter and  $\{b_k\}$ 's are the coefficients of the filter  $F(z)$  defined as:

$$F(z) = \sum_{k=1}^{m'} b_k z^{-k} \quad (2-64)$$

The output of the predictive coder can now be expressed as:

$$\begin{aligned} \hat{s}_n &= \hat{q}_n + \xi_n \\ &= \hat{q}_n + \sum_{k=1}^m a_k \hat{s}_{n-k} \\ &= q_n + \delta_n + \sum_{k=1}^m a_k \hat{s}_{n-k} \\ &= s_n + \sum_{k=1}^m a_k (\hat{s}_{n-k} - s_{n-k}) + \delta_n - \sum_{k=1}^{m'} b_k \delta_{n-k} \end{aligned} \quad (2-65)$$

Taking the  $z$  transformation of this equation yields

$$\hat{S}(z) - S(z) = \Delta(z) \frac{1 - F(z)}{1 - A(z)} \quad (2-66)$$

where  $\Delta(z)$ ,  $\hat{S}(z)$ ,  $S(z)$  represent the  $z$  transform of  $\delta_n$ ,  $\hat{s}_n$ , and  $s_n$ , respectively. The total processing noise will be the same as the quantizer noise  $\Delta(z)$ , if  $F(z)$  equals  $A(z)$ . In other words, the spectrum of the output noise can be controlled with great flexibility with the feedback filter  $F(z)$ . Assuming that the power of the quantizer noise  $\delta_n$  does not vary significantly by the feedback loop  $F(z)$ , the average value of the power spectrum of the output noise is determined only by the quantizer and is not altered by the choice of  $F(z)$  or  $A(z)$ . However, the filter,  $F(z)$ , distributes the noise power from one frequency to another. Thus, reduction of quantizer noise at one frequency can be obtained at the expense of increasing the quantizer noise of another one. Since a large part of the perceived noise in a coder comes from the frequency regions where the signal is low, the filter  $F(z)$  may be used to reduce the noise in such regions while increasing the noise in the formant regions where the noise could be effectively masked by the speech signal. It is also assumed that the quantizer noise is uncorrelated with the prediction error signal, which is a reasonable assumption, particularly when the prediction error signal is white. Then the power of the quantizer may be expressed as

$$E_q = E_p + E_f \quad (2-67)$$

where  $E_p$  is the power of the prediction error signal and  $E_f$  is the power of the filtered quantized noise. In many cases, it is desirable to have a small  $E_f$  to ensure the small changes of the quantized noise. Atal suggested that the APC system of Figure 2.4.3 can be operated in stable condition by adding a high passed filtered noise to the input speech. Consequently, the terms in the covariance matrix and the correlation vector have to be modified as:

$$\hat{\gamma}_{ij} = \gamma_{ij} + \lambda E_{\min} \mu_{i-j} \quad (2-68)$$

and

$$\hat{c}_i = c_i + \lambda E_{\min} \mu_i \quad (2-69)$$

where

$$\gamma_{ij} = \langle s_{n-i} s_{n-j} \rangle \quad (2-70)$$

$$c_i = \langle s_n s_{n-i} \rangle \quad (2-71)$$

The  $\lambda$  in eq. (2-68) is a small constant in the range 0.01-0.1,  $E_{\min}$  is the minimum value of the mean squared prediction error,  $\mu_i$  is the autocorrelation of the high-pass filtered white noise at a delay of  $i$  samples, and  $\langle \cdot \rangle$  denotes time averaging. In this study,  $\mu_i$ 's are chosen to be  $\mu_0 = 3/8$ ,  $\mu_1 = 1/4$ ,  $\mu_2 = 1/16$ ,  $\mu_k = 0$  for  $k \geq 3$ . With the addition of the high passed filtered noise, the stability of the feedback loop filter is increased.

The quantizer input  $\{q_n\}$  in Figure 2.4.3 sometimes contain large amplitudes especially for periodic signals in voiced speech. However, the large amplitudes can be removed by pitch prediction. The transfer function of this pitch loop may be expressed as:

$$P_d(z) = \beta_1 z^{-M+1} + \beta_2 z^{-M} + \beta_3 z^{-M-1} \quad (2-72)$$

where  $M$  represents the number of samples in one pitch period and  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$  are the filter coefficients in the pitchfilter. The values of  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$

may be obtained from the set of simultaneous linear equations, which is described in section 2.3.2.

The addition of the high pass filtered noise to the speech input increases the stability of the quantization feedback loop. A simple and effective solution to ensure the stability of the feedback loop is to limit the peak amplitude of the sample  $f_n$  as shown in Figure 2.4.3. The appropriate peak limiter in the feedback loop limits the samples  $\{f_n\}$  to a maximum value of twice the rms value of the prediction error. For some choices of  $F(z)$ , several instances of instability in the feedback loop have been encountered without peak limiter. However, the inclusion of the peak limiter in the feedback loop removes instability in those frames, and it does not increase the quantization noise significantly. Atal suggested that the feedback loop filter shown as

$$F(z) = A(\alpha z^{-1}), \quad 0 \leq \alpha \leq 1 \quad (2-73)$$

is a good choice because of the simplicity and flexibility of controlling the spectral shape of the quantization noise.

The above noise shaping method was applied to the SBAPC algorithm. Several choices of the feedback loop filter  $F(z)$  were considered in each band and their S/Q's are tabulated in Table 2.5. For  $\alpha_l = \alpha_h = 0$  (or  $F(z) = 0$  in both low and high bands), the quantization noise has the same spectral envelope as the original speech as illustrated in the spectral plot of 1 frame of data in Figure 2.4.4. This particular choice of  $\alpha$ 's leads to a noisy output of 11.61 dB S/Q at 8 Kb/s (excluding side information). As the value of  $\alpha$  increases, the performance of the SBAPC scheme in terms of S/Q improves. The ratio tends to reach the maximum

$\alpha$ in in $\alpha$ in LB HB	0.0	0.25	0.5	0.75	1.0
0.0	11.61 dB	11.66	11.69	11.73	11.77
0.4	13.04	13.09	13.12	13.17	13.22
0.5	14.33	14.39	14.44	14.49	14.55
0.75	15.82	15.91	15.95	16.05	16.12
1.0	15.56	15.65	15.70	15.81	15.88

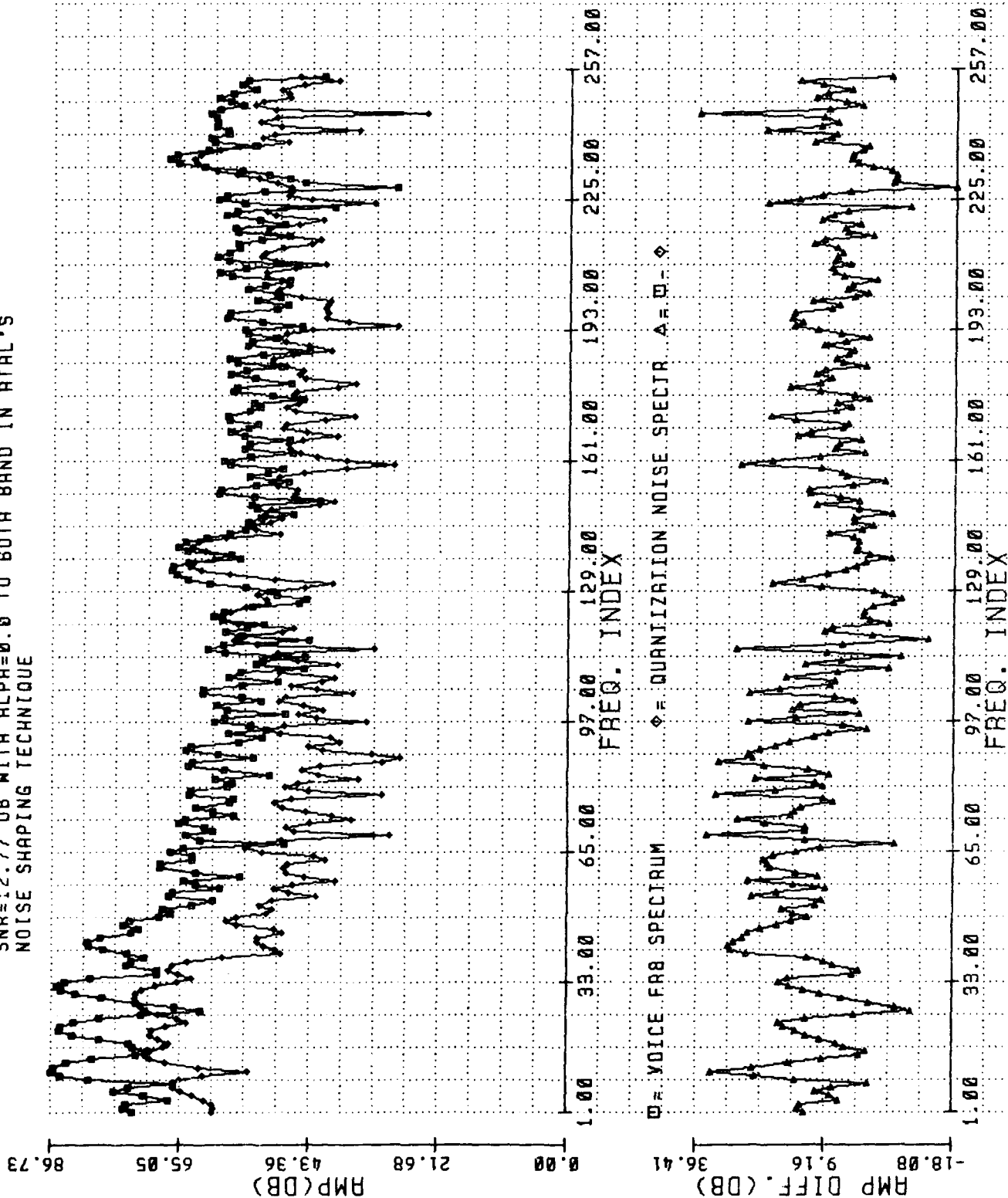
HB: Highband

LB: Lowband

Table 2.5 The Signal-to-Quantization Noise Ratio in dB  
of the SBAPC System with Atal's Noise Shaping  
at 8 KBPS.



Figure 2.4.4 SPECTRUM PLOT OF THE SBAPC SYSTEM WITH TIME DOMAIN  
SNR=12.77 DB WITH  $\alpha=0.0$  TO BOTH BAND IN ATAL'S  
NOISE SHAPING TECHNIQUE

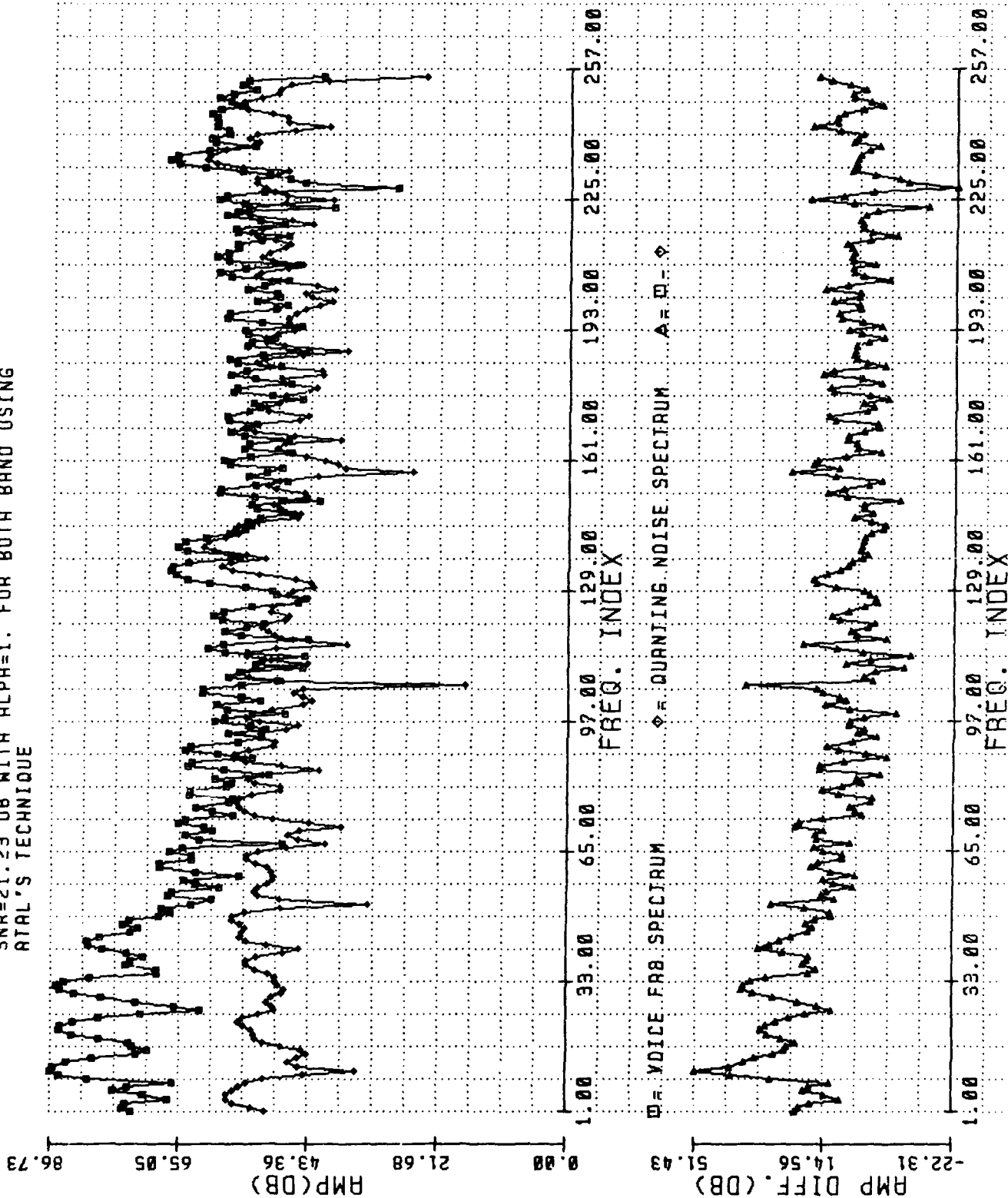


for  $\alpha_l = 0.75$ ,  $\alpha_h = 1.0$ . For  $\alpha_l = \alpha_h = 1$ , the system is similar to Makhoul's model shown in Figure 2.4.2 without noise shaping. In this case, the spectrum of the output noise is almost uniform as shown in Figure 2.4.5 and the S/Q is high (15.88 dB). The power of the quantization noise is small, but the reconstructed speech contains much wideband noise. For  $\alpha_l = \alpha_h = 0.75$ , the power of the quantization noise is small, and informal subjective listening tests indicate that the choice of  $\alpha_l = \alpha_h = 0.75$  leads to the highest quality of synthesized speech. It is, therefore, concluded that noise shaping actually enhances the synthesized speech quality of the SBAPC system.

#### 2.4.3 Comparison of Atal's and Makhoul's Noise Shaping Methods

The shaping of quantization noise has been applied to the SBAPC system in order to enhance the quality of synthesized speech at low data rates. Makhoul's technique and Atal's technique have been incorporated in the SBAPC system at the data rate 8 Kbps (quantization of error signal only, excluding side information) in order to determine the effects of noise shaping clearly. The second order all-zero filter proposed by Makhoul has been applied to various input speech signals. The performance of this scheme is tabulated in Table 2.4 in terms of the signal to noise ratio with male input speech. Informal listening tests suggest that noise shaping in the high band does not enhance the subjective speech quality for male speakers. Atal's noise shaping technique has also been applied to the SBAPC system. The system performance is tabulated in Table 2.5 with the parameter  $\alpha$  which controls the bandwidth of the noise feedback loop. Informal listening tests suggest that the choice of  $\alpha \approx 0.75$  in lowband and highband provides the best subjective speech quality.

Figure 2.4.5 SPECTRUM PLOT OF THE SBAPC SYSTEM WITH TIME DOMAIN  
 SNR=21.23 DB WITH ALPHA=1. FOR BOTH BAND USING  
 ATAL'S TECHNIQUE



Both Atal's technique and Makhoul's technique improve the subjective speech quality at the data rates below 12 Kbps. The technique of Makhoul attempts to change the flat spectral shape of the noise toward the spectral shape of input speech while the technique of Atal attempts to change the spectrum of the noise (same shape as input speech) toward the flat spectrum. The goal of both techniques is the same, but the complexity and stability of the SBAPC system and the flexibility of the noise spectral shapes are different. For the purpose of comparison, a typical performance of the SBAPC system using both techniques is tabulated in Table 2.6. Though the signal to quantization noise ratios are approximately equal, the subjective speech quality differs. Informal listening tests suggest that Makhoul's technique provides a slightly better speech quality as compared to that of the Atal technique.

The speech quality of the SBAPC system is quite natural at the data rate 16 KBPS. However, careful informal listening tests indicate that "beeps" are sometimes heard, especially at the low data rates. In general, "beeps" occur more often in female speech than in male speech. Experiments have been conducted to identify the source of the "beeps," and we conclude that it is caused by the coarse quantization of error signal in the highband, since the "beeps" disappear when the signals of the highband are not quantized. This is no easy way to reduce these "beeps." The only alternative is to mask the "beeps" by employing noise shaping at the high band and by inserting a small level random noise at the synthesizer. The random noise is added only when the number of bits allocated to the high band is small ( $\leq 1$ ). Unfortunately, the amplitude of the random noise has to be adjusted so that the output speech will not be too noisy.

	First order pitch prediction	Third order pitch prediction
Makhoul's technique	17.87 dB	18.94 dB
Atals technique	18.04 dB	18.70 dB

TABLE 2.6: COMPARISON OF SBAPC SYSTEMS WITH TWO  
DIFFERENT NOISE SHAPING TECHNIQUES

## 2.5 Quantization of Residual Signals

### 2.5.1 Adaptive Bit Allocations

One of the advantages of SBAPC algorithms is the possibility of using spectral densities of the subband signals and applying nonuniform quantization to each band. The conventional approach is to use a fixed bit allocation rule where a pre-determined number of bits is assigned to the coding of each band. In particular, a larger portion of the available bits will be allocated for the quantization of the low band in order to capture all pitch and formant information, whereas a smaller portion of the bits will be utilized for the high band. However, since the ratio of low band and high band energies fluctuates from frame to frame, fixed bit allocation may not necessarily be the best strategy. Instead, an adaptive bit allocation scheme that dynamically alters the bit assignments depending on the energies of the two bands seems more applicable.

It has been shown that the most dominant source of speech distortion in the SBAPC system is the quantization of residual waveforms in the prediction loops. To illustrate the effects of quantization errors, the S/Q of the SBAPC system are plotted in Figure 2.5.1 with or without applying quantization to low band and high band error signals. In this figure, the plot of ( $\square$ ) indicates that the quantization is not applied to the low band error signal, and the error signal in the high band is quantized with 2 bits per sample. The plot of ( $\diamond$ ) indicates that the quantization is not applied to the high band error signals and the error signals of low band are quantized with 3 bits per sample. In this figure, the SBAPC system performs poorly in regions I1, I2, and I3 as compared to that of ( $\diamond$ ).

THE PERFORMANCE CURVES OF SBAPC WITH  
4-TH ORDER PREDICTORS IN EACH BAND  
V2P14(ND CODING ON LOW BAND), V2P41(ND CODING ON HIGH BAND)

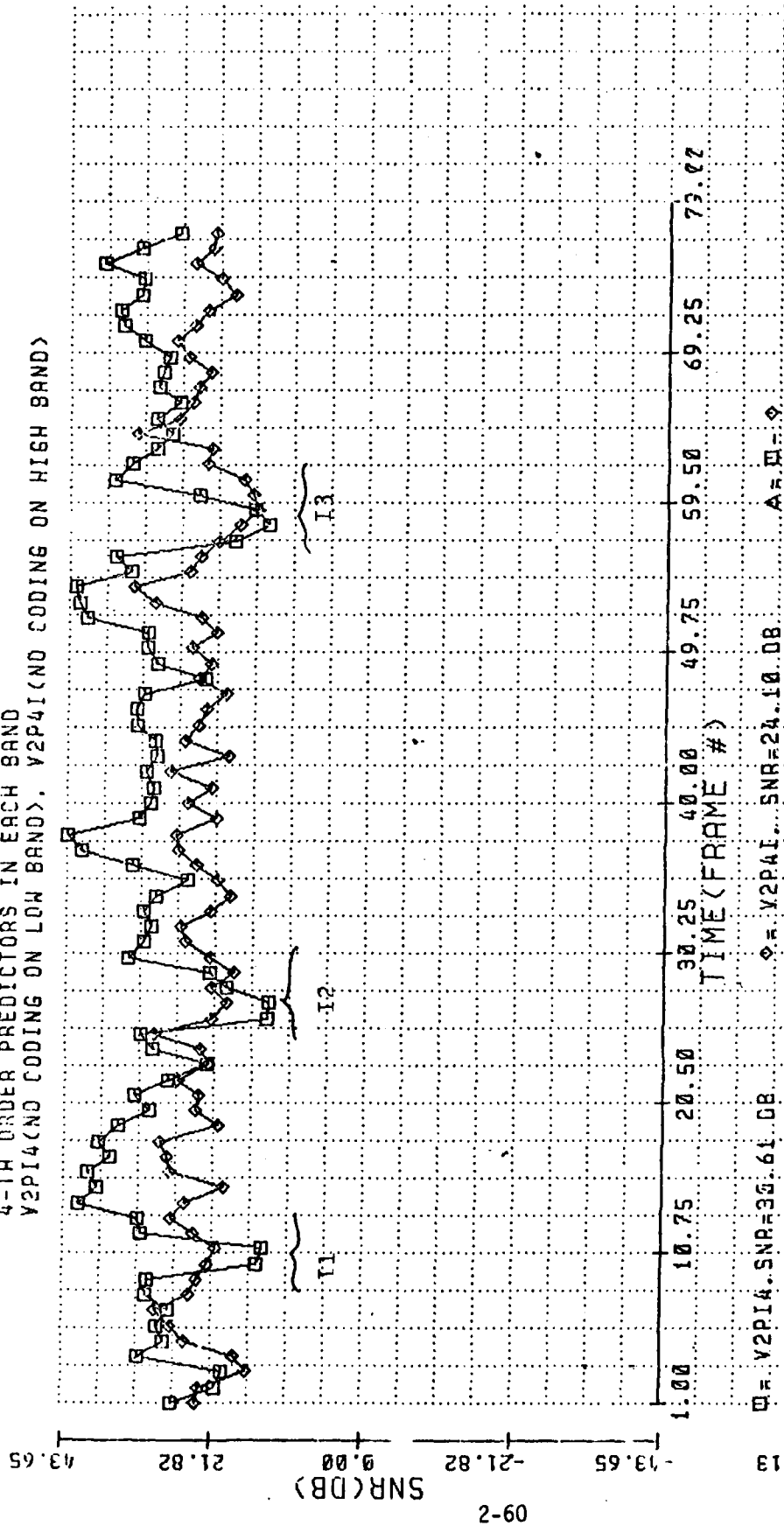


Figure 2.5.1 The Performance Curves of a SBAPC System with or without Quantization of Error Signals

It is, therefore, suggested that more bits may be allocated for the high band error signals in regions I1, I2, and I3 in order to improve the performance with fixed transmission data rate.

The performance of the SBAPC system with or without adaptive bits allocations is then compared and the results are shown in Table 2.7. The SBAPC system works better when the bits employed to quantize the low band and high bands are adaptively allocated according to the energy of each band. The adaptive bit allocations yield an increase of 1 dB in signal-to-quantization noise ratio over the scheme with fixed bit allocations. Since the energies of both bands have to be sent to the receiver, adaptive bit allocations do not require additional overhead bits. However, an additional bit assignment rule may be required in order to avoid the difficulties of encoding signals with non-integer number of bits per sample.

Let  $R_i$  be the actual number of bits allocated to the  $i$ -th subband, then the average number of bits per band,  $\bar{R}$ , may be expressed as

$$\bar{R} = \frac{1}{2} \sum_{i=1}^2 R_i \quad (2-74)$$

Let  $\sigma_i^2$  be the energy of the  $i$ -th band, then it can be shown that the optimum bit allocation can be obtained (in the sense of minimizing the rms error of the coded speech) as

$$R_i = \bar{R} + \frac{1}{2} \log_2 \frac{\sigma_i^2}{\sqrt{(\sigma_1^2 \sigma_2^2)}} ; \quad i = 1, 2 \quad (2-75)$$

Hence, bits to encode the error signal of each band can be adaptively allocated according to the energy of each band.



LB Order \ HB Order	2	4	6
4	22.25 dB	22.59	22.66
	23.28 *	23.00 *	24.11 *
6	22.49	22.86	22.94
	23.66 *	24.07 *	24.23 *
8	22.81	23.19	23.26
	23.64 *	24.24 *	24.25 *

\* with adaptive bit allocations

Table 2.7 Signal-to-Quantization Noise Ratio of the two-loop  
SBAPC System with ~~and without~~ adaptive bit allocations  
at 16 Kbps

The SBAPC performs better when the bits used to quantize the low band and high band error signals are adaptively allocated according to the energy of each band as shown in Figure 2.5.2. The adaptive bit allocations offer an inverse of 1-2 dB in S/Q over that of a scheme with fixed bit allocations. Only assignments of integer bits per sample are utilized in order to simplify the algorithm. Since the energies of both bands have to be sent to the receiver for quantization purposes, adaptive bit allocations do not require additional transmission of data.

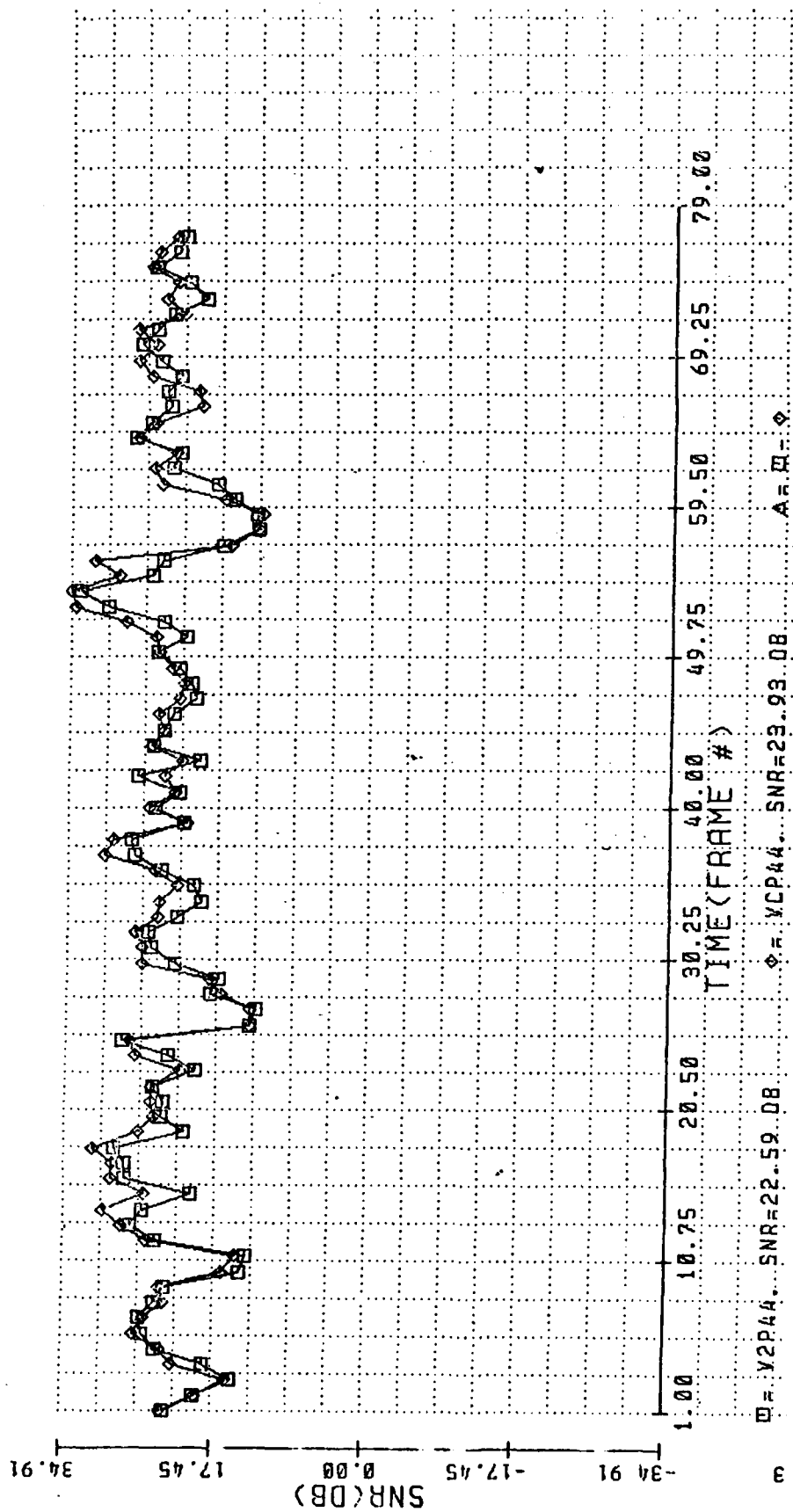


FIGURE 2.5.2 THE PERFORMANCE PLOTS OF 16 KBPS SBAPC SYSTEMS WITH  
FIXED AND ADAPTIVE BIT ALLOCATIONS

### 2.5.2 Quantization of Residual Signals

In APC systems, it is well known that the design of residual signal quantizers will significantly affect the voice quality of the processed speech. The SBAPC algorithm, which is very similar to the APC, is of no exception and fine quantization on both high and low band residual signals are vital to its success. In light of the fact that the adaptive bit allocation scheme as discussed in Section 2.5.1 only results in integer bit assignments, the emphasis of this study has been on the designs of integer bits quantizers (e.g., 2-level, 4-level, 8-level). More specifically, the quantizers which can adapt to the changing variance of its input by changing its step sizes has been investigated.

In general, two distinct classes of these quantizers exist; those that change their step size based on the transmitted value of the error signal and those that change their step size based on the variance of the unquantized error signal. The first form is known as "backward" quantizers since they look backward over previously quantized error samples to adjust their step size. The second form is labeled as "forward" quantizers because they look forward over the unquantized error sample to obtain their step size [13]. The backward quantizers need not send the quantizer step size to the receiver because the receiver can regenerate this value by looking at the transmitted sequence representing the quantized error waveform. This is not true of the forward quantizers. Here, since the step size is based on the value of the unquantized error signal, the receiver cannot regenerate it from the transmitted sequence. Thus, forward quantizers transmit the value of the quantizer to the receiver. Consequently, coders having forward quantizers require more bits than those having backward quantizers. For the SBAPC system, only the forward quantizers have

been investigated. One of the reasons is that during the course of the channel error study, the SBAPC algorithm has been found to be extremely sensitive to errors. Since the backward quantizer is known to be more susceptible to errors as compared to the forward one, only the latter is considered [7].

In the SBAPC algorithm, the error waveform obtained after the pitch and predictor loops still has some sample-to-sample correlations. In particular, the error signal exhibits a large concentration of energy around the pitch pulses. If this pitch information can be finely quantized, the processed speech quality will be improved. One such example is the pitch-compensating quantizer [14] where two additional quantizer levels are especially designed to code large pitch pulses. Since the occurrence of pitch does not happen that often, a variable coding scheme has to be utilized to reduce the total bit rate and this complicates the entire coding process.

An alternative approach is to use a segmental quantization scheme which applies different quantization to various regions of the frame [15]. Partitioning the entire frame into a pre-determined number of sub-intervals, bit allocations can be computed adaptively according to the energies of these sub-regions in the same manner as dictated in Eq. (2-75). An 8-segment quantizer has been implemented in the SBAPC algorithm, and the results indicate that the segmental quantizer offers an advantage of 1 to 1.5 dB over that of the conventional quantizers. However, when bits needed to transmit the energies of the sub-levels are included in the algorithm (that is, less bits are utilized to quantize the residual signals), the improvement becomes minimal. In practice, the only situation that the segmental quantizer can offer any advantage is that it works

pitch synchronously. In other words, more bits are utilized to quantize the larger pitch spikes especially during the onset of a pitch period. Unfortunately, there is no straightforward way to formulate such a pitch synchronous scheme owing to the fact that the pitch period is not always divisible by the number of sub-intervals. Consequently, the speech samples within a sub-interval cannot be guaranteed an integer making the transmission of a fixed number of bits per frame impossible.

In light of the fact that segmental quantizers do not offer any real-advantage, conventional quantizers based on the statistics of the input signals are considered. The performance between the Gaussian [16] and the Laplacian [9] quantizers have been compared. As it turns out, the Gaussian quantizer consistently yields lower signal-to-quantization noise as compared to the Laplacian ones. This indicates that the SBAPC residual signals have a distribution which closely resembles a Laplacian one.

To further improve the SBAPC performance, quantizers have been derived from the actual distributions of the normalized low and high band error signals. Figures 2.5.3 and 2.5.4 depict one half of distribution of the low band, high band residual signal, respectively. From these figures, the actual distributions resemble the Laplacian more than the Gaussian ones. Also, the low band distribution seems to have a larger spread as compared to the high band one. Based on these distributions, the 1-bit, 2-bit, and 3-bit quantizers for the two bands have been obtained. When incorporated in the SBAPC algorithm, the new quantizers gain 0.25 dB S/Q. Also, informal listening tests indicate the new quantizers yield a "smoother" processed speech quality.

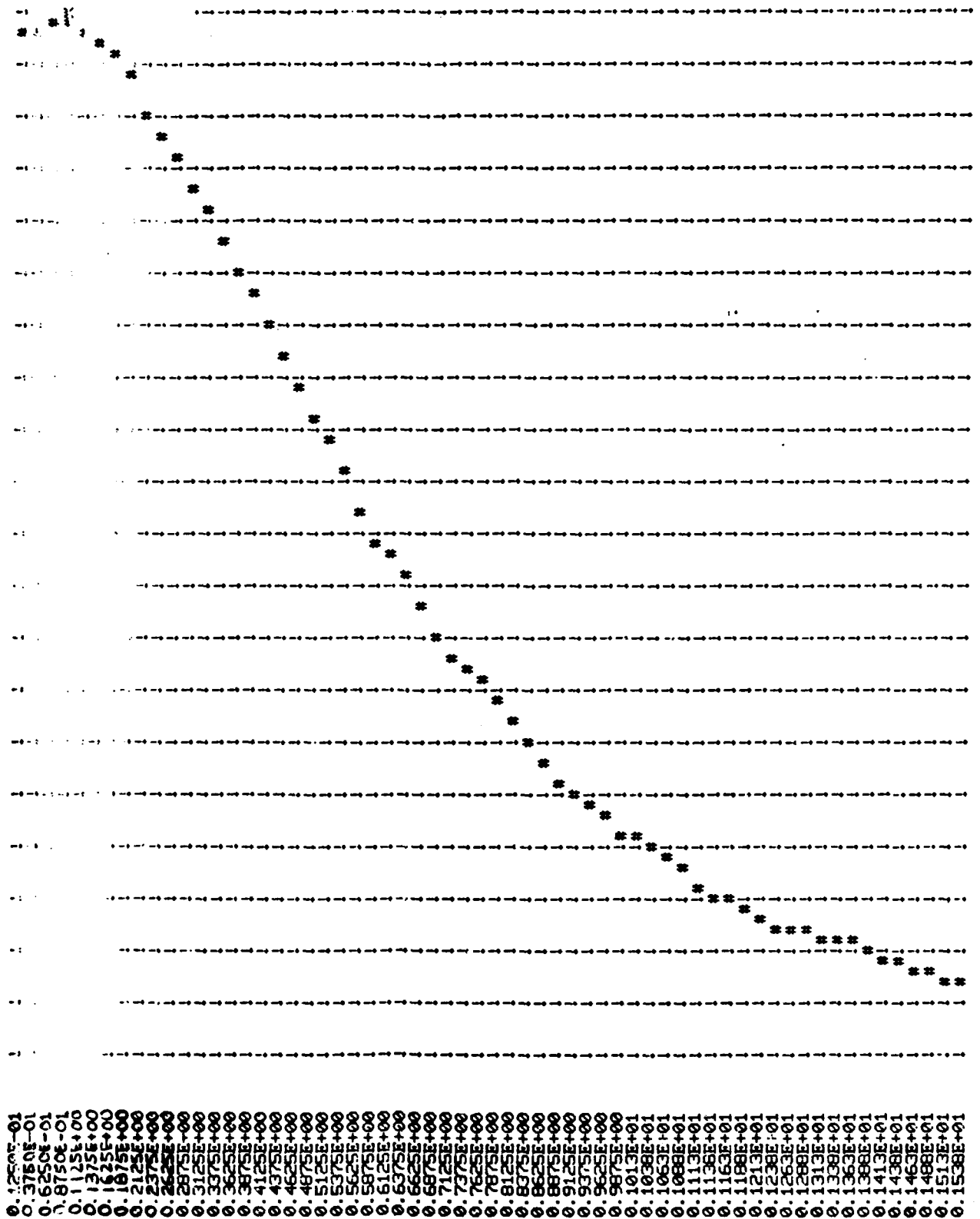


FIGURE 2.5.3: DISTRIBUTION OF THE LOW BAND RESIDUAL SIGNAL

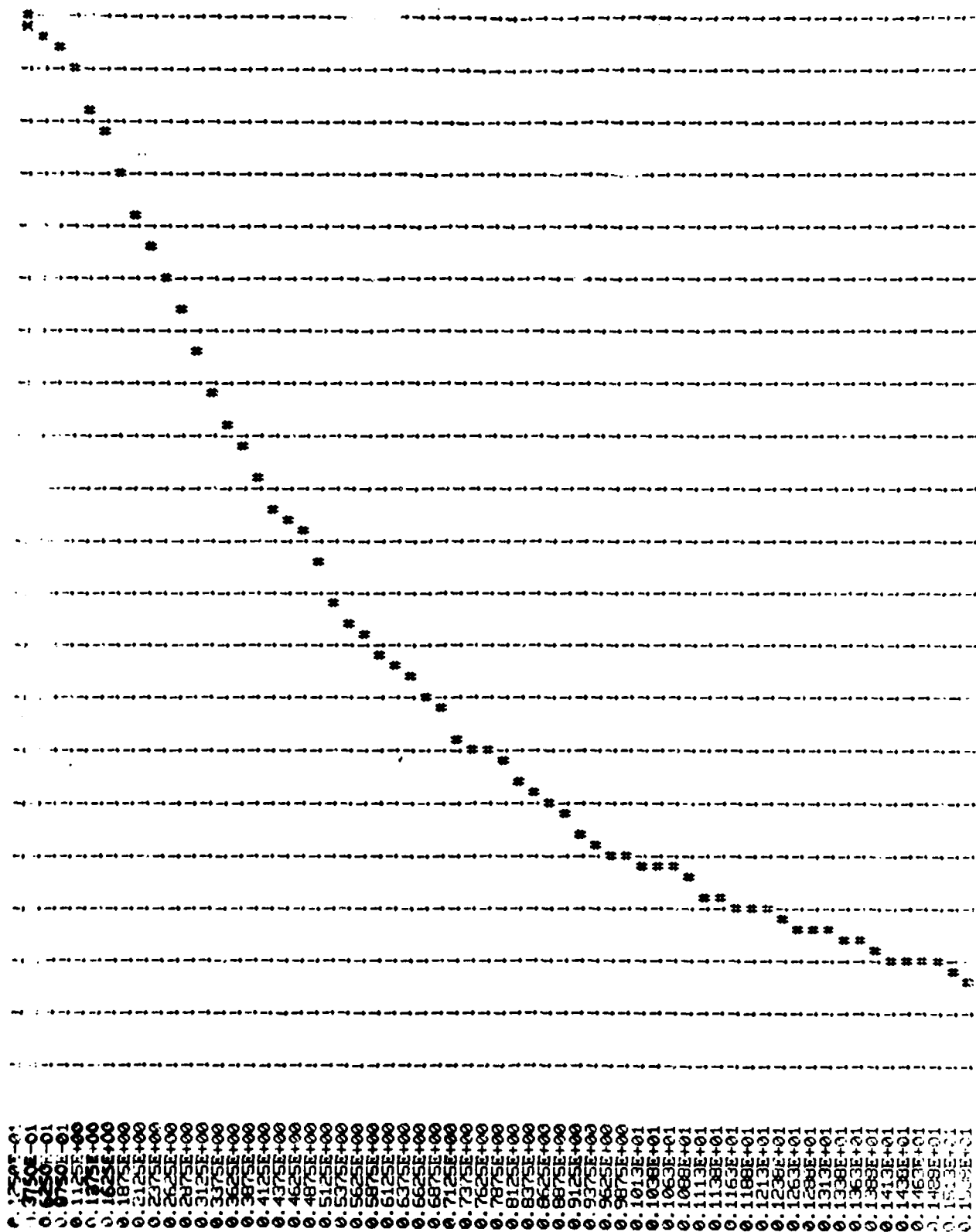


FIGURE 2.5.4: DISTRIBUTION OF THE HIGH BAND RESIDUAL SIGNAL



### Section III

#### PERFORMANCE UNDER CHANNEL IMPAIRMENTS

##### 3.1 The Effect of Background Noise on the SBAPC

It is well known that speech processing algorithms may produce high quality outputs with clean input speech materials, yet in many practical situations where the incoming signals are contaminated with acoustically coupled background noise, the quality of the speech processed through these algorithms can vary from slightly degraded to totally unintelligible. In this study, the effects of three types of background noises, namely, the office noise, the helicopter noise, and the P3C aircraft noise on the SPABC system have been investigated.

It has been shown in Section II that the SBAPC system yields high quality outputs at 16 Kb/s with *uncorrupted spoken materials*. Moreover, our result also indicates that the algorithm produces intelligible speech with noise coupled inputs even in high noise environments ( $S/N = -6$  dB). In the first part of this study, the original SBAPC algorithm is utilized to process the speech material supplied by DCA which contains standard sentences recorded in a low-level office environment ( $S/N = 90$  dB). Informal listening tests show that the quality of the processed sentences is the same as that of clean inputs. As a matter of fact, quantization noise of the SBAPC tends to mask out the background office noise yielding smooth quality speech. This indicates that the SBAPC scheme can indeed function in an office environment and can be employed in the Executive Secure Voice Network (ESVN). The second part of the study deals with the utility of the SBAPC technique in a tactical surrounding simulated using helicopter noise and P3C aircraft noise. In both situations,

the SBAPC yields highly intelligible speech even when the signal-to-noise ratios are as low as -6 dB. The periodic helicopter noise or the broad band P3C aircraft noise does not seem to have detrimental effects in the pitch extraction or the computation of predictor coefficients which render the processed speech unintelligible. However, the output material becomes extremely annoying to listen to especially for the high noise cases. So, for tactical situations, the algorithm has to be modified to include noise reduction techniques. Part 3 of this noise study deals with the design of a pre-processing scheme which is capable of suppressing the level of the background noise before inputting to the SBAPC algorithm.

#### 3.1.1 Reduction of the Background Noise

In general, there are two types of methods that attempt to reduce the noise components from the corrupted speech signals. The first noise suppression scheme, generally known as the 2-microphone technique, employs a second microphone, which is far away from the speech source thus providing information about background noise alone [17]. It is then subtracted from the noisy input speech. This technique is effective for extremely high-noise environments (below 0 dB signal-to-noise ratio) and for non-stationary noise backgrounds (viz, means and correlation functions change rapidly in time). However, this scheme requires large amounts of computations (for example, the order of the noise cancelling filter is often greater than a thousand) which may be beyond the limits of real-time implementation. The second noise suppression technique [18] - [19], which uses a single microphone, estimates the frequency spectrum of the noise during non-speech activity. Then the noise spec-

trum is subtracted from that of the noisy speech. There are two approaches to suppress the background noise using the 1-microphone technique. The first one, proposed by Boll, attenuates the residual signal by -30 dB after subtraction of the estimated frequency components of the noise. The second procedure suggested by McAuley, reduces the residual signals depending on the frequency domain signal-to-noise ratio. Though the objective of both methods is to remove the stationary noise, the latter technique offers more versatility since the amount of noise reduced is controlled adaptively by a signal-to-noise ratio computed on a frame basis. In the next section, this technique and results of noise suppression by McAuley will be discussed.

### 3.1.2 McAuley's Noise Suppression Technique

Assuming that the noise  $n(t)$  has been added to the speech signal  $s(t)$ , the computed input may be expressed as

$$x(k) = s(k) + n(k), \quad k=0, 1, \dots, M-1 \quad (3-1)$$

where  $M$  is the number of speech samples in a frame period. Taking the DFT of eq. (3-1) yields

$$X(m) = S(m) + N(m), \quad m=0, 1, \dots, M-1 \quad (3-2)$$

where  $X(m)$ ,  $S(m)$ , and  $N(m)$  are the DFT's of  $x(k)$ ,  $s(k)$ , and  $n(k)$ , respectively. Assuming that the noise and speech signal are uncorrelated and they are sample functions of zero-mean Gaussian processes, then the variance of the  $X(m)$  may be expressed as

$$\sigma_X^2(m) = \sigma_S^2(m) + \sigma_N^2(m) \quad (3-3)$$

where  $\sigma_S^2(m)$  and  $\sigma_N^2(m)$  represent the variances of  $S(m)$  and  $N(m)$ , respectively. Since  $X(m)$  is a complex Gaussian process with variance  $\sigma_X^2(m)$ , its real and imaginary parts are Gaussian with variances  $\sigma_X^2(m)/2$ . Therefore, the probability density function of  $X(m)$  may be expressed by the joint probability function:

$$p(X) = \frac{1}{\pi |\sigma_S^2 + \sigma_N^2|} \exp \left[ - \frac{|X|^2}{\sigma_S^2 + \sigma_N^2} \right] \quad (3-4)$$

where the index  $m$  is omitted for simpler notation. The maximum likelihood estimate of  $\sigma_S^2$  is obtained by differentiating  $p(X)$  with respect to  $\sigma_S^2$  and setting the result to zero which yields

$$\hat{\sigma}_S^2 = |X|^2 - \sigma_N^2 \quad (3-5)$$

In order to reduce the distortion due to the phase, the input phase have to be retained, and the estimated spectral component of the signal may be expressed as

$$\begin{aligned} \hat{S}(m) &= \hat{\sigma}_S(m) \frac{X(m)}{|X(m)|} \\ &= \left[ \frac{|X(m)|^2 - \sigma_N^2(m)}{|X(m)|^2} \right]^{1/2} X(m) \end{aligned} \quad (3-6)$$

This is generally known as the method of spectral subtraction. Modifications of this algorithm have been studied extensively by several authors

[18] - [19]. The result of eq. (3-6) has been derived under the assumption that the speech and noise are independent Gaussian random processes.

The second approach is to assume that the speech can be characterized by a deterministic waveform with unknown amplitude and phase. In other words, only  $X(m)$  and  $N(m)$  as given in eq. (3-2) are random variables. Then the mean value of  $X(m)$  is given by

$$\bar{X}(m) = S(m) = A \exp(j\theta) \quad (3-7)$$

where  $A, \theta$  is the amplitude, phase of the speech signal. Since  $N(m)$  is assumed to be zero-mean Gaussian, the probability density function of  $X(m)$  is written as

$$p(X|A, \theta) = \frac{1}{\pi \sigma_N^2} \exp \left[ - \frac{|X|^2 - 2A \operatorname{Re}\{X \exp(-j\theta)\} + A^2}{\sigma_N^2} \right] \quad (3-8)$$

Assuming the phase  $\theta$  is uniformly distributed over  $[0, 2\pi]$ , then the probability density function of  $X$  given  $A$  may be expressed as

$$\begin{aligned} p(X|A) &= \int_0^{2\pi} p(X|A, \theta) p(\theta) d(\theta) \\ &= \frac{1}{\pi \sigma_N^2} \exp \left[ - \frac{|X|^2 + A^2}{\sigma_N^2} \right] \cdot \frac{1}{2\pi} \int_0^{2\pi} \exp \left[ \frac{2A \operatorname{Re}\{X e^{-j\theta}\}}{\sigma_N^2} \right] d\theta \\ &= \frac{1}{\pi \sigma_N^2} \exp \left[ - \frac{|X|^2 + A^2}{\sigma_N^2} \right] I_0 (|2AX/\sigma_N^2|) \end{aligned} \quad (3-9)$$

where  $I_0(\cdot)$  is the zeroth order modified Bessel function of the first kind which is defined as

$$I_0(|X|) = \frac{1}{2\pi} \int_0^{2\pi} \exp[\operatorname{Re}(X e^{-j\theta})] d\theta \quad (3-10)$$

For large values of  $|X| \geq 3$ ,  $I_0(|X|)$  may be approximated by

$$I_0(|X|) \approx \frac{1}{\sqrt{2\pi|X|}} \exp|X| \quad (3-11)$$

In this case, the probability density function can be approximated as

$$p(X|A) \approx \frac{1}{\pi\sigma_N^2} \frac{1}{\sqrt{2\pi} \frac{2A|X|}{\sigma_N^2}} \exp\left[-\frac{|X|^2 - 2A|X| + A^2}{\sigma_N^2}\right] \quad (3-12)$$

The maximum likelihood estimate of the spectral amplitude may be obtained by differentiating eq. (3-12) with respect to  $A$  and by setting the result to zero which yields

$$\hat{A} = \frac{1}{2} \left[ |X| + \sqrt{|X|^2 - \sigma_N^2} \right] \quad (3-13)$$

The maximum likelihood estimate of the spectral component without changing the phase may be expressed as

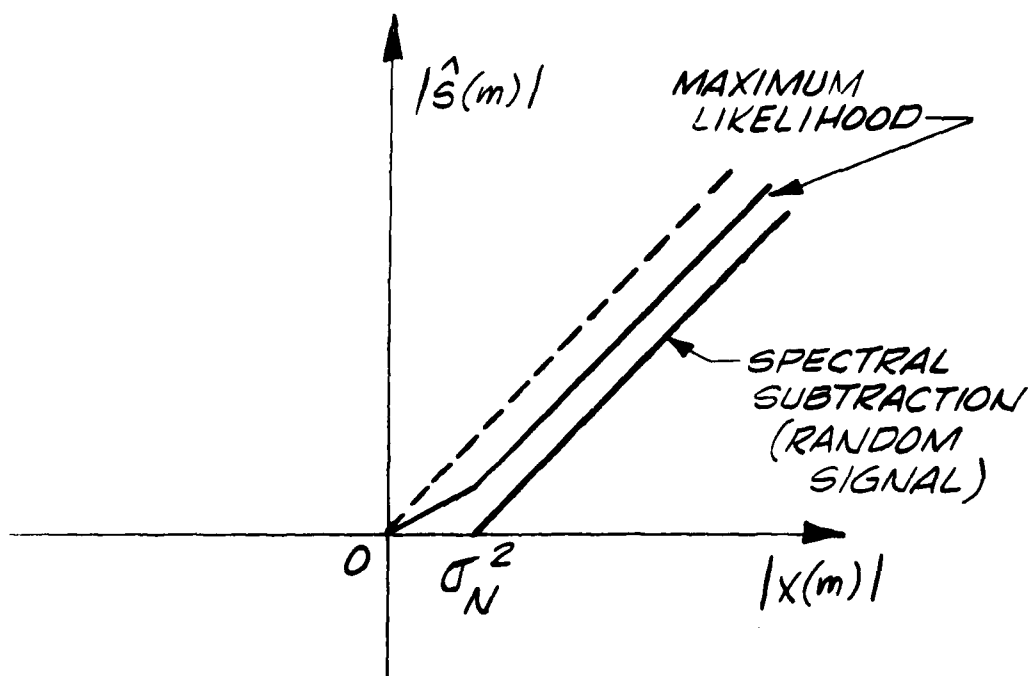
$$\begin{aligned} \hat{S}(m) &= \hat{A} \frac{X(m)}{|X(m)|} \\ &= \frac{1}{2} \left[ 1 + \sqrt{\frac{|X(m)|^2 - \sigma_N^2(m)}{|X(m)|^2}} \right] X(m) \end{aligned} \quad (3-14)$$

In this case, the maximum likelihood estimate is the average of the received spectrum and the estimate spectrum obtained from the method of spectral subtraction. The relations between the received spectral amplitude  $A$  and the estimated amplitude  $|X|$  given in eq. (3-13) are shown in Figure 3.1.1 for the cases of random input signal and deterministic input signal with unknown amplitude and phase. One advantage of the maximum likelihood algorithm is that the speech components at frequencies where the amplitude is small, is still preserved. In contrast, these components are removed completely in spectral subtraction technique which may degrade the quality of the speech or may decrease the intelligibility of speech.

However, the maximum likelihood algorithm does not adequately suppress the background noise in the absence of speech since the suppression rules are derived under the assumption that the speech signals are always present in the measured data. So a noise detector has to be developed in order to derive a better suppression rule that can be applied to reduce the noise component in the absence of speech signals. Instead of a fixed attenuation factor (-30 dB) in Boll's technique, an adaptive attenuation factor may be derived in this method. Modeling the speech activity as a hypothesis testing case, it can be represented as:

$$\begin{cases} H_0 : \text{speech absent: } |X(m)| = |N(m)| \\ H_1 : \text{speech present: } |X(m)| = |A e^{j\theta} + N(m)| \end{cases} \quad (3-15)$$

Only the measured envelope is used in this measurement model since the measured phase provides no useful information in the suppression of noise. The spectral envelope estimate,  $A$ , derived from the minimization of the



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FIGURE 3.1.1 TRANSFER CHARACTERISTICS OF THE NOISE SUPPRESSION DEVICE



mean-squared error  $E[(A - \hat{A})^2]$  is given as  $E[A|X]$ . This conditional mean can be expressed as

$$\begin{aligned}\hat{A} &= E[A|X] \\ &= E[A|X, H_1] P[H_1|X] + E[A|X, H_0] P[H_0|X]\end{aligned}\quad (3-16)$$

where  $P[H_k|X]$  is the probability that the speech is classified as in state  $H_k$ . The last term of eq. (3-16) becomes zero due to the fact that the average value of  $A$  when the speech is not present should be equal to zero. Then the estimate of the envelope  $A$  is given by

$$\hat{A} = E[A|X, H_1] P[H_1|X]\quad (3-17)$$

When speech is present, the expected spectrum  $E[A|X, H_1]$  represents the minimum variance estimate of  $A$  and it can be substituted with the maximum likelihood estimate given in eq. (3-13) which results:

$$\hat{A} \approx \frac{1}{2} \left[ |X| + \sqrt{|X|^2 - \sigma_N^2} \right] P[H_1|X]\quad (3-18)$$

where  $P[H_1|X]$  may be expressed as:

$$P[H_1|X] = \frac{P[|X|H_1] P[H_1]}{P[|X|H_1] P[H_1] + P[|X|H_0] P[H_0]}\quad (3-19)$$

Under hypothesis  $H_0$ , the received signal envelope consists of noise term only. Since the noise is a complex Gaussian process with a zero mean and

a variance  $\sigma_N^2$ , the envelope will have the Rayleigh probability density function and can be written as

$$p(|X| | H_0) = \frac{2|X|}{\sigma_N^2} \exp \left[ -\frac{|X|^2}{\sigma_N^2} \right] \quad (3-20)$$

Under hypothesis  $H_1$ , the probability density function of the received envelope will have the Rician density function and may be expressed as

$$p(|X| | H_1) = \frac{2|X|}{\sigma_N^2} \exp \left[ -\frac{|X|^2 + A^2}{\sigma_N^2} \right] I_0 \left[ \frac{2A|X|}{\sigma_N^2} \right] \quad (3-21)$$

Assuming that a priori probabilities of the hypothesis  $P[H_0]$ ,  $P[H_1]$  are equal and defining the a priori signal-to-noise ratio to be

$$\xi = \frac{A^2}{\sigma_N^2} \quad (3-22)$$

Equation (3-19) can be rewritten as

$$p(H_1 | |X|) = \frac{\exp(-\xi) I_0 \left[ 2\sqrt{\xi} (|X|^2/\sigma_N^2) \right]}{1 + \exp(-\xi) I_0 \left[ 2\sqrt{\xi} (|X|^2/\sigma_N^2) \right]} \quad (3-23)$$

It is this a-posteriori-probability that contributes the "soft-decision" aspect to the maximum likelihood envelope estimator as compared to the "hard decision" of eq. (3-13) for which the speech plus noise is either passed or is blocked depending on the decision of the hypothesis. Defining a posteriori signal-to-noise ratio (i.e., measured signal-to-noise ratio SNR) as

$$\text{SNR} = |X|^2/\sigma_N^2 \quad (3-24)$$

and appending the measured input phase, the estimated spectral component may be expressed as

$$\begin{aligned}
 \hat{S}(m) &= \hat{A}(m) \frac{X(m)}{|X(m)|} \\
 &= \frac{1}{2} \left[ 1 + \frac{\sqrt{|X(m)|^2 - \sigma_N^2}}{|X(m)|} \right] \cdot X(m) \cdot p[H_1 | |X(m)|] \\
 &= \frac{1}{2} \left[ 1 + \sqrt{\frac{\text{SNR}-1}{\text{SNR}}} \right] \frac{\exp(-\xi) I_0(2\sqrt{\xi \cdot \text{SNR}})}{1 + \exp(-\xi) I_0(2\sqrt{\xi \cdot \text{SNR}})} X(m)
 \end{aligned}
 \tag{3-25}$$

The channel gains, given as the multiplication of the a-posteriori probability for the speech state  $P[H_1 | |X|]$  by the maximum likelihood envelope estimate of eq. (3-13), are plotted in Figure 3.1.2 as a function of a-posteriori signal-to-noise ratio (SNR) for various values of a priori signal-to-noise ratio  $\xi$ . The two-state soft-decision maximum likelihood algorithm applies more suppression when the measured SNR is low and this case "most likely" corresponds to the noise state. On the other hand, little attenuation is applied when the SNR is large. This is a desirable property of the noise suppression device, since the state of large SNR "most likely" means that speech is present, in which little attenuation is desired. As  $\xi$  increases, the channel gain curves become sharper which indicate that the speech state ( $H_0$  or  $H_1$ ) can be distinguished easier for large  $\xi$ . In the limit, the output may be totally suppressed or passed depending on the value of a measured a posteriori signal-to-noise ratio. This particular case leads to the similar performance of Boll's noise suppression algorithm whose attenuation factor depends solely on the decision of

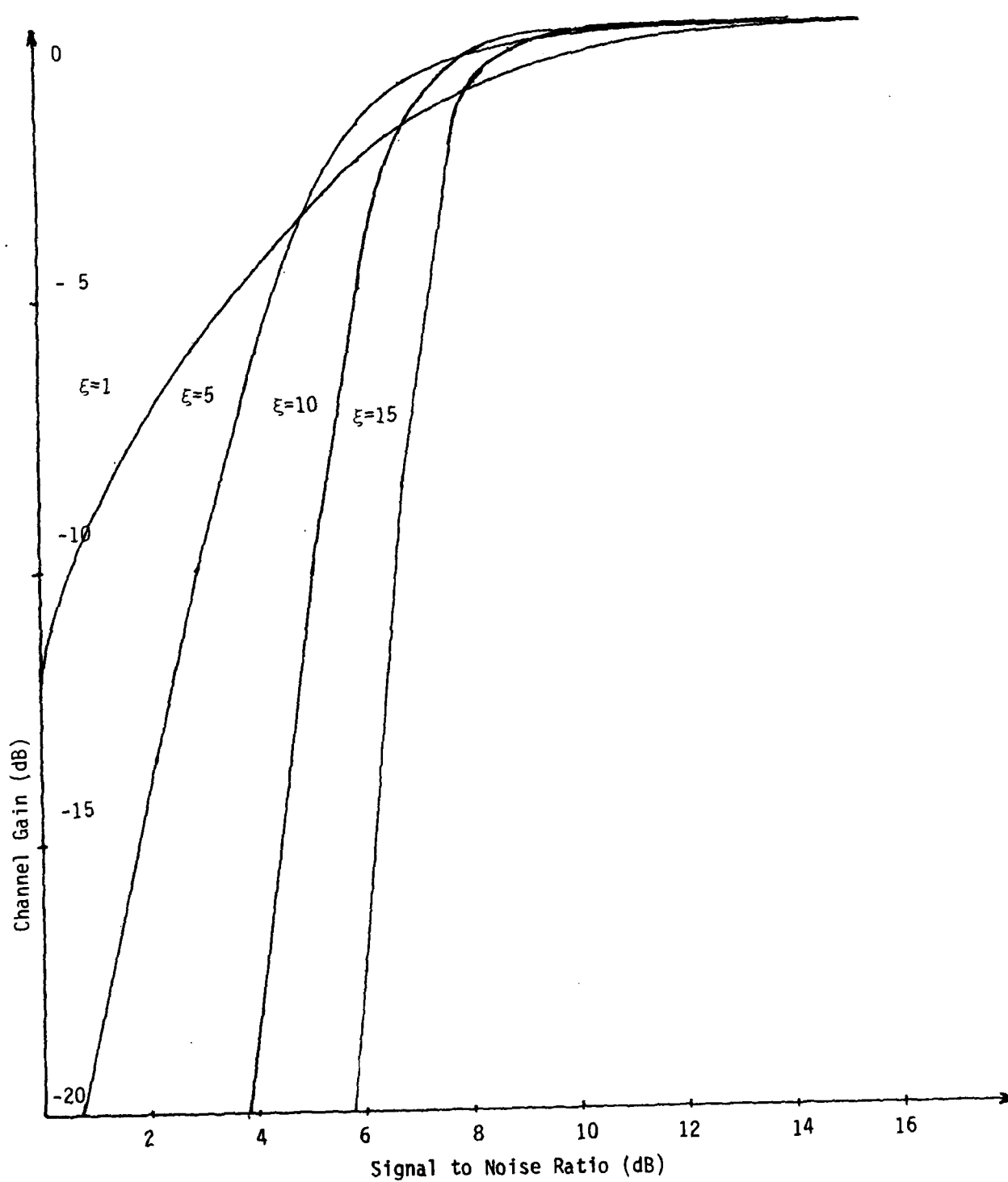


FIGURE 3.1.2: THE CHARACTERISTIC FUNCTION OF THE MAXIMUM LIKELIHOOD NOISE SUPPRESSION

speech state. With the selection of  $\xi$ , the McAuley technique provides the versatility of noise suppression in an adaptive fashion. It is, therefore, convenient to refer  $\xi$  as the "suppression factor" which is chosen according to the background noise level. Once  $\xi$  is chosen, the a posteriori signal-to-noise ratio must be measured in order to calculate the channel gain as shown in eq. (3-25).

The block diagram of the noise suppression technique is shown in Figure 3.1.3. In this scheme, the energy of the input signal is computed and fed to the noise detector which decides the speech activity, i.e., speech present or speech not present (noise) using the detection algorithm as discussed in Appendix B. Concurrently, the spectra of the input signal  $X(k)$  are calculated via the FFT (fast Fourier transform) technique. The resulting spectral components are directed to the spectral mean adjustment device when the speech is not present. The multiplication gain factors are calculated for each spectral component from the input spectra and the average noise spectra. These gain factors are then multiplied with the input spectra, and the estimated signal is obtained via inverse FFT.

Mathematically, let the average noise power at the  $m$ th frame and  $n$ th channel be:

$$\lambda(m) = \lambda_n(m-1) + \alpha \left[ |X(m)|_n^2 - \lambda_n(m-1) \right] \quad (3-26)$$

where  $\lambda(m) = \sigma_N^2(m)$  is used for notational convenience and  $|X(m)|_n^2$  represents the measured noise power spectrum at the  $n$ th channel of the  $m$ th frame. Then, the average noise power is updated after each frame using the time constant about 1 sec., i.e.,

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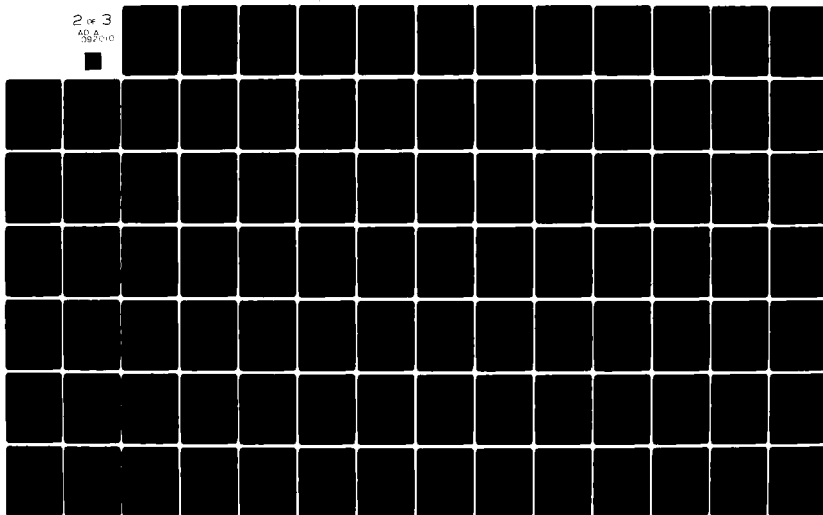
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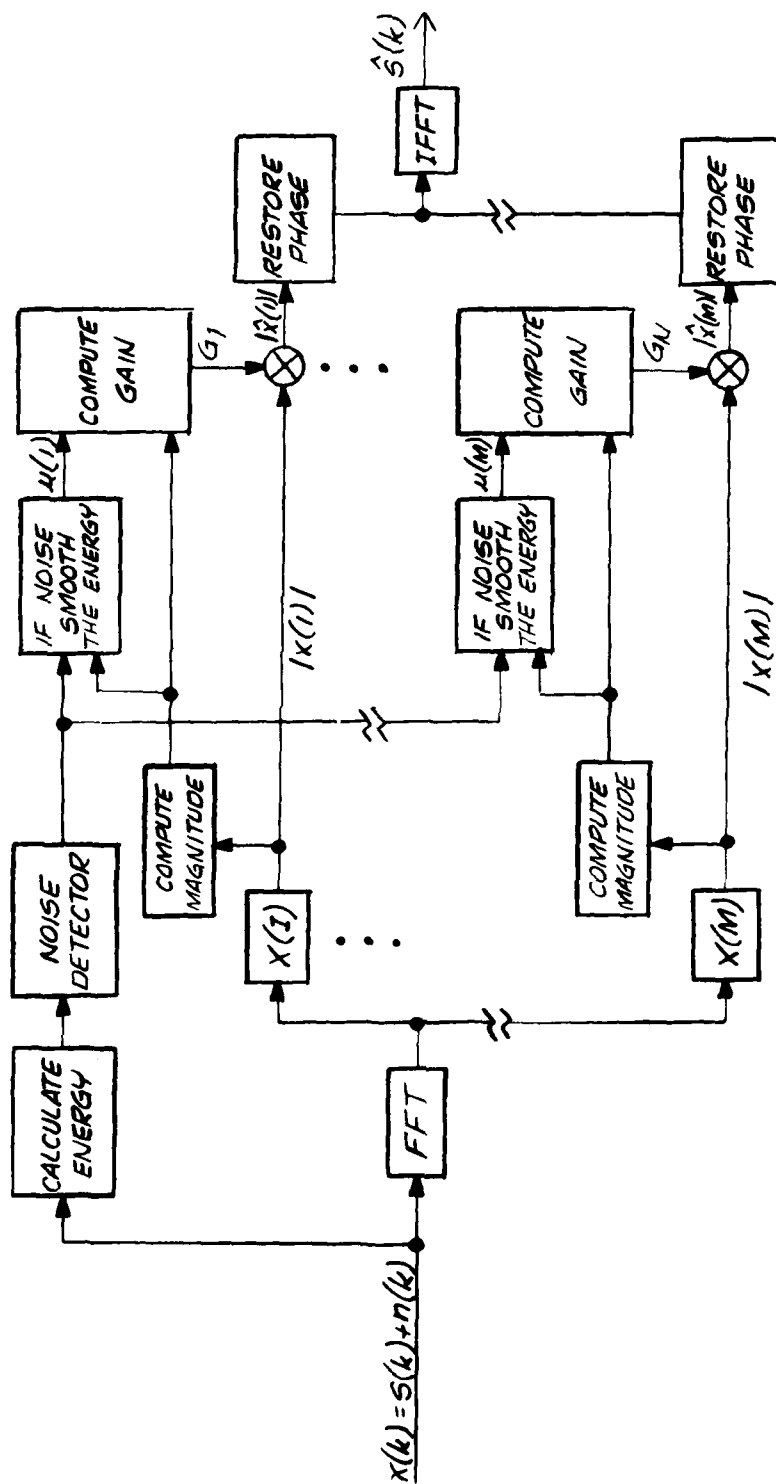
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FIGURE 3.1.3 BLOCK DIAGRAM OF MCAULEY'S NOISE SUPPRESSION ALGORITHM

$$\alpha = \exp \{-22.5/T\} \quad (3-27)$$

where 22.5 represents a frame period in msec and T is the time constant in msec. One of the disadvantages of this scheme is the relatively long adaptation time required to determine the detection threshold and then additional training period may be required to learn the channel noise statistics. Let the gain factor of the spectral subtraction be

$$g_n(m) = \frac{|X(m)|_n^2 - \lambda_n(m-1)}{|X(m)|_n^2} \quad (3-28)$$

Then the channel gain can be expressed from eq. (3-25) as

$$\begin{aligned} G_n(m) &= \frac{|\hat{S}_n(m)|}{|X(m)|_n} \\ &= \frac{1}{2} (1 + \sqrt{g_n(m)}) \frac{\exp(-\xi) I_0\left(2\sqrt{\frac{\xi}{1-g_n(m)}}\right)}{1 + \exp(-\xi) I_0\left(2\sqrt{\frac{\xi}{1-g_n(m)}}\right)} \end{aligned} \quad (3-29)$$

The advantage of using  $g_n(m)$  as an independent variable is that the value of  $g_n(m)$  is less than one, which facilitates the computation of the channel gain using a simple table look-up program. Fifteen tables corresponding to values  $\xi = 1, 2, \dots, 15$  have been tabulated in the noise suppression algorithm, with each table consisting of 50 values of suppression rule computed for equal increment of  $g_n(m)$  from 0 to 1.

The McAuley algorithm has been applied to the processing of speech signals added with various types of background noise with the 16 Kb/s SBAPC system. The output of the noise suppression device or the synthesizer



speech is noted to have amplitude fadings when large  $\xi$  is used in the high noise environment ( $S/N < 0$  dB). This is a very objectionable degradation of speech. In order to maintain a constant amplitude output even for

large  $\xi$ , a simple automatic gain control (AGC) routine has to be incorporated with the noise suppression algorithm. If  $G_A(m)$  denotes the average channel gain at the  $m$ th frame, i.e.,

$$G_A(m) = \frac{1}{M} \sum_{n=0}^{M-1} G_n(m) \quad (3-30)$$

where  $M$  is the channel number in frequency domain. This average gain factor may indicate approximately the amounts of the spectral suppression. A small number of  $G_A(m)$  may correspond to a large amount of power attenuation. In this case, the output may need a large amplification to avoid the fading of amplitudes. Furthermore, to maintain a constant gain throughout all the frames, a smoothing algorithm is utilized and the overall gain becomes:

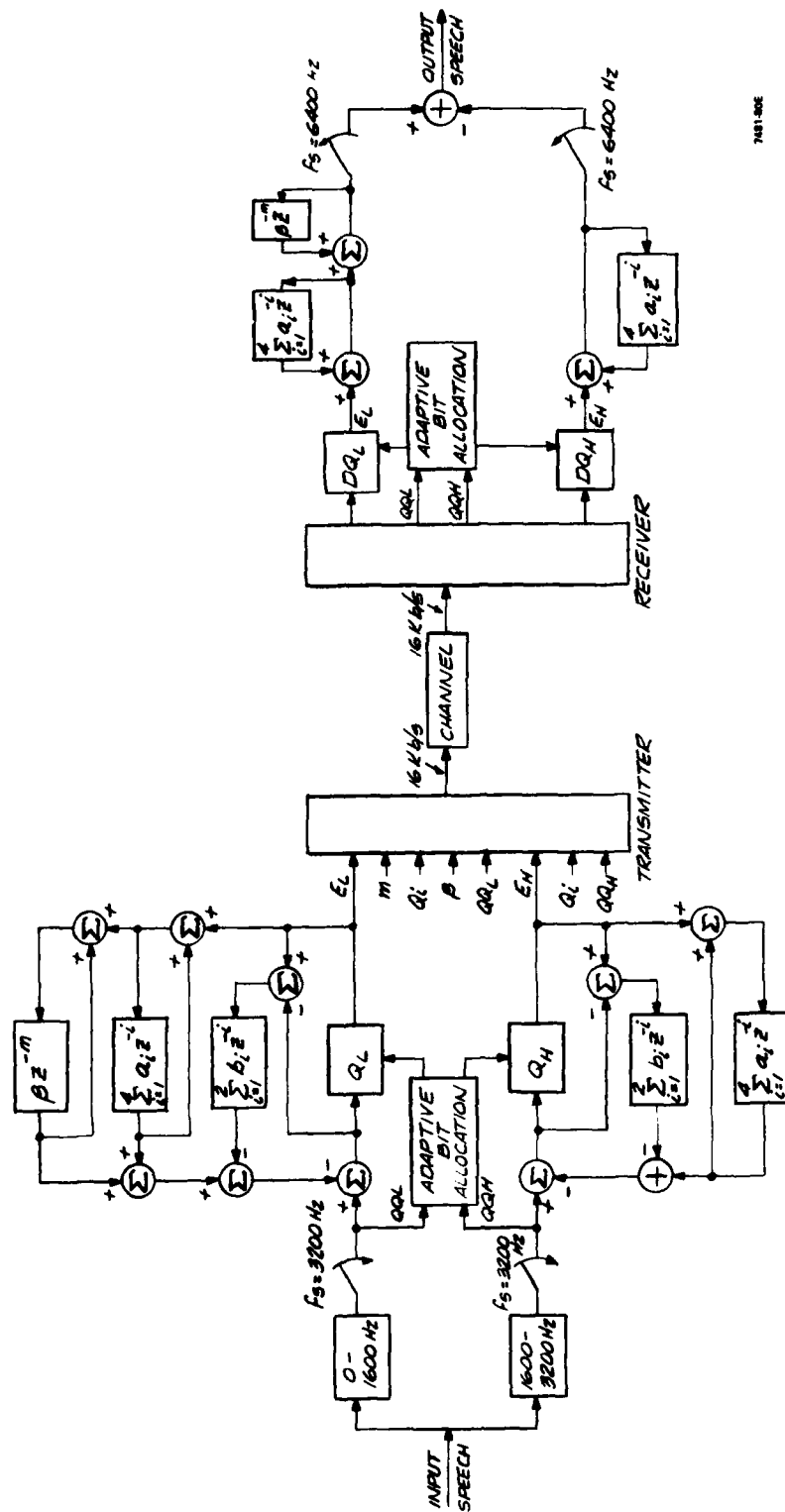
$$G(m) = \frac{\frac{1}{128} \sum_{\ell=0}^{129} G_A(m-\ell)}{\frac{1}{4} \sum_{\ell=0}^3 G_A(m-\ell)} \quad (3-31)$$

In our simulations, the effects of amplitude fading have been reduced even in the high noise case ( $S/N = -6$  dB) where the gain factor  $G(m)$  is utilized to adjust the output of the noise suppression device. The noise suppression algorithm developed in this project can be used as a pre-processor to any speech signal processing algorithm, and the overall system can be further optimized with respect to the noise suppression/speech distortion tradeoff analysis by choosing an appropriate suppression factor  $\xi$ .

### 3.2 The Effect of Random Channel Errors on the SBAPC

The SBAPC system, as discussed in Section II, produces a high quality synthesized speech at the data rate of 16 Kbps. However, error-free transmissions are not always possible in many practical systems, since the transmitted signals may be corrupted by noises in the channel which may or may not vary with time. Under these circumstances, the performance of the SBAPC changes greatly with the rates and also with the positions of the channel errors within the frame.

In this study, the effect of random channel errors at rates ranging from  $0 - 10^{-2}$  is investigated. The configuration of the SBAPC system tested ( $\approx 15$  Kbps) is shown in Figure 3.2.1 which includes the 32-tap QMF, 1st order pitch loop on the low band, 4th order APC on both bands, noise shaping on both bands, and adaptive allocation of 288 bits on quantizing the subband signals. The signal-to-noise ratio plot versus bit error rates (BER) is shown in Figure 3.2.2. The result indicates that the SBAPC system is extremely sensitive to channel errors. At  $10^{-4}$  BER, the algorithm's performance is virtually unchanged as compared to the no error case. However, the degradation becomes noticeable at  $5 \times 10^{-4}$  BER, and the signal-to-noise ratio drops by 5 dB at  $10^{-3}$ . At  $10^{-2}$  BER, the system is useless since the output speech becomes unintelligible. As expected, errors occurred on the side information bits which include pitch, PARCOR coefficients, energy, etc., have a more detrimental effect as compared to those occurred on the quantized residual signal bit stream. This suggests that in order to make the SBAPC system useful in a noisy channel, protections of the transmitted bits are vital, particularly for the side information bits. The following section describes the utility of forward error correcting codes in reducing the effect of channel errors.



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FIGURE 3.2.1 THE 16 KBPS SPLIT-BAND APC SYSTEM

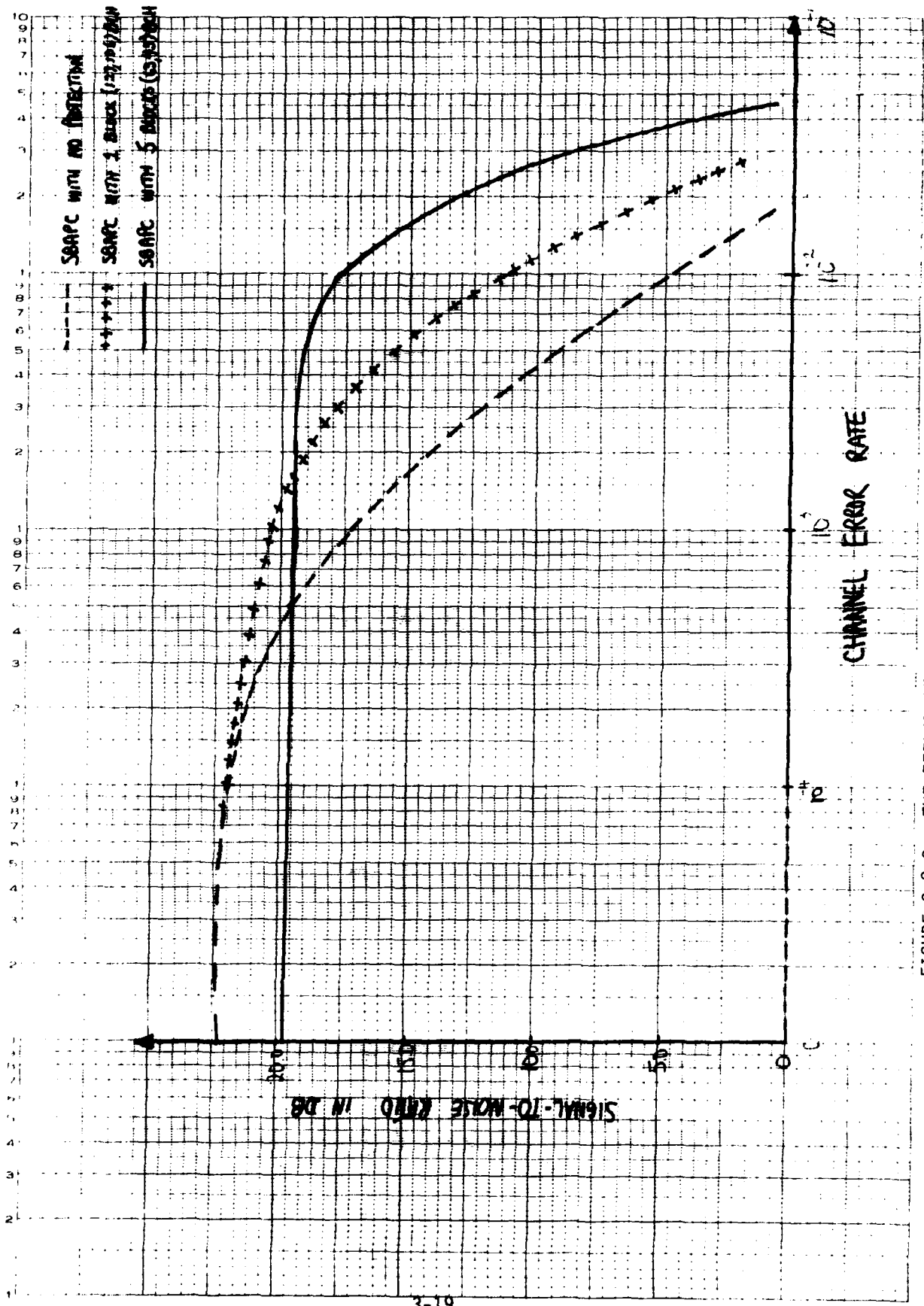


FIGURE 3.2.2: THE EFFECT OF CHANNEL ERROR RATES ON 3 SBAPC SYSTEMS

### 3.2.1 Application of BCH Codes

The method of correcting errors may be chosen depending on the application circumstances, i.e., data rate, channel error rate, complexity and cost, etc. Since the SBAPC coder is designed for real-time implementations, it is desirable to have error correcting codes that require the least amount of time delay in correcting channel errors. Block codes of short length may be well suited to the real-time implementation of the SBAPC algorithm since no additional time delay is required to process the error correcting procedure if the length of the block code is less than the number of bits received in a frame period. There are many types of block codes that can be utilized for different channel characteristics.

Practical communication channels corrupt signals in many ways, such as the additive Gaussian noise and/or impulsive noise that produce random and burst errors, respectively. In other situations, the characteristics of the channel may vary in time (fading HF channels) or may be random since it represents a sample function of an ensemble of channels with widely different characteristics (switched telephone network). Hence, it is non-trivial to construct a coding scheme that adapts to various types of channels. Since additive Gaussian noise is the main source of noise in many practical communication channels, only forward error correcting codes that are capable of correcting random errors are considered.

The Base-Chaudhuri-Hocquenhem (BCH) code, which is a remarkable generalization of Hamming codes, has been known to be the most powerful multiple random-error correcting code. Also, the decoding algorithm can be implemented with a reasonable amount of complexity. A more fundamental description of the BCH codes and their encoding, decoding algorithms are given in Appendix C. This appendix has shown that

with the block length of  $n = 2^m - 1$  and  $mt$  parity bits it is possible to correct any  $t$  or less errors using a  $(n, k)$  BCH code where  $k$  is the number of information bits. The proper choice of  $m, n, t$  for BCH codes may depend on the channel error rate, data rate, and the system's specifications. The information rate of the  $(n, k)$  BCH code is given as:

$$R = k/n \quad (3-32)$$

The performance of random-error correcting BCH codes may be expressed in terms of error-probability. Let  $P(m, n)$  be the probability of  $m$  errors occurring in an  $n$ -bit block and  $\beta_m$  be the probability of decoding an error pattern of weight  $m$  correctly, then the probability of decoding received code word erroneously may be expressed as

$$\begin{aligned} P_e &= 1 - \sum_{m=0}^n \beta_m P(m, n) \\ &= \sum_{m=0}^n \alpha_m P(m, n) \end{aligned} \quad (3-33)$$

where  $\alpha_m = 1 - \beta_m$  denotes the probability of erroneously decoding an error pattern of weight  $m$ . The parameter  $\alpha_m$  is a function of the code and decoding algorithm. If a  $t$  error-correcting BCH code is employed and it is decoded using the Peterson decoding algorithm shown in Appendix D, the parameter  $\alpha_m$  may be expressed as

$$\begin{aligned} \alpha_m &= 0 & 0 \leq m \leq t \\ &= 1 & t < m \leq n \end{aligned} \quad (3-34)$$

and the probability of erroneously decoding the code word may be reduced, .....  
from eq. (3-33) as

$$P_e = \sum_{m=t+1}^n p(m, n) \quad (3-35)$$

If the bit errors occur independently at random with probability  $e$ , then the probability  $p(m, n)$  can be expressed as

$$p(m, n) = \sum_m^n e^m (1-e)^{n-m} \quad (3-36)$$

where the probability  $p(m, n)$  is simply the binomial distribution and  $P_e$  in eq. (3-35) is equal to the tail of the distribution.

### 3.2.2 Error Protection via the (127,106) BCH code

This technique employs one block of three-error correcting (127,106) BCH code which protects 106 information bits with 21 parity ones. For the 16 Kb/s SBAPC system, all 50 side information bits, together with 56 sign bits of the residual signals are encoded. A sync bit and 232 error signal bits are left unprotected. Though this coding scheme is efficient (i.e., only 5.8% of the total bits are used for error protection), its success hinges largely on the assumption that the SBAPC system is tolerant to random errors occurred on the residual signal bit stream. The S/Q plot versus BER for the SBAPC system with the (127,106) BCH Code is depicted by the graph (+) in Figure 3.2.2. As illustrated in the figure, the protected SBAPC system consistently out-performs the original unmodified one in high error cases. For the system with the (127,106) BCH code, the S/Q remains relatively unchanged for BER from  $0 - 10^{-3}$ . Unfortunately, its

performance starts to degrade at  $2 \times 10^{-3}$  BER, and poor quality, though intelligible, speech is obtained at  $10^{-2}$  BER. This result reveals two important findings: 1) protection of only side information is not even adequate in maintaining the SBAPC performance in relatively low-error environments; 2) the utilization of long block BCH codes is not the best strategy for high-error situations (e.g.,  $\text{BER} = 10^{-2}$ ). The first finding can be attributed to the presence of the pitch loop in the SBAPC algorithm which propagates the residual signal errors to successive frames. One solution to the above situation is to apply error protection to residual signal bits as well as to side information bits at the expense of higher transmission rates. The second finding results from the fact that the occurrence of channel errors is more likely in a longer data block. If this error count exceeds the correcting capability of the BCH code ( $t = 3$  for the (127,106) BCH code), the code renders no utility. To illustrate this, the probability of more than 3 error occurrence in the block of 127 bits at  $10^{-2}$  channel error rate is computed using eq. (3-36) as follows:

$$\begin{aligned}
 P_e &= \sum_{m=4}^{127} p(m, 127) \\
 &= 1 - p(0,127) - p(1,127) - p(2,127) - p(3,127) \quad (3-37) \\
 &= 0.0393
 \end{aligned}$$

On the average, there will be 4 blocks out of every 100 that will have more than 3 errors, and they will not be corrected. Furthermore, the presence of the pitch loop in the SBAPC algorithm compounds the effects by propagating the errors through several frames. One solution to overcome the above deficiency is the utilization of several blocks of short BCH codes



e.g., (63,45). To illustrate this, the probability of more than 3-error occurrence in the block of 63 bits at  $10^{-2}$  channel error rate is computed using eq. (3-36) as follows:

$$\begin{aligned}
 P_e &= \sum_{m=4}^{63} p(m, 63) \\
 &= 1 - p(0,63) - p(1,63) - p(2,63) - p(3,63) \quad (3-38) \\
 &= 0.003725
 \end{aligned}$$

This indicates that on the average, 4 blocks out of every 1000 will have more than 3 errors, making this code an order of magnitude more resistant to channel errors than the (127,106) BCH code.

### 3.2.3 Error Protection via Five Blocks of (63,45) BCH Codes

As discussed in Section 3.2.2, the incorporation of 1 block of (127,106) BCH code to protect the 50 side information bits and 50 residual signal bits does extend the utility of the SBAPC system from  $10^{-3}$  to  $5 \times 10^{-3}$  channel error rate. However, at  $10^{-2}$ , its performance is still considered unacceptable. One alternative is to use shorter length BCH codes to maintain their error correcting capability in high error environments. Also, the employment of multiple blocks of these short BCH codes to protect more residual signal bits will further enhance the SBAPC system's robustness to channel errors. The following describes a forward error-correcting procedure that employs 5 blocks of (63,45) BCH codes, and it extends the utility of the SBAPC algorithm to  $10^{-2}$  BER.

Since 5 blocks of (63,45) BCH codes require 90 parity bits, the SBAPC algorithm has to be modified slightly in order to maintain a transmission

rate of 16 Kbps (360 bits per frame at 44.44 frames/sec.). In this new configuration, 50 bits/frame are for side information quantization, 216 bits/frame are for encoding residual signals, 90 bits are needed for parity checks, and the remaining 4 bits are for synchronization purposes. As for the error protection, 90 parity bits are used to defend 50 side information bits and 175 residual signal bits. The signal-to-quantization noise plot versus bit error rates is shown in Figure 3.2.2. Compared to the SBAPC system with no protection or that with 1 block of (127,106) code, the multiple-block encoding scheme yields slightly inferior S/Q for low channel error rates ( $BER \leq 5 \times 10^{-3}$ ). This result is not surprising since a higher percentage (25%) of the available bits are spent on parity checking rather than on quantizing the residual signals. Consequently, the subband error signals are represented less precisely yielding lower S/Q. However, informal listening tests reveal no or little audible differences between the processed sentences obtained through the SBAPC system with 5 blocks of (63,45) BCH codes and the SBPAC with 1 block of (127,106) code in the error-free case. This may be explained by the fact that the S/Q for the SBAPC with multiple-block error coding is already high ( $\sim 19.6$  dB). An additional 2.5 dB increase obtained from the SBAPC with 1 block error coding is not sufficient to perceptually improve voice quality. For channels with high error rates, the multiple block coding scheme outperforms the one block system by as much as 7 dB, and it yields high quality speech even at  $10^{-2}$  BER. So, employing the 5-block (63,45) BCH coding scheme, the performance of the 16 Kb/s SBAPC system can be made robust to channel error rates as high as  $10^{-2}$ .

### 3.3 Tandem Performance with 2.4 Kb/s LPC-10

In daily communications, users of the 16 Kb/s wideband terminals may have to converse with those of the 2.4 Kb/s narrowband ones. Though these terminals may individually produce satisfactory outputs, the overall speech quality when they are in connection or in tandem is sometimes degraded. This type of distortion is exemplified by the "buzzy" speech quality obtained when the 16 Kb/s Tenley terminal, which employs the Continuously Variable Slope Deltamodulator (CVSD), is connected with the 2.4 Kb/s STU-2 terminal which encodes speech using the LPC-10. The degradation may be partly attributed to the algorithms which have been optimized only for clean input speech. Moreover, it may also be due to the interactions of distortions introduced by the first speech encoding scheme with that of the subsequent terminals. So, in order for the 16 Kb/s SBAPC algorithms to provide greater utility, good tandem performance with LPC is a definite requirement.

APC schemes are known to tandem well with LPC [20]. Since the SBAPC algorithm is a modified form of APC, it also exhibits no undesirable distortions when connected with LPC. In particular, when the peaky LPC synthesized waveform is fed into the SBAPC, a smooth but slightly low-passed quality speech results. When compared to the processed material obtained from the LPC/CVSD tandem, the speech quality of the LPC/SBAPC tandem is less muffled since the SBAPC algorithm does not produce

slope overloading. On the other hand, when the SBAPC synthesized speech is fed into LPC, outputs similar to that derived from LPC alone are obtained. The SBAPC/LPC is much more pleasant to listen to than the "buzzy" quality of the CVSD/LPC tandem.

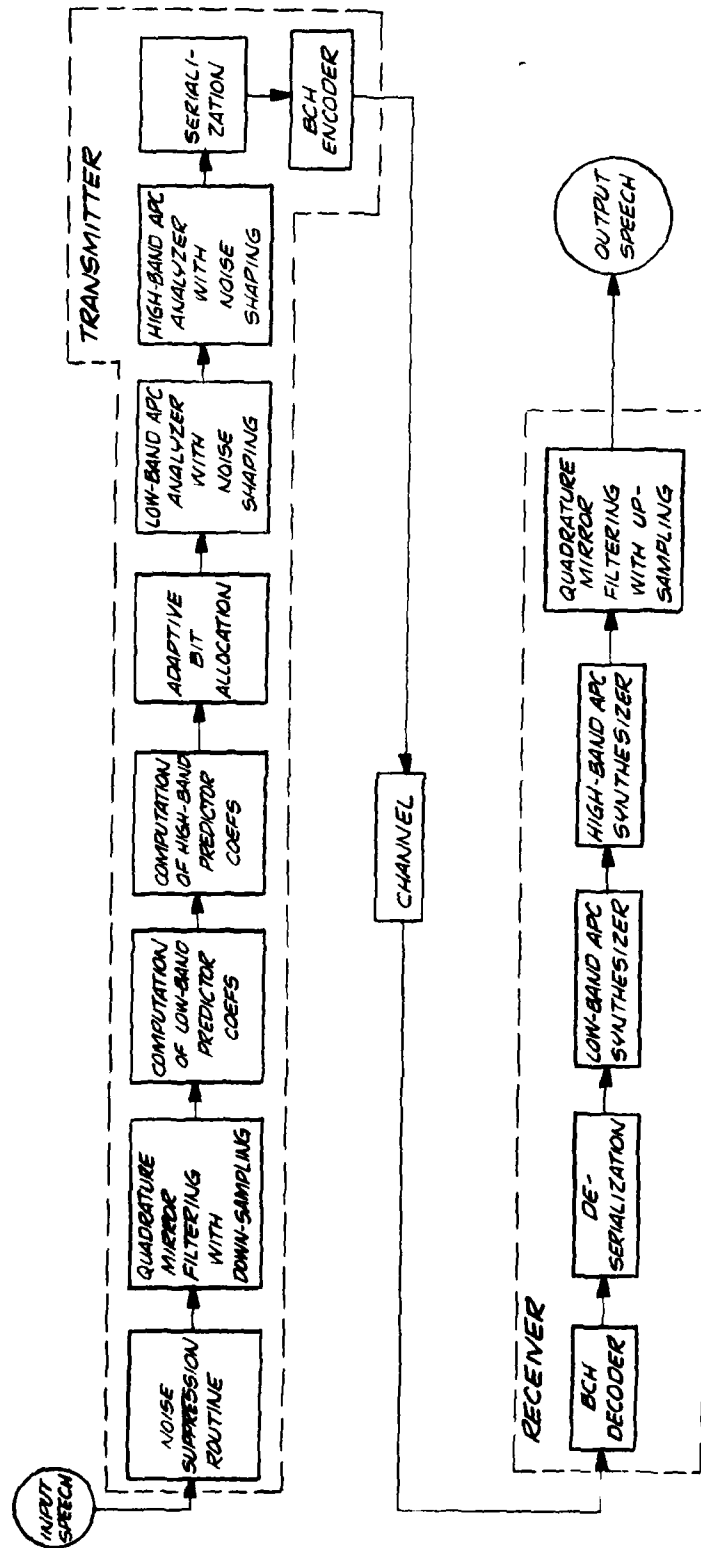
## SECTION IV

### FORTRAN SIMULATIONS

#### 4.1 FORTRAN Simulations of the SBAPC System

The SBAPC algorithm, as depicted in Figure 3.2.1, has been simulated on a PDP 11/70 computer using FORTRAN IV-PLUS. The flow diagram of the program is summarized in Figure 4.1.1. Input speech, previously digitized and stored on disks or magnetic tapes, is processed by the SBAPC program and the output material is also written back on disks or tapes. Operations of the transmitter include noise suppression, quadrature mirror filtering with down-sampling, computation of low band predictor coefficients, computations of high band predictor coefficients, adaptive bit allocations, low band APC analyzer with noise shaping, high band APC analyzer with noise shaping, serialization, and BCH encoder. At the receiver, transmissions of wrong binary bits are corrected via a BCH decoder. After deserialization and dequantization, the received residual signals and APC parameters generate estimates of the low band and the high band waveforms via their corresponding APC synthesizers. The output speech is then obtained by up-sampling the two subband signals together with quadrature mirror filtering.

At the transmitter, the speech samples are brought in  $(144 + 18)$  at a time, but only 144 samples correspond to the new frame. The other 18 samples belong to the previous frame and they are employed for smoothing frame boundaries. Then the new data are processed through the noise suppression routine whose flowchart is shown in Figure 4.1.2. Initially, the energy and the spectrum of the input signal are computed. According to its energy, the decision on whether the frame is silence, noise only or speech with noise is made with the help of the modified Robert's algorithm in



7480-90E

FIGURE 4.1.1 FLOW DIAGRAM OF THE 16 KBPS SBAPC FORTRAN PROGRAM

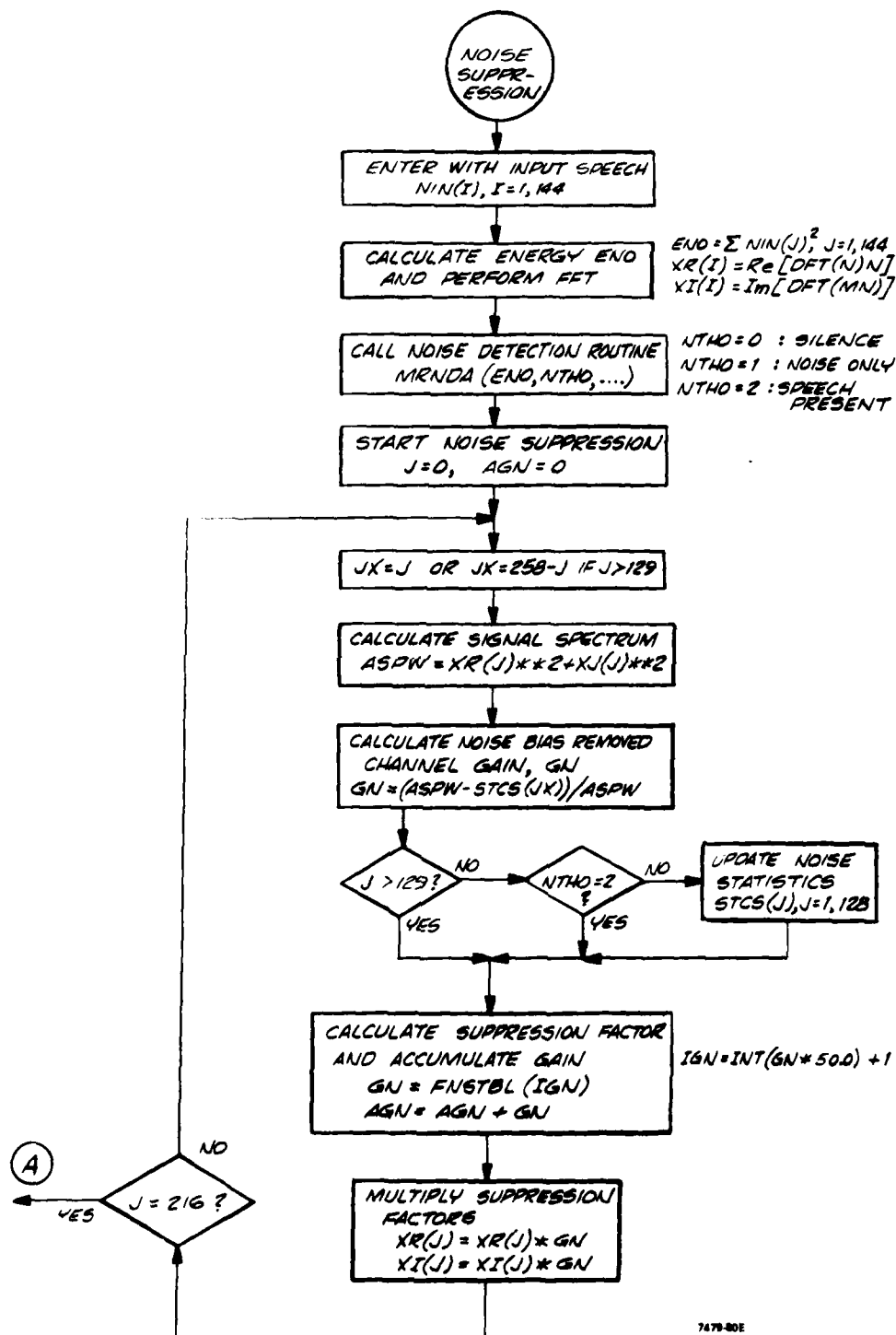


FIGURE 4.1.2 FLOW CHART OF NOISE SUPPRESSION ROUTINE

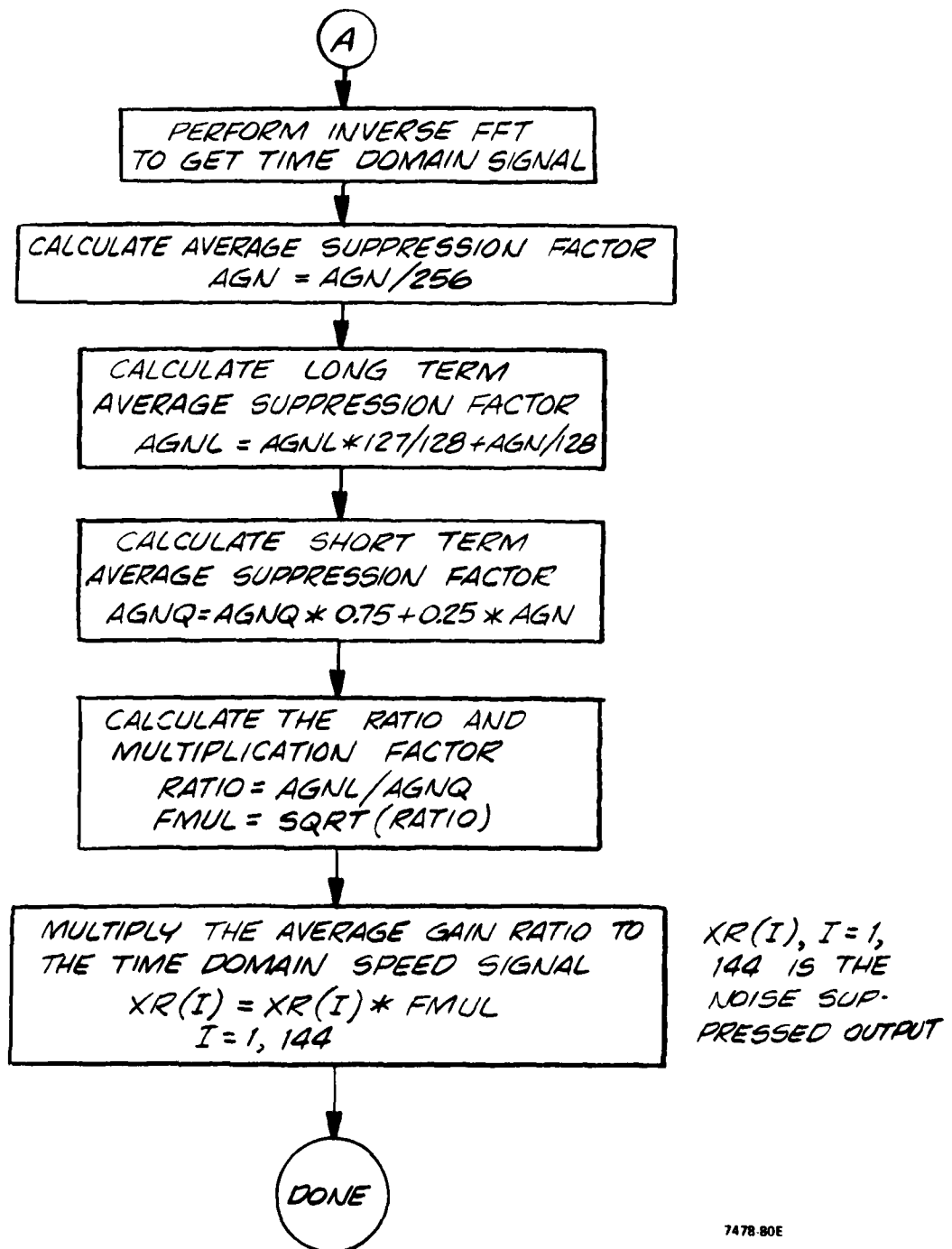


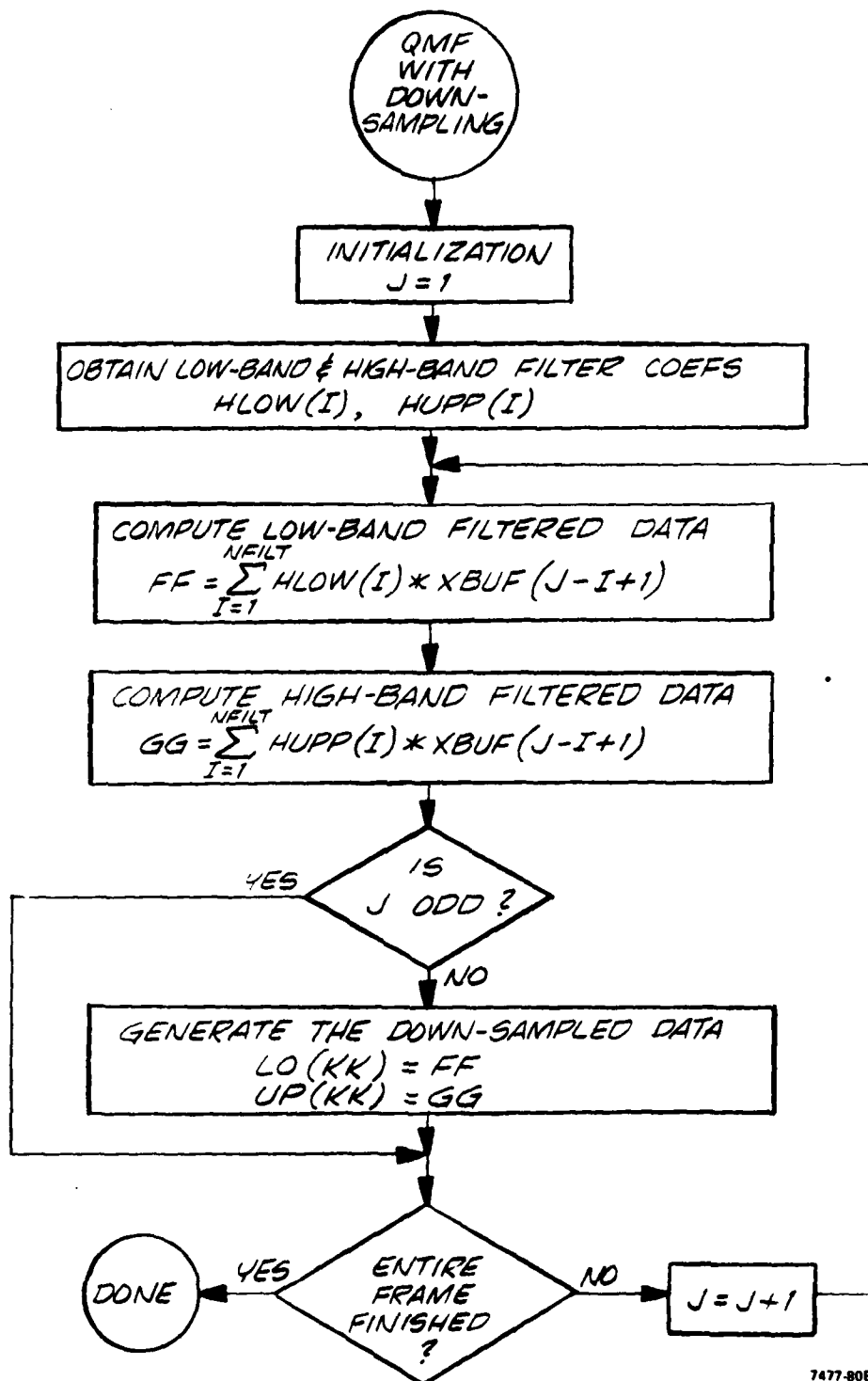
FIGURE 4.1.2 FLOW CHART OF THE NOISE SUPPRESSION ROUTINE (Cont.)

Appendix B. Based on this decision, the noise statistics are updated, and the noisy components are suppressed from the incoming signal using the McAuley algorithm as discussed in Section 3.2. Then the noise-reduced speech is fed into the SBAPC coder.

The first operation in the coder is to split the frequency band of the incoming signal into two subbands via quadrature mirror filtering in the manner as depicted in Figure 4.1.3. The waveforms of the low and high bands after down sampling are encoded using APC. The computation of the four low band APC coefficients are performed as shown in Figure 4.1.4 which includes the pitch extraction via the autocorrelation technique, the calculation of pitch gain, and the determination of PARCOR coefficients from the reduced waveform using the Levinson recursion. Similarly, the computation of the four high band APC coefficients are done as depicted in Figure 4.1.5. In contrast to the low band case, no pitch loop is necessary in the high band. After computing the filter coefficients, the prediction residual energies (QQL, QQH) for the two bands are utilized for quantizer bit allocation. The adaptive rule is detailed in Figure 4.1.6. With the definition of quantizer bit assignments, the APC residual signals for both bands are generated and quantized as illustrated in Figure 4.1.7. Makhoul's second order all-zero filter is also incorporated for shaping the quantizing noise. After serializing the quantized parameters into a bit stream, 5 blocks of (63,45) BCH codes (90 parity bits) are employed to encode 50 side information and 175 error signal bits as shown in Figure 4.1.8.

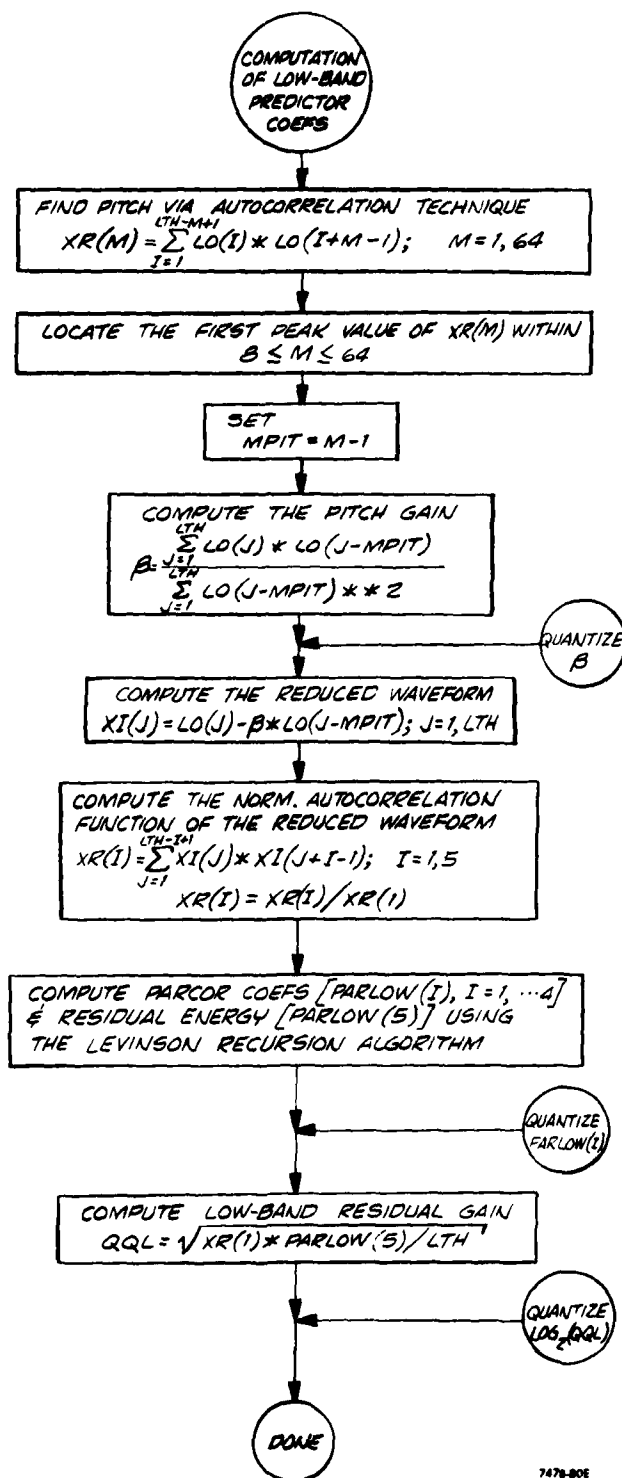
At the receiver, the reverse of the transmitter operations are performed. After correcting the transmission errors via the BCH decoder whose flowcharts are included in Figures C.1 and C.2, the bit stream is





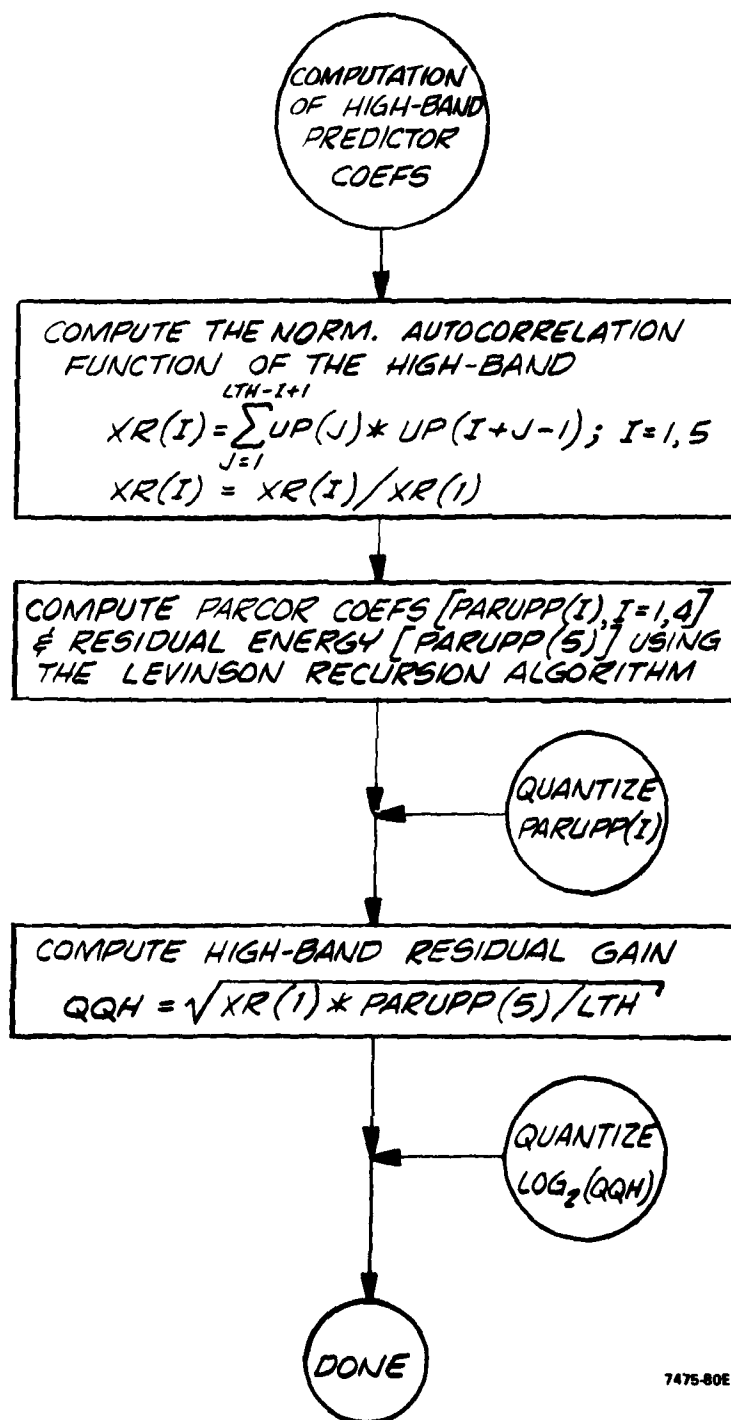
7477-80E

FIGURE 4.1.3 FLOW CHART OF QMF WITH DOWN-SAMPLING



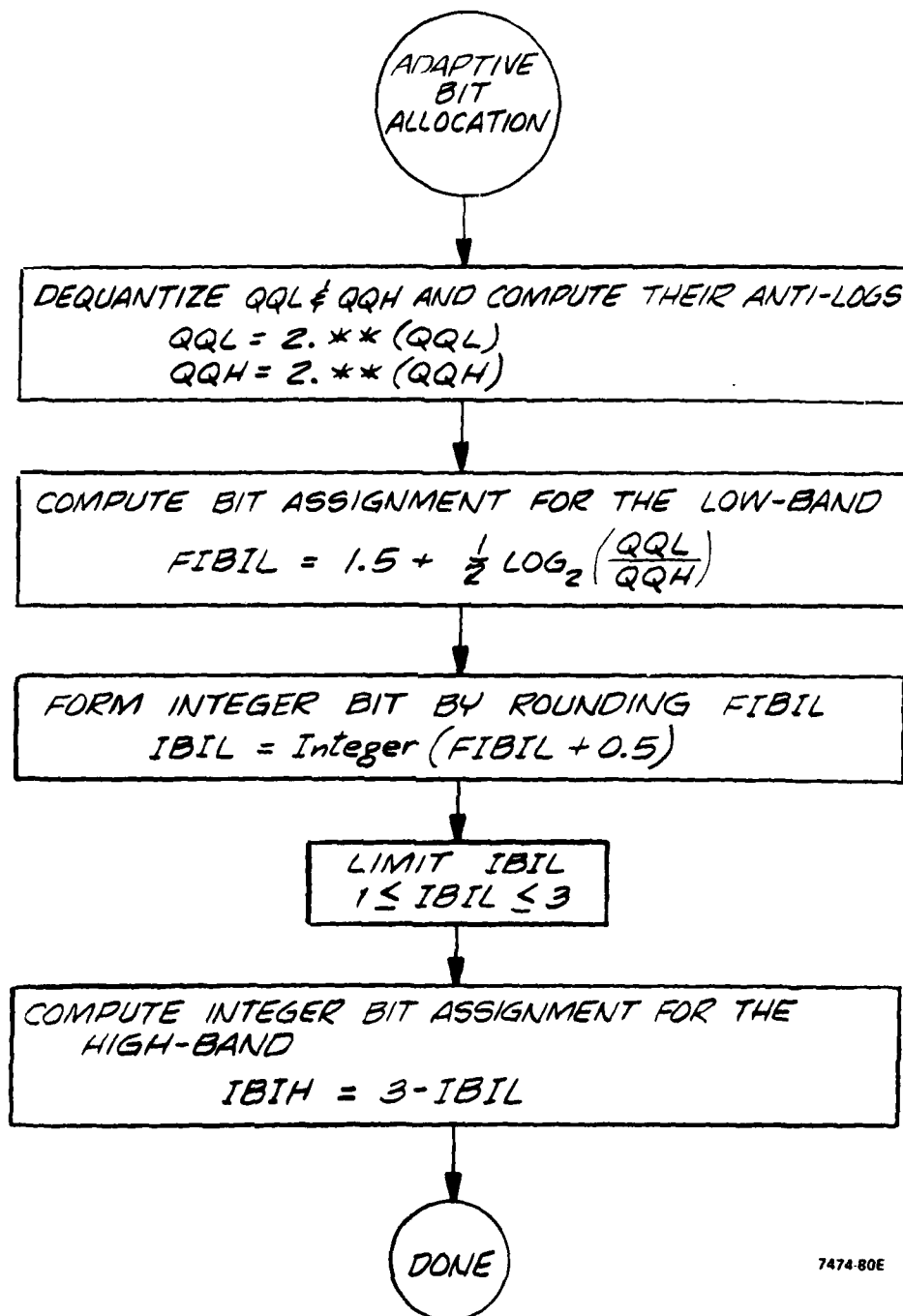
7478-80E

FIGURE 4.1.4 FLOW CHART OF LOW-BAND PREDICTOR COEFS COMPUTATION



7475-80E

FIGURE 4.1.5 FLOW CHART OF HIGH-BAND PREDICTOR COEFS COMPUTATION



7474-80E

FIGURE 4.1.6 FLOW CHART OF ADAPTIVE BIT ALLOCATION

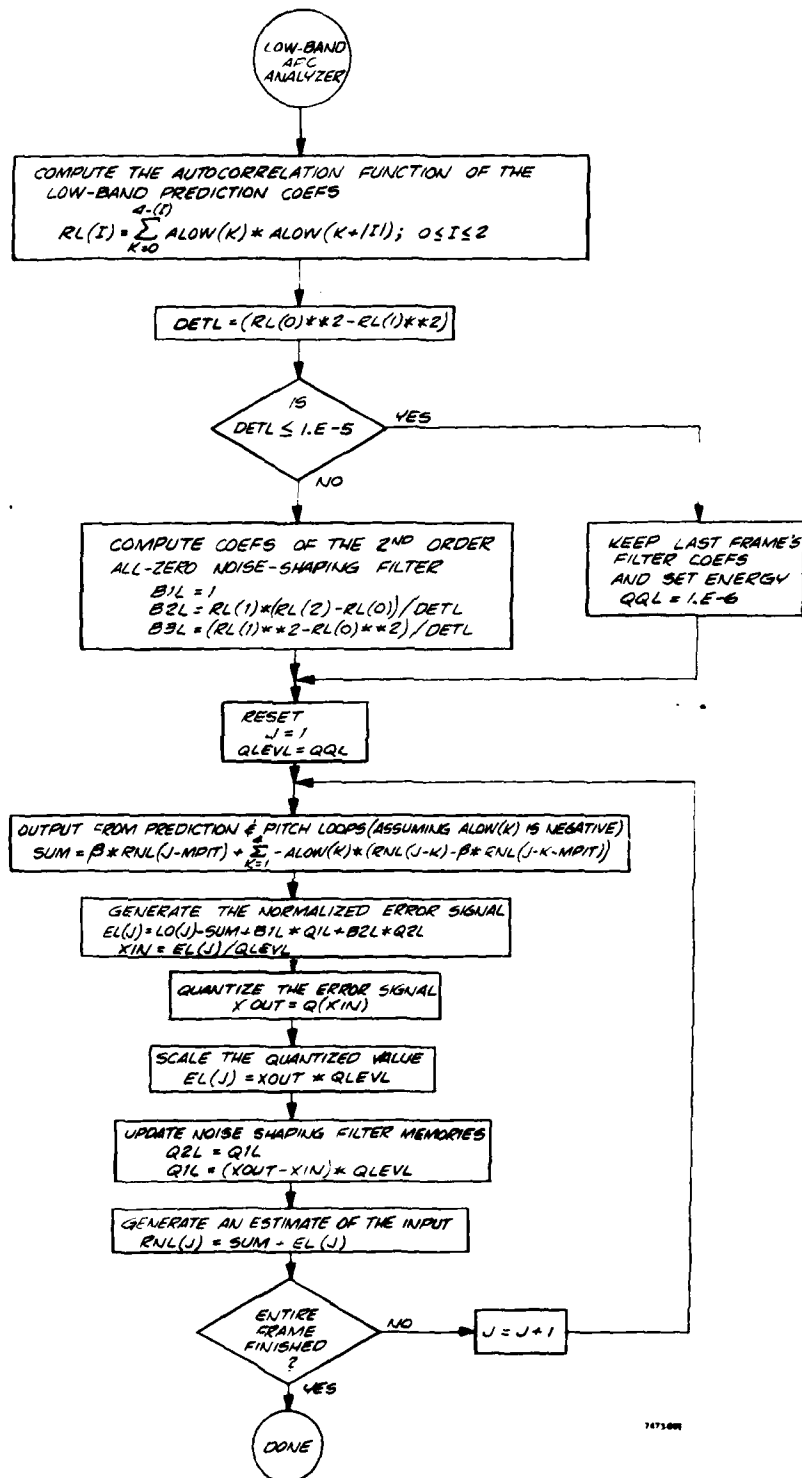
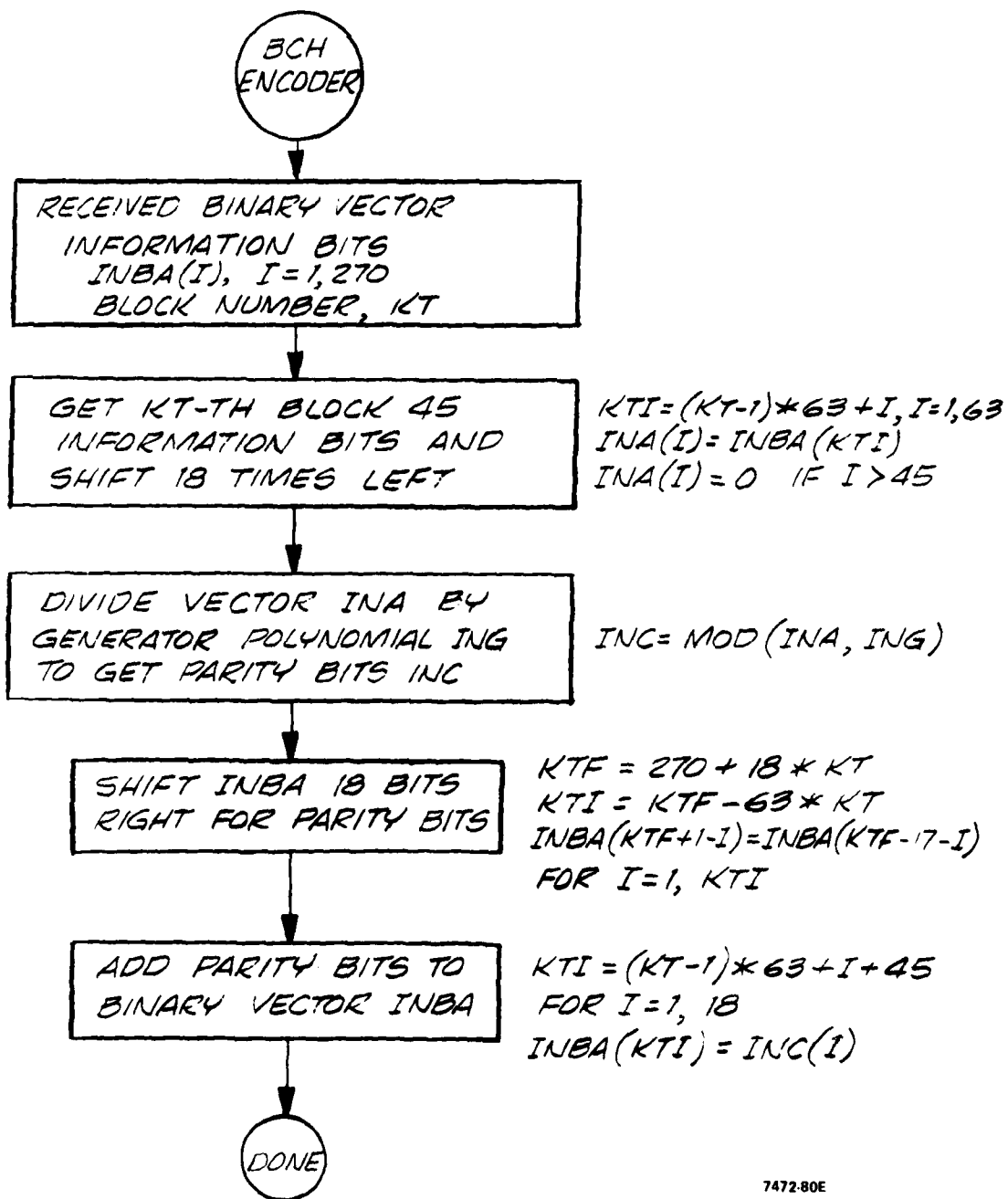


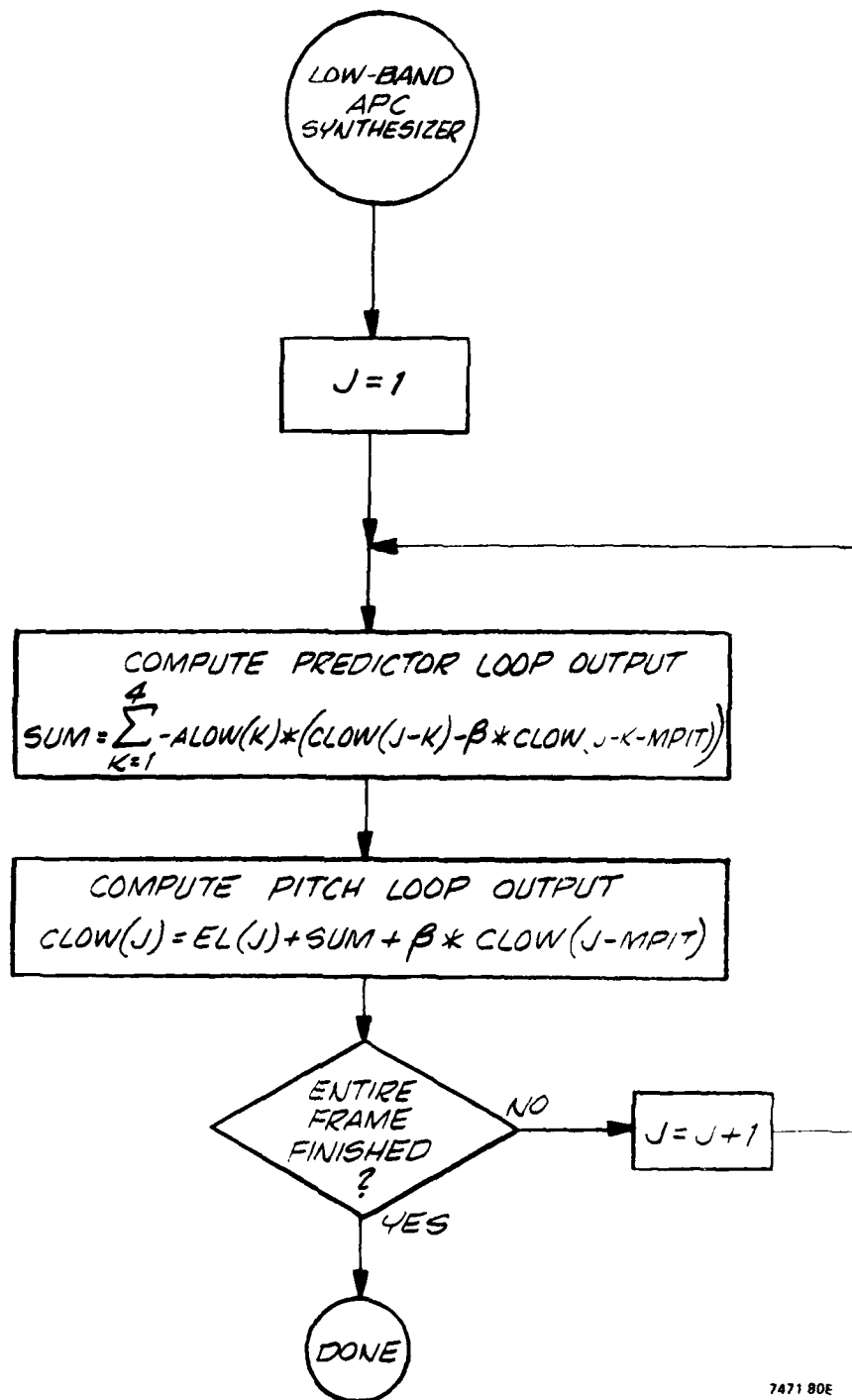
FIGURE 4.1.7 FLOW CHART OF LOW-BAND APC ANALYZER WITH NOISE SHARING



7472-80E

FIGURE 4.1.8  $KT$ -TH BLOCK ENCODING ROUTINE FOR (63, 45) BCH  
CODE IN 16 Kbps SBAPC SYSTEM

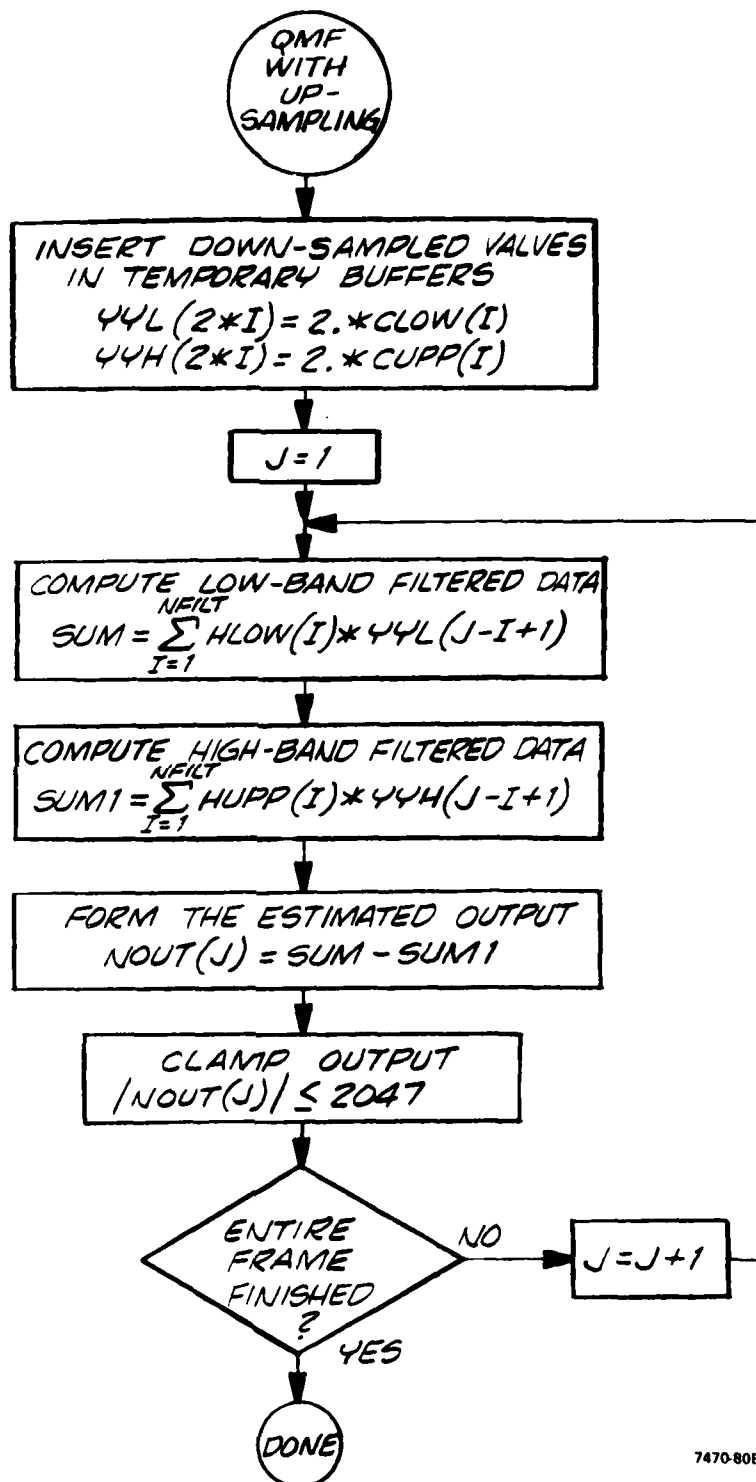
deserialized back to APC parameters. Then the received residual signals are fed into the APC synthesizers as shown in Figure 4.1.9 , and the estimates of the low band and high band waveforms are generated. These sub-band signals are filtered using quadrature mirror filters as illustrated in Figure 4.1.10. The difference between the low and high band creates a replica of the input.



7471 80E

FIGURE 4.1.9 FLOW CHART OF LOW-BAND APC SYNTHESIZER





7470-80E

FIGURE 4.1.10 FLOW CHART OF QMF WITH UP-SAMPLING

## 4.2 The User's Guide

### 4.2.1 Task Building

To build the loadable module of the SBAPC program, issue the following indirect command:

@ SBAPC

Operations performed by this indirect command file includes the compilation of all FORTRAN routines, the purging of older FORTRAN and OBJECT modules, and the task building of TSK module. The print-outs involving the task building of the SBAPC program are shown as follows:

```
>@SBAPC
>!      SBAPC.CMD
>!      AUG. 11, 1980
>!      CMD FILE TO COMPILE AND BUILD SBAPC PROGRAM AT 16 KBPS
>PIP *.FTN/PU
>PIP *.OBJ;*/PU
>F4P SBAPC=SBAPC/NOTR
>F4P TAPE2=TAPE2/NOTR
>F4P FFTRR8=FFTRR8/NOTR
>F4P SER=SER/NOTR
>F4P CESR=CESR/NOTR
>F4P BNSR=BNSR/NOTR
>F4P DSER=DSER/NOTR
>F4P GF2AMD=GF2AMD/NOTR
>F4P CONV=CONV/NOTR
>PIF SBAPC.TSK;*/DE
>TKB SBAPC,LP=SBAPC,SER,CESR,BNSR,DSER,GF2AMD,CONV,TAPE2,FFTRR8

>@ <EOF>
>
```

#### 4.2.2 Operating Procedures

After building the SBAPC.TSK module, the program can be started by issuing:

```
>RUN SBAPC
```

Print-outs of the actual running of the program for two situations (one with no noise suppression and one with noise suppression) are depicted in Figures 4.2.1 and 4.2.2.

RUN SBAPC

\*\*\* FORTRAN SIMULATION OF SBAPC \*\*\*

ENTER PROGRAM PARAMETERS:

NOISE SUPPRESSION FACTOR[0:MIN,15:MAX]=8

CHANNEL ERROR RATE(E15.8)=1.E-2

BEGINNING FRAME NUMBER(I4)= 1

ENDING FRAME NUMBER(I4)= 10

SIGNAL-TO-NOISE COMPUTATION: 0=YES 1=NO 0

IS THE INPUT ON MAG. TAPE? N

IS THE OUTPUT GOING TO MAG TAPE? N

OUTPUT FILE NAME= OUT.DAT

INPUT FILE NAME= VOICE.3KC

FR #=	1	SNR=	0.2177E+02DB	CSNR=	0.2177E+02	CH. ERRS	0	1	0	0	0	0
FR #=	2	SNR=	0.1259E+02DB	CSNR=	0.1718E+02	CH. ERRS	1	0	0	1	2	0
FR #=	3	SNR=	0.8408E+01DB	CSNR=	0.1426E+02	CH. ERRS	0	1	0	1	1	0
FR #=	4	SNR=	0.8371E+01DB	CSNR=	0.1278E+02	CH. ERRS	2	0	2	2	0	0
FR #=	5	SNR=	0.1591E+02DB	CSNR=	0.1341E+02	CH. ERRS	2	3	1	0	0	1
FR #=	6	SNR=	0.1555E+02DB	CSNR=	0.1377E+02	CH. ERRS	1	0	0	1	0	0
FR #=	7	SNR=	0.1806E+02DB	CSNR=	0.1438E+02	CH. ERRS	0	1	0	0	0	0
FR #=	8	SNR=	0.1340E+02DB	CSNR=	0.1426E+02	CH. ERRS	1	0	0	0	0	0
FR #=	9	SNR=	0.1818E+02DB	CSNR=	0.1469E+02	CH. ERRS	0	0	0	1	0	0
FR #=	10	SNR=	0.1182E+02DB	CSNR=	0.1441E+02	CH. ERRS	0	0	0	0	0	0

MISSION ACCOMPLISHED

FIGURE 4.2.1: PRINTOUTS OF SBAPC PROGRAM ( $\xi=0$ , BER=0)

>RUN SBAPC

\*\*\* FORTRAN SIMULATION OF SBAPC \*\*\*

ENTER PROGRAM PARAMETERS:

NOISE SUPPRESSION FACTOR(I0:MIN,15:MAX)=0

CHANNEL ERROR RATE(E15.8)=0

BEGINNING FRAME NUMBER(I4)= 1

ENDING FRAME NUMBER(I4)= 10

SIGNAL-TO-NOISE COMPUTATION: 0=YES 1=NO 0

IS THE INPUT ON MAG. TAPE? N

IS THE OUTPUT GOING TO MAG TAPE? N

OUTPUT FILE NAME= OUT.DAT

INPUT FILE NAME= VOICE.3KC

FR #=	1	SNR= 0.1787E+02DB	CSNR= 0.1787E+02	CH. ERRS	0	0	0	0	0	0
FR #=	2	SNR= 0.1435E+02DB	CSNR= 0.1611E+02	CH. ERRS	0	0	0	0	0	0
FR #=	3	SNR= 0.1190E+02DB	CSNR= 0.1471E+02	CH. ERRS	0	0	0	0	0	0
FR #=	4	SNR= 0.9367E+01DB	CSNR= 0.1337E+02	CH. ERRS	0	0	0	0	0	0
FR #=	5	SNR= 0.1379E+02DB	CSNR= 0.1346E+02	CH. ERRS	0	0	0	0	0	0
FR #=	6	SNR= 0.1672E+02DB	CSNR= 0.1400E+02	CH. ERRS	0	0	0	0	0	0
FR #=	7	SNR= 0.1901E+02DB	CSNR= 0.1472E+02	CH. ERRS	0	0	0	0	0	0
FR #=	8	SNR= 0.1371E+02DB	CSNR= 0.1459E+02	CH. ERRS	0	0	0	0	0	0
FR #=	9	SNR= 0.1770E+02DB	CSNR= 0.1494E+02	CH. ERRS	0	0	0	0	0	0
FR #=	10	SNR= 0.1028E+02DB	CSNR= 0.1447E+02	CH. ERRS	0	0	0	0	0	0

MISSION ACCOMPLISHED

FIGURE 4.2.2: PRINTOUTS OF SBAPC PROGRAM ( $\xi=7$ ,  $BER=10^{-2}$ )

## SECTION V

### CONCLUSIONS AND RECOMMENDATIONS

#### 5.1 Conclusions

This contract has resulted in the development of a high quality 16 Kb/s Split-Band Adaptive Predictive Coder (SBAPC) whose specifications are shown in Table 1-1. Based on our tradeoff analysis, the SBAPC system with separate pitch and short-term prediction loops performs better than the system with one combined loop. In the scheme with two loops, a 1st order pitch loop improves 2-3 dB signal-to-noise ratio as compared to the system without any pitch prediction. Though further improvement can be obtained with a 3rd order pitch predictor, the system is sometimes unstable at data rates below 12 KBPS. It is, therefore, recommended to use 1st order pitch prediction to always ensure the stability of the system. In contrast to the low band, the pitch information is not needed in the high band since this waveform contains little information about pitch. Our results also indicate that 4th order short-term predictors on both low and high bands represent a good compromise between the overhead bit rate and the quality of the processed speech. In addition, noise shaping algorithms have been found to be advantageous in SBAPC schemes. Particularly, Makhoul's second order all-zero noise shaping filter has resulted in slightly better quality speech as compared to that of the Atal's technique. As for the quantization of the residual signals, adaptive bit allocation of quantizer bits according to the energies of subbands yields further improvement in speech quality. Since these energies have to be sent to the receiver for quantization purposes, adaptive bit allocation does not require additional transmission of data.

Informal listening tests indicate that the SBAPC system yields much higher speech quality than that of CVSD in a back-to-back mode. Also, when

compared with other high quality 16 Kb/s algorithms, such as, adaptive transform coding (ATC), the SBAPC processed speech is slightly low-passed, but its smooth quality is much preferred over that of ATC with the noticeable "dish-washing" background noise. Furthermore, the SBAPC system has also shown to perform well in simulated tactical situations. With the help of 5 blocks of (63,45) BCH codes, the algorithm yields high processed speech quality even in the presence of  $10^{-2}$  channel error rate. In addition, the noise suppression routine in the SBAPC is capable of reducing background noise whose level is as high as -6 dB S/N which results in highly intelligible speech without the annoying noise components. Since the SBAPC is a modified version of adaptive predictive coding, it also tandems favorably with the 2.4 Kb/s linear predictive coder.

## 5.2 Recommendations

Based on our findings in this contract, the SBAPC algorithm can indeed replace the existing Continuously Variable Slope Deltamodulation scheme in future 16 Kb/s terminals. GTE strongly recommends that the SBAPC should be further studied and be implemented in real-time. In particular, the following areas should be pursued to enhance the performance and robustness of the algorithm:

- 1) segmental quantization of residual signals using pitch information
- 2) protection against channel errors with more efficient error-correcting codes
- 3) noise reduction with adaptive suppression factors

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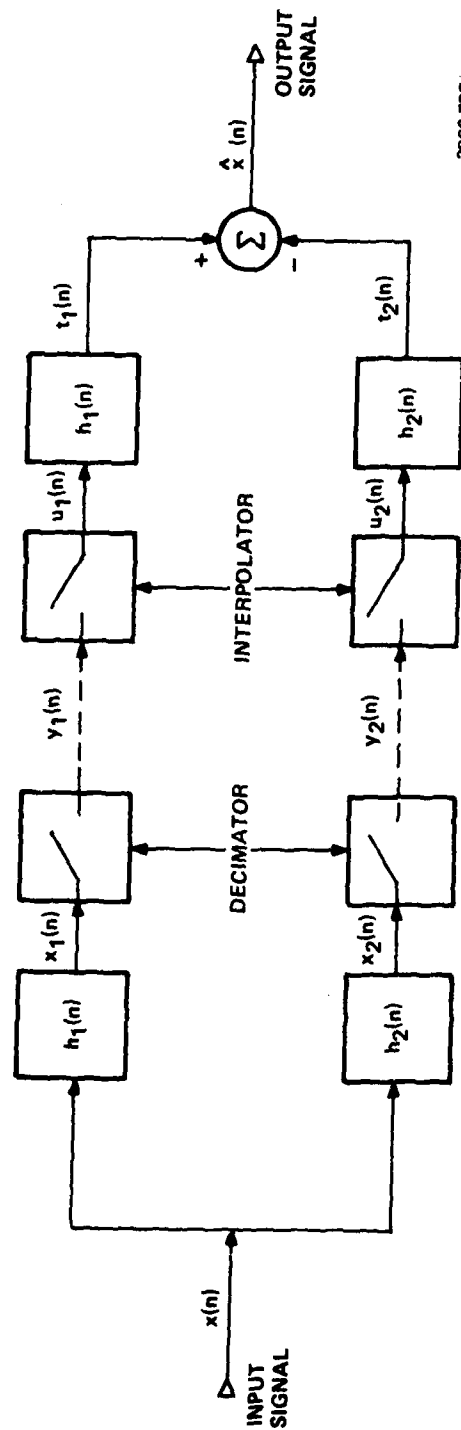
## Appendix A

### Theory of Quadrature Mirror Filters

One approach to band-split/reconstruct the input waveform is to make use of quadrature mirror filters (QMF) since the use of QMF design equations will achieve perfect splitting/reconstruction without large order filters. For explanatory purposes, consider the ideal splitting/reconstruction process described in Figure A.1. For this system, the following definitions apply:

- a.  $x(n)$  is a Nyquist band-limited signal with z-transform  $X(z)$ .
- b.  $h_1(n)$  is the impulse response of the low-pass filter the z-transform of which is  $H_1(z)$ .
- c.  $h_2(n)$  is the impulse response of the high-pass filter the z-transform of which is  $H_2(z)$ .
- d.  $y_1(n)$  is a baseband equivalent low-pass signal with z-transform  $Y_1(z)$ .
- e.  $y_2(n)$  is a baseband equivalent high-pass signal with z-transform  $Y_2(z)$ .

The signal,  $x(n)$ , is processed by filters  $h_1(n)$  and  $h_2(n)$  yielding the low-pass and high-pass equivalents,  $x_1(n)$  and  $x_2(n)$ , of the input signal. As their spectra occupy half the Nyquist bandwidth of the original signal, the sampling rate in each band can be halved by decimating (ignoring) every second sample. For reconstruction, the signals  $y_1(n)$  and  $y_2(n)$  are interpolated, by inserting one zero-valued sample every other time, and then filtered respectively by  $h_1(n)$  and  $h_2(n)$  before being added, to give the signal  $\hat{x}(n)$ . The dashed lines, shown in Figure A.1 represent the data passed to the communication channel(s) by the speech processing system.



3866-78E

FIGURE A.1 BAND-SPLITTING AND RECONSTRUCTION USING QMF

In order to minimize  $(\hat{x}(n) - x(n))$ , certain restrictions on the filters,  $h_1(n)$  and  $h_2(n)$ , must be met. We will derive these restrictions by constructing the transfer function of the QMF structure.

Using z-transform notation and referring to Figure A.1, we may write the intermediary filtered outputs as

$$X_1(z) = H_1(z) X(z) \quad (A-1)$$

and

$$X_2(z) = H_2(z) X(z) \quad (A-2)$$

The transforms of the decimated signals,  $y_1(n)$  and  $y_2(n)$ , and of the interpolated signals,  $u_1(n)$  and  $u_2(n)$ , are given by:

$$Y_1(z) = 1/2 [X_1(\tilde{z}) + X_1(-\tilde{z})] \quad , \quad \tilde{z} = z^{1/2} \quad (A-3)$$

$$Y_2(z) = 1/2 [X_2(\tilde{z}) + X_2(-\tilde{z})] \quad (A-4)$$

$$U_1(z) = Y_1(z^2) \quad (A-5)$$

$$U_2(z) = Y_2(z^2) \quad (A-6)$$

After the final filtering operation, the transforms of the reconstructed waveform components,  $t_1(n)$  and  $t_2(n)$ , are given by

$$T_1(z) = H_1(z) U_1(z) \quad (A-7)$$

$$T_2(z) = H_2(z) U_2(z) \quad (A-8)$$

Using the relations expressed in (A-1) through (A-6), the z-transforms can be rewritten as

$$T_1(z) = 1/2 [H_1(z) X(z) + H_1(-z) X(-z)] H_1(z) \quad (A-9)$$

$$T_2(z) = -1/2 [H_2(z) X(z) + H_2(-z) X(-z)] H_2(z) \quad (A-10)$$

The z-transform of the reconstructed waveform,  $\hat{x}(n)$ , is obtained by adding (A-9) and (A-10)

$$\hat{X}(z) = 1/2 [H_1^2(z) - H_2^2(z)] X(z) + 1/2 [H_1(-z) H_1(z) - H_2(-z) H_2(z)] X(-z) \quad (A-11)$$

If we assume that

$$H_2(z) = H_1(-z) \quad (A-12)$$

then the reconstructed waveform transform becomes

$$\hat{X}(z) = 1/2 [H_1^2(z) - H_1^2(-z)] X(z) \quad (A-13)$$

Evaluating  $z$  on the unit circle gives the Fourier transform of  $\hat{X}(z)$

$$\hat{X}(e^{j\omega T}) = 1/2 [H_1^2(e^{j\omega T}) - H_1^2(e^{j(\omega + \omega_s/2) T})] X(e^{j\omega T}) \quad (A-14)$$

For the case when  $h_1(n)$  is an even, symmetrical FIR filter of order  $N$ , then it can be shown that (A-14) reduces to

$$\hat{X}(e^{j\omega T}) = 1/2 e^{-j(N-1)\omega T} X(e^{j\omega T}) \quad (A-15)$$

where  $H_1^2(e^{j\omega T})$  exhibits an odd symmetric property about  $\omega_s/4$  and the half-power point  $H_1^2(\omega_s/4) = 0.5$ .

The inverse transform yields a perfectly reconstructed signal (no frequency distortion) with a gain factor of 1/2 and delay of  $N-1$  samples as shown by

$$\hat{x}(n) = 1/2 x(n - N + 1) \quad (A-16)$$

Therefore, we have shown that no guarantee perfect reconstruction of the original spectrum, the following filter constraints must be satisfied

$$h_1(n): \text{ symmetrical, even order} \quad (A-17)$$

$$H_2(z) = H_1(-z) \quad (A-18)$$

$$H_1^2(e^{j\omega T}) + H_1^2(e^{j(\omega + \frac{\omega_s}{2}) T}) = 1 \quad (A-19)$$

## APPENDIX B

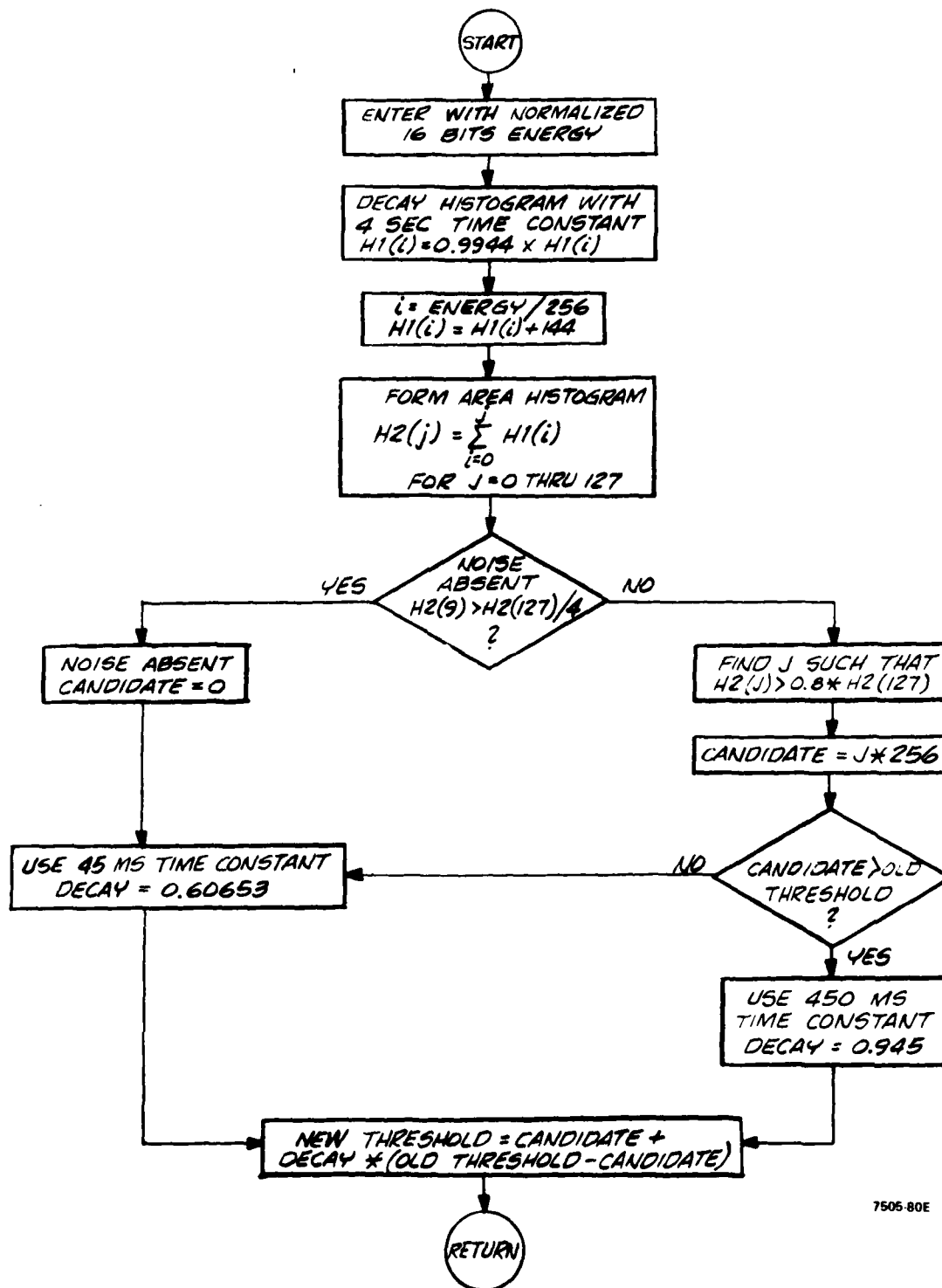
### Modified Robert's Noise Detection Algorithm

For all noise cancellation techniques, it is essential to obtain an accurate estimate of the statistics of the background noise. Hence, a noise detection algorithm is needed which considers only those frames of data which have a high probability of containing noise alone. In the modified Robert's algorithm, the boundary between noise and speech plus noise is established by monitoring the energy on a frame by frame basis and maintaining energy histograms which reflect the bimodal distribution (viz; one mode depicts the all noise state and one mode represents the speech plus noise state). The flow chart of the algorithm is shown in Figure B-1.

In this figure, the energy of the input speech is computed and normalized by a multiplication factor so that the maximum noise energy may vary around 32767. If the input energy does not exceed 16 bits (i.e., does not strongly imply the presence of speech), the algorithm updates the adaptive threshold. This routine first applies decay factor of 0.9944 to a 128-bin histogram of energy causing exponential decay of the histogram values with a time constant of 4 seconds. The value of the bin which encompasses the energy of the current frame is incremented by 144.

A second 128-point cumulative histogram is then formed to represent the area under the first histogram by computing the accumulated scores from the low energy bin to a high energy bin. If the 10th point of the second histogram exceeds 25% of the total area, it is assumed that there is no noise present (silence).

If noise is present, a search is made through the second histogram for the point which represents 80% of the total area. The quantum of energy



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FIGURE B-1 MODIFIED ROBERT'S NOISE DETECTION ALGORITHM



corresponding to this point becomes the new threshold candidate. If this candidate exceeds the current threshold, the threshold is updated using a decay factor of 0.945 (a slow time constant of 450 ms). If the candidate is below the current threshold, the threshold is updated with a decay factor of .60653 (a fast time constant of 45 ms).

If noise is absent, the new threshold candidate is set to zero, and the threshold is updated using a decay factor of .60653 (a fast time constant of 45 ms). Finally, the threshold is held to a minimum of 1024 to guarantee updating of the estimated noise components when background noise suddenly disappears.

## Appendix C Primitive BCH Codes

The BCH codes described in this appendix are cyclic codes that are well defined in terms of the roots of the generator polynomials [1]. These codes were discovered by Bose and Chaudhuri [2] - [3] and separately by Hocquenghem [4]. A binary  $(n,k)$  BCH code word consists of  $n$  symbols (bits in the binary case) where the first  $k$  bits are the information bits and the remaining  $r = n-k$  bits are redundant parity checks. It is convenient to represent code words with polynomials as

$$f(x) = f_0 + f_1x + \dots + f_{n-1}x^{n-1}, \quad f_i \in GF(2) \quad (C-1)$$

where each bit position is associated with a locator. If  $f(x)$  is a code word, then

$$f_1(x) = f_1 + f_2x + \dots + f_{n-1}x^{n-2} + f_0x^{n-1} \quad (C-2)$$

is also a codeword in a cyclic codes. In the primitive BCH code, which is the most convenient and powerful BCH code in theory and practice, the block length of the code may be defined as

$$n = 2^m - 1 \quad (C-3)$$

and with  $mt$  parity checks, it can correct any set of  $t$  independent errors within the block of  $n$  bits, where  $m$  and  $t$  are arbitrary positive integers [5]. This code may be described conveniently with the aid of finite Galois field theory introduced in Appendix D.

Let  $\alpha$  be a primitive element of the finite field  $GF(2^m)$ , then the primitive BCH code may be described as the set of polynomials such that

$$f(\alpha^i) = 0, i = 1, 3, 5, \dots, 2t - 1 \quad (C-4)$$

It is known in coding theory that these polynomials consist of all multiples of a single polynomial  $g(x)$ , known as the generator polynomial.

This polynomial also satisfies the equations as

$$g(\alpha^i) = 0, i = 1, 3, 5, \dots, 2t - 1 \quad (C-5)$$

These generator polynomials are tabulated in Table C-1 for the selected primitive BCH codes.

#### Encoding Procedures

Let the  $k$  information bits be represented by the polynomial  $d(x)$  as

$$d(x) = \sum_{i=0}^{k-1} d_i x^i \quad (C-6)$$

then, the code word of  $n$  bits may be expressed as

$$f(x) = x^{n-k} d(x) + r(x) \quad (C-7)$$

where  $r(x)$  is the remainder (parity check) obtained according to the following equation:

$$\frac{x^{n-k} d(x)}{g(x)} = q(x) + \frac{r(x)}{g(x)} \quad (C-8)$$

Block length n	k	t	Generator Polynomial
63	57	1	$g_1(x) = (6, 1, 0) = x^6 + x + 1$
	51	2	$g_3(x) = g_1(x) \cdot (6, 4, 2, 1, 0)$
	45	3	$g_5(x) = g_3(x) \cdot (6, 4, 2, 1, 0)$
127	120	1	$g_1(x) = (7, 3, 0) = x^7 + x^3 + 1$
	113	2	$g_3(x) = g_1(x) \cdot (7, 3, 2, 1, 0)$
	106	3	$g_5(x) = g_3(x) \cdot (7, 4, 3, 2, 0)$
255	247	1	$g_1(x) = (8, 4, 3, 2, 0) = x^8 + x^4 + x^3 + x^2 + 1$
	239	2	$g_3(x) = g_1(x) \cdot (8, 6, 5, 4, 2, 1, 0)$
	231	3	$g_5(x) = g_3(x) \cdot (8, 7, 6, 5, 4, 2, 0)$

TABLE C-1 GENERATOR POLYNOMIALS FOR SELECTED PRIMITIVE BCH CODES

where  $g(x)$  is the generator polynomial of the code. Therefore, encoding can be performed by the following procedures:

- 1). Calculate  $x^{n-k} d(x)$  by left shifting the information bits  $n-k$  times
- 2). Calculate the remainder (parity bits)  $r(x)$  from the division of  $x^{n-k} d(x)$  by  $g(x)$
- 3). Add the polynomial  $x^{n-k} d(x)$  and  $r(x)$  to form the code word

The procedures of 1) and 3) can be done simply by shifting and addition. However, the procedure of 2) is rather involved in computation if the actual division is performed to get the remainder. If the BCH code is specified and it is desired to speed up the processing time of 2), it is recommended to use a look-up table procedure for the calculation of the remainder from 2). The code word is then transmitted through the noisy channel, where the received code word may be altered depending on the introduction of channel errors.

#### Decoding Procedures

There are several algorithms for a decoding of BCH codes. Efficient decoding algorithms have been discovered for BCH codes [1] - [7]. The Berlekamp decoder is particularly attractive for powerful codes that provide for a good deal of error corrections (e.g., 10 or more). The Peterson algorithm, however, is more efficient for less powerful codes (e.g., the codes used in generalized burst trapping). In this decoding procedure, the problem of finding efficient solutions to the key decoding equation will be addressed by using the Peterson technique.

When a BCH code word  $\{f(x)\}$  is transmitted over a noisy channel, this code word may be corrupted by the channel, and what is received  $\{\gamma(x)\}$  can be different from the intended code word. Thus, the received word may be expressed as

$$\gamma(x) = f(x) + e(x) \quad (C-9)$$

where  $e(x)$  is the error polynomial which a decoder must compute to correct errors introduced by the channel. Let the received data be expressed in vector  $\gamma$  as

$$\gamma = [\gamma_0, \gamma_1, \dots, \gamma_{n-1}] \quad (C-10)$$

or its associated polynomial  $\gamma(x)$  by

$$\gamma(x) = \gamma_0 + \gamma_1 x + \dots + \gamma_{n-1} x^{n-1} \quad (C-11)$$

Denote each of the error location numbers by  $\beta_j$ ,  $j = 1, 2, \dots, t$ , then it is shown [1] that the power sums  $S_i$  can be expressed as

$$\begin{aligned} S_i &= \gamma(\alpha^i) \\ &= \sum_{j=1}^t \beta_j^i, \quad i = 1, 3, 5, \dots, 2t-1 \end{aligned} \quad (C-12)$$

In order to find the error locations, the Peterson procedures consist of three steps:

Step 1: Compute the power sums  $S_i$  from the received sequence through the relations

$$S_i = \gamma(\alpha^i), i = 1, 3, 5, \dots, 2t-1 \quad (C-13)$$

$$S_{2i} = S_i^2$$

Step 2: Compute the symmetric functions  $\sigma_k$ ,  $k = 1, 2, \dots, t$  from the power sums  $S_i$ , i.e.,

$$\begin{aligned} \sigma(x) &= x^t + \sigma_1 x^{t-1} + \dots + \sigma_{t-1} x + \sigma_t \\ &= (x + \beta_1) (x + \beta_2) \dots (x + \beta_t) \end{aligned} \quad (C-14)$$

and the  $\sigma_k$ 's may be obtained by the use of Newton's identities [1]

$$\underline{\sigma} = \begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \vdots \\ \sigma_t \end{bmatrix} \quad (C-15)$$

$$\begin{aligned} &= M_t^{-1} \underline{S} \\ &= \begin{bmatrix} 1 & 0 & 0 & 0 & \dots & 0 \\ S_2 & S_1 & 1 & 0 & \dots & 0 \\ \dots & & & & & \\ \dots & & & & & \\ S_{2t-2} & S_{2t-3} & S_{2t-4} & \dots & \dots & S_{t-1} \end{bmatrix}^{-1} \begin{bmatrix} S_1 \\ S_3 \\ \vdots \\ S_{2t-1} \end{bmatrix} \end{aligned}$$

If the determinant of  $M_t$  is singular, then reduce the error number  $t$  by 2 and proceed with it again.

Step 3: Find the error position locator  $\beta_j$ ,  $j = 1, 2, \dots, t$ , which is the roots of the polynomial  $\sigma(x)$  in eq. (C-14).

An efficient algorithm for calculating the  $\beta_j$ 's from eq. (C-14) has been developed by Chien [5], and all that remains to completely specify a binary BCH decoder is the computation of the coefficients of error locator polynomial,  $\sigma_j$ 's. As it is noted from eq. (C-15), the calculation of the  $\sigma_j$ 's involved matrix inversion which can be expressed analytically for the case  $t \leq 3$ . The results are:

For  $t = 1$ ,

$$\sigma_1 = S_1$$

For  $t = 2$ ,

$$\sigma_1 = S_1$$

$$\sigma_2 = (S_3 + S_1^3)/S_1$$

For  $t = 3$ ,

$$\sigma_1 = S_1$$

$$\sigma_2 = (S_1^2 S_3 + S_5)/(S_1^3 + S_3)$$

$$\sigma_3 = (S_1^3 + S_3) + S_1 \sigma_2$$

The calculation of the  $\sigma_j$ 's and the estimation of the error number are shown in Figure A1 for  $t = 3$ . The flowchart of Chien's search decoding



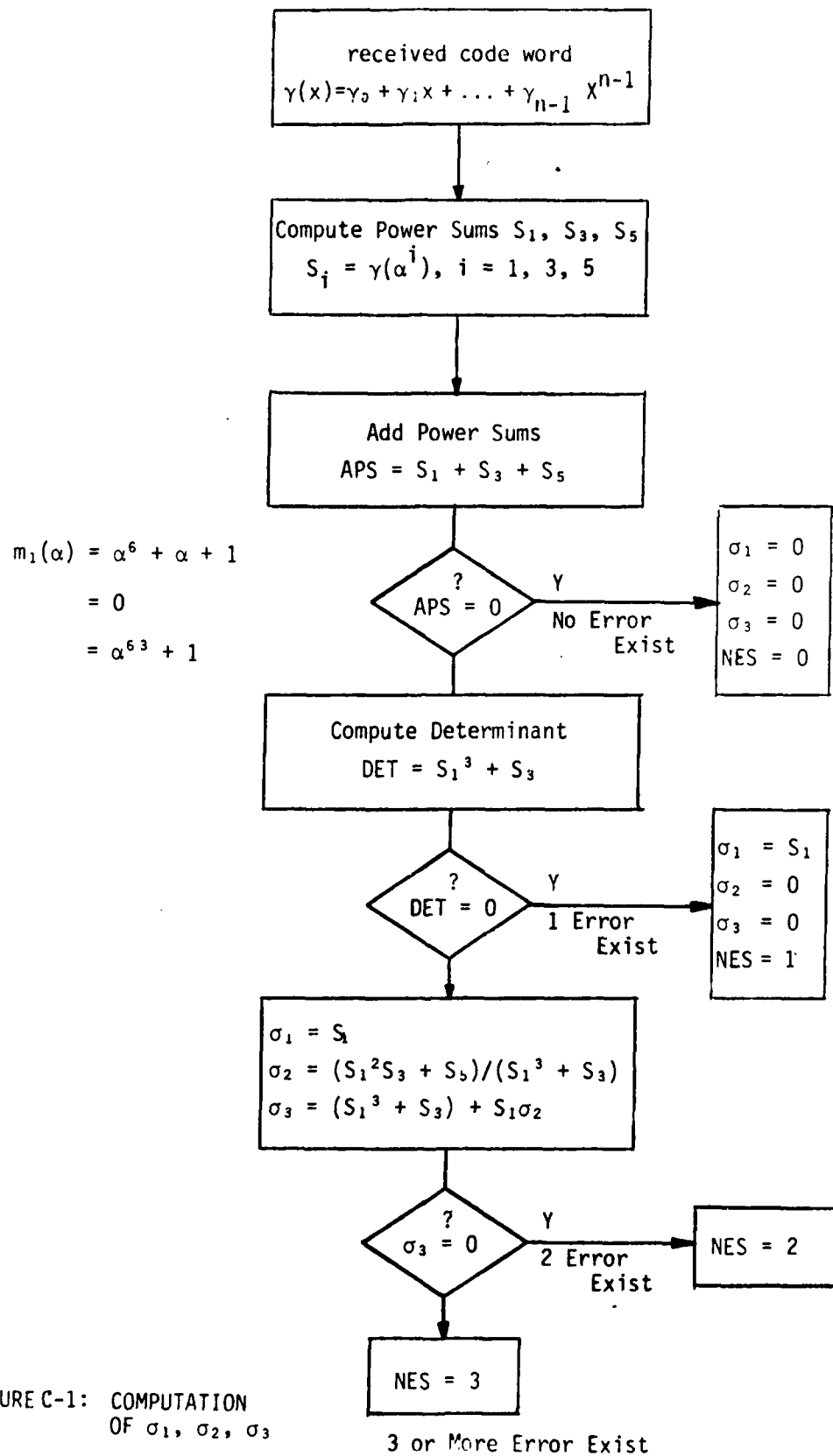


FIGURE C-1: COMPUTATION  
 OF  $\sigma_1, \sigma_2, \sigma_3$

procedure is shown in Figure C-2. This flowchart is for  $t = 3$ , i.e., the decoding algorithm can correct errors up to 3. One interesting observation in this decoding procedure is that the correction of errors may be performed erroneously if the number of errors in the block is greater than 3. Hence, the corrections may introduce additional channel errors. In order to avoid these additional errors, error corrections are made only when the estimated error number (NES in Figure C-1) equals to the measured error number (K in Figure C-2). This procedure eliminates most of the additional errors when more than 3 errors exist in the received word. In other words, the detection of errors more than 3 (i.e., 4, 5, 6, ..., etc.) is feasible in most of the cases. This fact contributes some improvements of the coder performance when the channel is very noisy (bit error rate  $\approx 10^{-2}$ ).

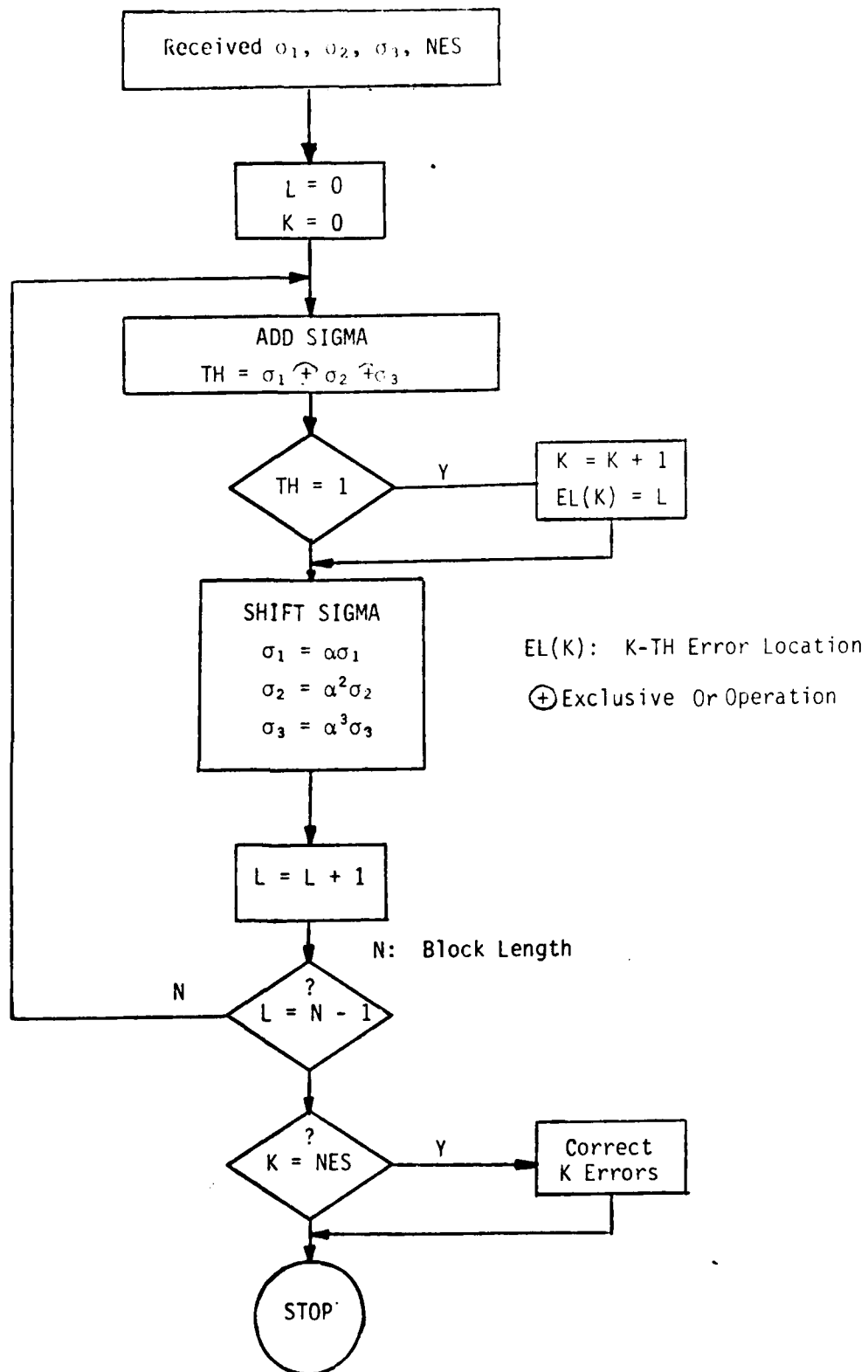


FIGURE C-2: CHIEN'S SEARCH DECODING PROCEDURE

References for Appendix C

- [1] Peterson, W. W., Error-Correcting Codes, The MIT Press, Cambridge, MA, 1961.
- [2] Bose, R. C. and D. K. Ray-Chandhuri, "On a Class of Error-Correcting Binary Group Codes," IEEE Trans. on Information and Control, Vol. IC-3, pp. 68-79, 1960.
- [3] Bose, R. C. and D. K. Ray-Chandhuri, "Further Results on Error-Correcting Binary Group Codes," IEEE Trans. on Information and Control, Vol. IC-3, pp. 279-290, 1960.
- [4] Hocquenghem, A., "Codes Correcteurs d'erreurs," Chiffres, Vol. 2, pp. 147-156, 1959.
- [5] R. T. Chien, "Cyclic Decoding Procedures for Bose-Chandhuri-Hocquenghem Codes," IEEE Trans. on Information Theory, Vol. IT-10, pp. 357-363, 1964.
- [6] E. R. Berlekamp, Algebraic Coding Theory, New York, McGraw-Hill, 1968.
- [7] J. L. Massey, "Shift-Register Synthesis and BCH Decoding," IEEE Trans. on Information Theory, Vol. IT-15, No. 1, pp. 122-127, 1969.

## Appendix D Operations in Galois Field

A Galois field is a finite set of elements that satisfy the axioms of a general field. Two operations (addition and multiplication) and their inverses are defined on the field elements. There is an identity element for each field element for both of the operations (0, 1) that is itself in the field. Also, both addition inverses and multiplication inverses are in the field. Finally, the rules of commutation and associativity are obeyed by the elements of the field.

Consider the following sixteen polynomials and their vector binary representations.

0	0000
1	0001
$1 + X$	0011
$1 + X + X^2$	0111
$1 + X + X^2 + X^3$	1111
$X$	0010
$X + X^2$	0110
$X + X^2 + X^3$	1110
$X^2$	0100
$X^2 + X^3$	1100
$X^3$	1000
$1 + X^3$	1001
$1 + X^2$	0101
$1 + X^2 + X^3$	1101
$X + X^3$	1010
$1 + X + X^3$	1011

As long as addition and multiplication of these polynomials is defined so that the axioms for the field are obeyed, then this will, in fact, be a Galois field of  $2^4$  elements ( $GF(2^4)$ ).

Addition is defined to be modulo 2. Each element is its own additive inverse and addition and subtraction of elements are the same.

Multiplication must be defined so that the product of two elements does not take us out of the field. For this reason, multiplication in a Galois field is not ordinary multiplication of polynomials. Rather, multiplication is defined modulo an irreducible polynomial, the primitive polynomial of the Galois field. For our field  $GF(2^4)$ , the primitive polynomial is  $1 + X + X^4$ . To generate the 16 vectors in the field, all one needs to do is to divide  $X^m$  where  $m = 0, 1, \dots, 14$  by the primitive polynomial.

0	-1	
1	0	
X	X	
X <sup>2</sup>	X <sup>2</sup>	
X <sup>3</sup>	X <sup>3</sup>	
X <sup>4</sup>	1 + X	$\frac{1}{1 + X + X^4} R[1 + X]$
X <sup>5</sup>	X + X <sup>2</sup>	$\frac{X}{1 + X + X^4} R[X + X^2]$
X <sup>6</sup>	X <sup>2</sup> + X <sup>3</sup>	$\frac{X^2}{1 + X + X^4} R[X^2 + X^3]$
X <sup>7</sup>	X <sup>3</sup> + X + 1	
X <sup>8</sup>	X <sup>2</sup> + 1	
X <sup>9</sup>	X <sup>3</sup> + X	
X <sup>10</sup>	X <sup>2</sup> + X + 1	
X <sup>11</sup>	X <sup>3</sup> + X <sup>2</sup> + 1	
X <sup>12</sup>	X <sup>3</sup> + X <sup>2</sup> + X + 1	
X <sup>13</sup>	X <sup>3</sup> + X <sup>2</sup> + 1	
X <sup>14</sup>	X <sup>3</sup> + 1	
X <sup>15</sup>	X <sup>0</sup> + 1	

It is now seen that the product of two binary vectors in the field is just the sum of their powers. The table repeats every fifteen powers so it is all done modulo 15.

$$x^i + x^j = x^{i+j} \pmod{15}$$

$$\frac{x^i}{x^j} = x^{i-j} \pmod{15}$$

APPENDIX E

LISTINGS OF FORTRAN PROGRAMS

```
!      SBAPC.CMD
!      AUG. 11, 1980
!      CMD FILE TO COMPILE AND BUILD SBAPC PROGRAM AT 16 KBPS
PIP *.FTN/PU
PIP *.OBJ;*/PU
F4P SBAPC,LP:=SBAPC/NOTR
F4P TAPE2,LP:=TAPE2/NOTR
F4P FFTRR8,LP:=FFTRR8/NOTR
F4P SER,LP:=SER/NOTR
F4P CESR,LP:=CESR/NOTR
F4P BNSR,LP:=BNSR/NOTR
F4P DSER,LP:=DSER/NOTR
F4P GF2AMD,LP:=GF2AMD/NOTR
F4P CONV,LP:=CONV/NOTR
PIP SBAPC.TSK;*/DE
TKB SBAPC,LP=SBAPC,SER,CESR,BNSR,DSER,GF2AMD,CONV,TAPE2,FFTRR8
```



```

C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
C      @                                     @
C      @           SBAPC.FTN               @
C      @                                     @
C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

```

```

C      FORTRAN PROGRAM TO SIMULATE THE SPLIT-BAND ADAPTIVE
C      PREDICTIVE CODING(SBAPC) AT 16 KBPS
C      STUDIED FOR DCA UNDER CONTRACT 100-79-C-0038
C      BY GTE PRODUCTS INC., NEEDHAM HEIGHTS, MASS.02194
C      DATE :OCT-6-80

```

```

C      TO BUILD THE TSK FILE, TYPE

```

```

C          @SBAPC

```

```

C      TO RUN THE PROGRAM, TYPE

```

```

C          RUN SBAPC

```

```

C      DEVICE ALLOCATIONS:      1=SBAPC PARAMETER FILE
C                                2=INPUT FOR TAPE2
C                                3=OUTPUT FOR TAPE2
C                                4=CHANNEL ERROR FILE
C                                5=KEY BOARD
C                                6=LINE PRINTER

```

```

0001      COMMON/MTAPE0/NIN(170),NOUT(170)
0002      COMMON/MTAPE1/NSKIP,IST,NTOTI,NTUPS,NTOTO
0003      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0004      COMMON/TBL/QTBL(457)
0005      COMMON/NSTBL/FNSTBL(50)
0006      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0007      COMMON/SDTA/MPIT,IBETA,IQQL,IQGH,IDPL(4),IDPH(4)
0008      COMMON/SW/ICOUNT,IPRSW
0009      DIMENSION XR(256),XI(256)
0010      DIMENSION HLOW(32),HUPP(32)
0011      DIMENSION YYH(288),YYL(288),CLOW(144),CUPP(144)
0012      DIMENSION PARLOW(5),PARUPP(5),ALOW(5),AUPP(5)
0013      DIMENSION RNL(144),RNH(144)
0014      DIMENSION XBUF(288),EL(72),EH(72)
0015      DIMENSION INBA(360),INB(63),NERB(6),INC(18)
0016      REAL OLP(32),LO(144),UP(144)
C      BITS ALLOCATIONS TO QUANTIZE SIDE INFORMATION
0017      DATA IBPT,IBBT,IBQL,IBQH,IBPL,IBPH/6,4,4*5,3,3,4,4,3,3/
C*****
C      I-O INTERACTION
C*****
C
0018      70      IKB=5

```

```

0019      IWR=6
          C      PRINT INTERMEDIATE RESULTS:      0=NO      1=PRINT
0020      ISW0=0
0021      ISW1=0
0022      IPRSW=0
          C
          C
0023      WRITE(IKB,200)
0024      200      FORMAT(///,20X,'*** FORTTRAN SIMULATION OF SBAPC ***',
          1//,10X,'ENTER PROGRAM PARAMETERS:')
          C
          C
          C      NOISE SUPPRESION FACTOR
          C
0025      WRITE(IKB,217)
0026      217      FORMAT(1H$,'NOISE SUPPRESSION FACTOR[0:MIN,15:MAX]=')
0027      READ(IKB,216)NSF
          C
          C      CHANNEL ERROR RATE
          C
0028      WRITE(IKB,213)
0029      213      FORMAT(1H$,'CHANNEL ERROR RATE(E15.8)=')
0030      READ(IKB,490)CERT
          C
          C
0031      WRITE(IKB,214)
0032      214      FORMAT(1H$,'BEGINNING FRAME NUMBER(I4)= ',3X)
0033      READ(IKB,216)LCOUNT
0034      WRITE(IKB,215)
0035      215      FORMAT(1H$,'ENDING FRAME NUMBER(I4)=',3X)
0036      READ(IKB,216)MCOUNT
0037      216      FORMAT(I6)
          C
0038      WRITE(IKB,242)
0039      242      FORMAT(1H$,'SIGNAL-TO-NOISE COMPUTATION:
          1 0=YES      1=NO',3X)
0040      READ(IKB,246)ISNR
0041      246      FORMAT(I1)
          C
          C
          C
          C
          C*****
          C      INITIALIZATION
          C*****
0042      LX=144
0043      NOL=18
0044      XP=FLOAT(NOL+1)
0045      LOCNT=1
0046      NFILT=32
0047      NFILT2=NFILT/2
0048      ILMX=3
0049      ILMN=1
0050      IQIL=406
0051      IQIH=432

```

```

0052          IRN=0
0053          JRN=0
0054          CSNR=0.
0055          KOUNT=0
0056          XSNR=0.
0057          Q1L=0.0
0058          Q2L=0.0
0059          Q1H=0.0
0060          Q2H=0.0
0061          DO 302 I=1,LTH
0062             RNL(I)=0.
0063             RNH(I)=0.
0064             LO(I)=0.
0065 302        UP(I)=0.
0066             DO 303 I=1,LX
0067                XBUF(I)=0.
0068                YYL(I)=0.
0069                YYH(I)=0.
0070                CUPP(I)=0.
0071 303        CLOW(I)=0.
0072             ICOUNT=0
          C
          C
          C*****
          C      MAG TAPE OR DISK I-O
          C*****
0073          NEND=0
0074          LTH=LX/2
0075          FLTH=LTH
0076          NTOTI=LX+NOL
0077          NTOTO=LX
0078          NTUPS=LX
0079          IST=1
0080          NSKIP=1
0081          NSKIPS=NSKIP
0082          NFILE=1
0083          CALL TAPE2(8)
          C
          C
          C*****
          C      READ IN PARAMETERS FOR FILTERS & QUANTIIZERS
          C*****
0084          CALL ASSIGN(1,'PARAM.DAT')
0085          DO 495 I=1,NFILT
0086 495        READ(1,490)HLOW(I)
0087 490        FORMAT(E15.8)
          C
          C
          C      INITIALIZE RANDOM NUMBER GENERATORS
0088          DO 491 I=1,457
0089             CALL RANDU(IRN,JRN,YQ)
0090             READ(1,493)QTBL(I)
0091 493        FORMAT(1X,E12.5)
0092 491        CONTINUE
          C
          C      READ NOISE SUPPRESSION TABLE

```

```

      C
0093      DO 497 I=1,NSF
0094      READ(1,493)(FNSTBL(J),J=1,50)
0095      497      CONTINUE
0096      CALL CLOSE(1)

      C
      C
      C
      C
      C*****
      C      DEFINITION OF SBAPC SYSTEM PARAMETERS
      C*****
0097      NLOW=4
0098      NUPP=4
0099      NNN=NLOW+1
0100      NNU=NUPP+1

      C
      C
      C***
      C      COMPUTE THE HIGH BAND IMPULSE RESPONSE
      C***
0101      DO 144 I=1,NFILT
0102      HUPP(I)=HLOW(I)*(-1)**(I-1)
      D      WRITE(IKB,143)HLOW(I),HUPP(I)
      D143    FORMAT(1X,'HLOW-HUPP',2(E15.8))
0103      144      CONTINUE

      C
      C
      C+++++
      C
      C      TRANSMITTER STARTS HERE
      C
      C+++++
      C
      C
      C*****
      C      DATA INPUT
      C*****
0104      1000     ICOUNT=ICOUNT+1
0105      CALL TAPE2(1)
0106      IF (NERR .NE. 0)GOTO 4900
      C      IF THE END OF TAPE IS REACHED,PROCESS 1 MORE FRAME
0107      IF(NEND .EQ. 0)GOTO 1014
0108      DO 1005 I=1,LX
0109      1005     NIN(I)=0
0110      1014     IF(ICOUNT .LT. LCOUNT)GOTO 1000
0111      IF(ICOUNT .GT. MCOUNT)GOTO 5000

      C
      C
0112      DO 1015 J=1,LX
0113      XBUF(LX+J)=NIN(J)
0114      1015     CONTINUE

      C
      C*****
      C      SUPPRESS BACKGROUND NOISE IF DESIRED
      C*****

```

```

      C
0115      IF(NSF.EQ.0)GO TO 8100
      C
      C      PASS THROUGH THE NOISE SUPPRESSION FILTER
      C
0116      CALL MRNSA(XR,XI,NTOTI,NSF)
      C
0117      DO 8040 I=1,NTOTI
0118      XBUF(LX+I)=XR(I)
0119      8040 CONTINUE
      C
      C      INTERPOLATE FRAME BOUNDARY
      C
0120      DO 8020 I=1,NOL
0121      F1=FLOAT(I)/XP
0122      F2=1.-F1
0123      XBUF(LX+I)=XBUF(LX+I)*F1+F2*OLP(I)
0124      8020 OLP(I)=XR(LX+I)
      CCC
      C
0125      8100 CONTINUE
      C***
      C      BANDPASS FILTERING WITH QUADRATURE MIRROR FILTERS
      C***
0126      DO 1101 J=1,LX
0127      FF=0.
0128      GG=0.
0129      DO 1100 I=1,NFILT
0130      FF=FF+HLOW(I)*XBUF(LX+J-I+1)
0131      GG=GG+HUPP(I)*XBUF(LX+J-I+1)
0132      1100 CONTINUE
0133      KK=J/2
0134      JJ=KK*2
0135      IF(JJ.NE. J)GOTO 1101
0136      LO(LTH+KK)=FF
0137      UP(LTH+KK)=GG
0138      1101 CONTINUE
      C
      C
      C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
      C      @
      C      @          LOW BAND ENCODING          @
      C      @
      C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
      C
      C
      C      COMPUTE THE ACF OF INPUT
      C
0139      DO 1105 M=1,64
0140      XR(M)=0.
0141      LTR=LTH-M+1
0142      DO 1105 I=1,LTR
0143      1105 XR(M)=XR(M)+LO(LTH+I)*LO(LTH+I+M-1)
      C
      C
      C      FIND PITCH NUMBER SKIPPING UNVOICED FRAMES

```

```

C
0144      TERM=0.0
0145      TERM1=0.0
0146      XLG=0.0
0147      MPIT=0
0148      ISLOPE=1
0149      IF(IPITL.EQ.1.OR.XR(1).LE.1)GO TO 2047
0150      DO 2040 I=8,64
0151      IF(XR(I) .LT. 0)ISLOPE=-1
0152      IF(ISLOPE.EQ. 1.OR.XR(I).LE.XLG)GOTO 2040
0153      MPIT=I-1
0154      XLG=XR(I)
0155      2040  CONTINUE
C
C
C*****
C      CALCULATE FEEDBACK GAIN IN PITCH LOOP
C*****
0156      DO 2045 J=1,LTH
0157      TERM1=TERM1+LO(LTH+J)*LO(LTH+J-MPIT)
0158      2045  TERM=TERM+LO(LTH+J-MPIT)**2
0159      2047  BETA=0.
0160      IF(TERM .NE.0)BETA=TERM1/TERM
C
CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
C
D      WRITE(IKB,2048)IBBT,BETA,IBETA
C
CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
C
C
C      QUANTIZE BETA
0161      IQI=1
0162      CALL QTZ(IQI,IBBT,BETA,IBETA)
C
CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
D      WRITE(IKB,2048)IBBT,BETA,IBETA
0163      2048  FORMAT(10X,'IBBT-BETA-IBETA:',I3,E15.8,I6)
CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
C
C*****
C      COMPUTE THE REDUCED WAVEFORM
C*****
0164      IF(MPIT .EQ. 0)BETA=0.
0165      DO 2100 J=1,LTH
0166      XI(J)=LO(LTH+J)-BETA*LO(LTH+J-MPIT)
0167      2100  CONTINUE
C
C
C
C*****
C      COMPUTE ACF FROM THE REDUCED WAVEFORM
C*****
C
0168      DO 2111 I=1,NNN
0169      XR(I)=0.0

```

```

0170      ITR=LTH-I+1
0171      DO 2111 J=1,ITR
0172      2111  XR(I)=XR(I)+XI(J)*XI(I+J-1)
           C
           C
           C      NORMALIZE ACF
           C
0173      R0=XR(1)
0174      IF(R0 .LE. 0)R0=1.
0175      DO 2200 I=1,NNN
0176      2200  XR(I)=XR(I)/R0
           C*****
           C      COMPUTE SPECTRAL PREDICTION COEFFICIENTS
           C*****
           C
0177      CALL NR2NAP(ALOW,XR,NLOW,U,PARLOW)
           C
           C
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           D      DO 2204 I=1,NLOW
           D      WRITE(IKB,2205)IBPL(I),PARLOW(I),IDPL(I),ALOW(I)
           D2204  CONTINUE
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           C
           C      QUANTIZE LOW BAND PARCORS
0178      CALL QTPCRL(PARLOW)
           C
           C
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           D      DO 2206 I=1,NLOW
           D      WRITE(IKB,2205)IBPL(I),PARLOW(I),IDPL(I),ALOW(I)
           D2205  FORMAT(20X,'IBPL-PARLOW-IDPL-ALOW:',I3,E15.8,I6,E15.8)
           D2206  CONTINUE
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           C
           C*****
           C      CONVERT PARCORS BACK TO PREDICTOR COEFS
           C*****
0179      CALL PARPRE(NLOW,PARLOW,ALOW)
           C
           C
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           D      DO 2207 I=1,NLOW
           D      WRITE(IKB,2208)ALOW(I)
           D2208  FORMAT(30X,E15.8)
           D2207  CONTINUE
           CDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD
           C
           C*****
           C      CALCULATE GAIN
           C*****
           C
0180      QQL=SQRT(R0*PARLOW(NNN)/FLTH)
0181      IF(QQL .LE. 1.0)QQL=1.0
0182      QQL=ALOG(QQL)/ALOG(2.0)
           C

```

E-9



E-10

```

0213      RL1=ALOW(1)
0214      RL2=ALOW(2)
0215      DO 4522 K=1,NLOW
0216      K1=K+1
0217      K2=K+2
0218      TR=ALOW(K)
0219      TR1=0.0
0220      TR2=0.0
0221      IF(K1.LE.NLOW)TR1=ALOW(K1)
0222      IF(K2.LE.NLOW)TR2=ALOW(K2)
0223      RL0=RL0+TR**2
0224      RL1=RL1+TR*TR1
0225      RL2=RL2+TR*TR2
0226      4522  CONTINUE
0227      DETL=RL0**2-RL1**2
0228      IF(DETL.GT.1.E-5)GO TO 4524
0229      QQL=1.E-6
0230      GOTO 4530
0231      4524  B1L=RL1*(RL2-RL0)/DETL
0232      B2L=(RL1**2-RL0*RL2)/DETL
          C
          C*****
          C      HIGH BAND NOISE SHAPING
          C*****
0233      4530  CONTINUE
          C
0234      B1H=0.0
0235      B2H=0.0
          C
          C      CALCULATE ACF OF THE HIGH-BAND PREDICTION COEFFICIENT
0236      RH0=1.0
0237      RH1=AUPP(1)
0238      RH2=AUPP(2)
0239      DO 4544 K=1,NUPP
0240      K1=K+1
0241      K2=K+2
0242      TR=AUPP(K)
0243      TR1=0.0
0244      TR2=0.0
0245      IF(K1.LE.NUPP)TR1=AUPP(K1)
0246      IF(K2.LE.NUPP)TR2=AUPP(K2)
0247      RH0=RH0+TR**2
0248      RH1=RH1+TR*TR1
0249      RH2=RH2+TR*TR2
0250      4544  CONTINUE
0251      DETH=RH0**2-RH1**2
0252      IF(DETH.GT.1.E-5)GO TO 4555
0253      QQL=1.E-6
0254      QQH=1.E-6
0255      GOTO 4015
          C
          C
0256      4555  B1H=RH1*(RH2-RH0)/DETH
0257      B2H=(RH1**2-RH0*RH2)/DETH
          C
0258      4015  CONTINUE

```

```

C
C*****
C      CODING THE LOW-BAND:
C      GENERATE THE TRUE ERROR SIGNAL WITH QUANTIZER IN LOOP
C*****
C
C
C
0259      QLEVL=QQL
0260      DO 2109 J=1,LTH
0261      SUM=0.
0262      DO 2108 K=1,NLOW
0263      TERM=-ALOW(K)*(RNL(LTH+J-K)-BETA*RNL(LTH+J-K-MPIT))
0264      SUM=SUM+TERM
0265      SUM=SUM+BETA*RNL(LTH+J-MPIT)
0266      EL(J)=LO(LTH+J)-SUM+B1L*Q1L+B2L*Q2L
0267      XIN=EL(J)/QLEVL
0268      IQI=IQIL
0269      IF(IBIL.GE.1)CALL ERSQTZ(IQI,IBIL,XIN,XOUT,IDOT)
0270      NIN(J)=IDOT
0271      EL(J)=XOUT*QLEVL
0272      QL=(XOUT-XIN)*QLEVL
0273      Q2L=Q1L
0274      Q1L=QL
0275      2107 RNL(LTH+J)=SUM+EL(J)
0276      2109 CONTINUE
C
C
C
C
C*****
C      CODING THE HIGH-BAND
C      GENERATE THE ERROR SIGNAL WITH QUANTIZER IN LOOP
C*****
0277      QLEVH=QQH
0278      DO 3050 J=1,LTH
0279      SUM=0.
0280      DO 3040 K=1,NUPP
0281      TERM=-AUPP(K)*RNH(LTH+J-K)
0282      SUM=SUM+TERM
0283      EH(J)=UP(LTH+J)-SUM+B1H*Q1H+B2H*Q2H
0284      XIN=EH(J)/QLEVH
0285      IQI=IQIH
0286      IF(IBIH.GE.1)CALL ERSQTZ(IQI,IBIH,XIN,XOUT,IDOT)
0287      NIN(J+72)=IDOT
0288      EH(J)=XOUT*QLEVH
0289      QH=(XOUT-XIN)*QLEVH
0290      Q2H=Q1H
0291      Q1H=QH
0292      3050 RNH(LTH+J)=EH(J)+SUM
C
C
C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
C      @
C      @      FOR DEBUGGING ONLY      @
C      @

```

```

C      @
C      @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
0293      IF(IPRSW.NE.1)GO TO 8444
C      PRINT TRANSMITTER DATA
C
0294      WRITE(5,8410)ICOUNT,MPIT,IBIL,IBIH
0295      8410      FORMAT(1X,'FR=',I6,3X,3I6)
0296      WRITE(5,8420)QQL,QQH,BETA,(PARLOW(KK),KK=1,4),(PARUPP(N),N=1,4)
0297      WRITE(5,8430)IQQL,IQQH,IBETA,(IDPL(KK),KK=1,4),(IDPH(N),N=1,4)
0298      8420      FORMAT(10X,11E11.4)
0299      8430      FORMAT(10X,11(I6,5X))
C      DO 8222 K=1,72
C      WRITE(5,8333)K,EL(K),EH(K),NIN(K),NIN(K+72)
C      8222      CONTINUE
0300      8333      FORMAT(1X,'EL(',I3,')=',E11.4,3X,E11.4,3X,2I6)
C
C
C
C
C*****
C      SERIALIZATION OF PARAMETERS
C*****
0301      8444      CONTINUE
0302      CALL SER(INBA,INB,IBIL)
0303      IF(IPRSW.EQ.1)WRITE(5,8450)(INBA(K),K=1,360)
C
C
C+++++
C
C      RECEIVER STARTS HERE...
C
C+++++
C*****
C      BCH CODE ENCODER
C*****
C
C      ENCODE 5 BLOCK
C
0304      DO 8447 KT=1,5
0305      CALL ENCBCH(INBA,INB,INC,KT)
0306      8447      CONTINUE
C
C
C      PRINT INPUT BINARY DATA IF DESIRED
C
C      IF(IPRSW.EQ.1)WRITE(5,8450)(INBA(K),K=1,360)
0307      8450      FORMAT(60I2)
C
C
C
C      *** END OF TRANSMITTER ***
C
C
C*****
C      CHANNEL ERROR SIMULATOR
C*****

```

```

C
0308      CALL CEIR(INBA,360,CERT,IRN,JRN,NERB,5)
C
C      PRINT BINARY DATA IF DESIRED
C
C      IF(IPRSW.EQ.1)WRITE(5,8450)(INBA(K),K=1,360)
C
C
C*****
C      BCH CODE DECODER
C*****
C      DECODE 5 BLOCK OF BCH CODE
C
0309      JSP=0
0310      DO 9700 KT=1,5
0311      CALL DECBCH(INBA,INB,KT,NES)
0312      IF(KT.EQ.1.AND.NES.EQ.4)JSP=1
0313      9700 CONTINUE
C
C
C      PRINT INPUT BINARY DATA IF DESIRED
C
0314      IF(IPRSW.EQ.1)WRITE(5,8450)(INBA(K),K=1,360)
C
C      SKIP ONE FRAME SYNTHESIS IF BURST ERRORS(MORE THAN 4 ERRORS) ARE LE
C      IN THE 1ST BLOCK(SIDE INFORMATION)
0315      IF(JSP.EQ.1)GO TO 8558
C
C*****
C      DESERIALIZE BINARY DATA INTO DECIMAL NUMBER AND DEQUANTIZE
C*****
C
0316      CALL DSER(INBA,INB,QQL,QQH,IBIL,IBIH,ILMX,ILMN)
C
C      IF(IPRSW.EQ.1)
C      1 WRITE(IKB,8430)IBETA,IQQL,IQQH,(IDPL(K),K=1,4),(IDPH(J),J=1,4)
C
C      DEQUANTIZE SBAPC PARAMETERS
C
C      MPIT DOES NOT REQUIRE DEQUANTIZATION SINCE IBPT=6
C
C      DEQUANTIZE BETA
C
0317      IQI=1
0318      CALL DEQTZ(IQI,IBETA,BETA)
0319      IF(MPIT.EQ.0)BETA=0.0
C
C      IF(IPRSW.EQ.1)
C      1 WRITE(IKB,2048)IBBT,BETA,IBETA
C
C      DEQUANTIZE LOWBAND PARCOR COEFS
C
0320      IQI=158
0321      CALL DQTPCR(IQI,PARLOW)
C

```

E-15

E-16

```

0365      SNRNUM=0.
0366      SNRDEN=0.
0367      DO 4100 I=1,LX
0368      SNRNUM=SNRNUM+(XBUF(I+LX+1-NFILT))**2
0369      4100 SNRDEN=SNRDEN+(XBUF(I+LX+1-NFILT)-XR(I))**2
0370      IF(SNRDEN .EQ. 0 .OR. SNRNUM .EQ. 0.)GOTO 4115
0371      SSNR=10.*ALOG10(SNRNUM/SNRDEN)
0372      GOTO 4120
0373      4115 SSNR=0.
0374      WRITE(IKB,4117)ICOUNT
0375      4117 FORMAT(1X,'FRAME NO.=',I4,'ENERGY OF INPUT SIGNAL=0.')
0376      4120 XSNR=XSNR+SSNR
0377      CSNR=XSNR/FLOAT(KOUNT)
0378      WRITE(IKB,4122)ICOUNT,SSNR,CSNR,(NEKB(L),L=1,6)
0379      4122 FORMAT(1X,'FR #=',I4,4X,'SNR=',E11.4,'DB',
1          3X,'CSNR=',E11.4,3X,'CH. ERRS',6I3)
C
C
C
C*****
C      THIS SHIFTS THE DATA FOR NEXT TIME
C*****
C
0380      4402 CONTINUE
0381      DO 4403 I=1,LX
0382      XBUF(I)=XBUF(I+LX)
0383      YYL(I)=YYL(I+LX)
0384      4403 YYH(I)=YYH(I+LX)
C
C
0385      DO 4404 J=1,LTH
0386      LO(J)=LO(LTH+J)
0387      UP(J)=UP(LTH+J)
0388      RNL(J)=RNL(LTH+J)
0389      RNH(J)=RNH(J+LTH)
0390      CLOW(J)=CLOW(J+LTH)
0391      CUPP(J)=CUPP(J+LTH)
0392      4404 CONTINUE
C
C
C***
C      CONTINUE PROCESSING IF END OF TAPE IS NOT READ
C***
0393      IF(NEND .EQ. 0)GOTO 1000
C
0394      GOTO 5000
C
C
C
C****
C      ERROR DIAGNOSTICS
C****
0395      4900 WRITE(IKB,4910)
0396      4910 FORMAT(1X,'ERROR ENCOUNTERED DURING TAPE READ'//)
0397      GOTO 70
C
C
C

```



```

C*****
C      WRITES THE END OF FILE
C*****
0398    5000    CONTINUE
0399          DO 5001 I=1,LX
0400    5001    NOUT(I)=0
0401          DO 5002 I=1,32
0402    5002    CALL TAPE2(2)
0403          CALL TAPE2(5)
0404          WRITE(IKB,5109)
0405    5109    FORMAT(1X,'MISSION ACCOMPLISHED'//)
0406          STOP
0407          END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
\$CODE1	011762 2553	RW,I,CON,LCL
\$PDATA	000056 23	RW,D,CON,LCL
\$IDATA	001334 366	RW,D,CON,LCL
\$VARS	025664 5594	RW,D,CON,LCL
\$TEMPS	000006 3	RW,D,CON,LCL
MTAPE0	001250 340	RW,D,OVR,GBL
MTAPE1	000012 5	RW,D,OVR,GBL
MTAPE2	000012 5	RW,D,OVR,GBL
TBL	003444 914	RW,D,OVR,GBL
NSTBL	000310 100	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL
SW	000004 2	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 046622 9929

## PROGRAM SECTIONS

TOTAL SPACE ALLOCATED = 000604 194

```

C
C
C      SUBROUTINE PARPRE,FTN
C      THIS ROUTINE CONVERTS PARCOR COEFS TO PREDICTION COEFS
C      THE RESULTING A'S SHOULD BE NEGATED IF
C      (1-SUM(A(I)*Z**(-I)) IS USED AS THE PREDICTION POLYNOMIAL
C
0001      SUBROUTINE PARPRE(N,PARCOR,A)
0002      DIMENSION PARCOR(1),A(1),AP(10)
0003      A(1)=-PARCOR(1)
0004      NN=N+1
0005      PARCOR(NN)=1.0-A(1)**2
0006      DO 120 I=2,N
0007      IM1=I-1
0008      DO 110 J=1,IM1
0009      110      AP(J)=A(J)-PARCOR(I)*A(I-J)
0010      AP(I)=-PARCOR(I)
0011      PARCOR(NN)=PARCOR(NN)*(1.0-AP(I)**2)
0012      DO 140 J=1,I
0013      140      A(J)=AP(J)
0014      120      CONTINUE
C      TYPE 997,(I,A(I),I=1,N)
C997      FORMAT(1X,'A(',I2,')= ',E15.8)
0015      RETURN
0016      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000372 125	RW,I,CON,LCL
SIDATA	000024 10	RW,D,CON,LCL
SVARS	000060 24	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000502 161

```

      C
      C
      C      SUBROUTINE QTPCRL
      C      QUANTIZE PARAMETERS OF LOW BAND PARCORS IN SBAPC
      C
0001      SUBROUTINE QTPCRL(PCRL)
0002      COMMON/TBL/QTBL(457)
0003      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0004      COMMON/SDTA/MPIT,IBETA,IQQL,IQQH,IDPL(4),IDPH(4)
0005      DIMENSION PCRL(1)

      C
      C      PCRL(1,2) WITH 5 BITS
      C      PCRH(1,2) WITH 4 BITS
      C      PCRL(3,4),PCRH(3,4) WITH 3 BITS
      C
      C      QUANTIZE PARCOR IN LOW BAND
0006      IQS=158
0007      IQI=IQS
0008      DO 110 I=1,4
0009      IBT=IBPL(I)
0010      CALL QTZ(IQI,IBT,PCRL(I),IDP)
0011      IDPL(I)=IDP
0012      IQS=IQS+15
0013      IF(IBPL(I).GE.4)IQS=IQS+16
0014      IF(IBPL(I).GE.5)IQS=IQS+32
0015      IQI=IQS
0016      110 CONTINUE
0017      RETURN
0018      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000216 71	RW,I,CON,LCL
SIDATA	000024 10	RW,D,CON,LCL
SVARS	000012 5	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 004002 1025

NO FPP INSTRUCTIONS GENERATED

```

      C
      C
      C      SUBROUTINE QTPCRH
      C      SUBROUTINE TO QUANTIZE HIGH BAND PARCOR IN SBAPC
      C
0001      SUBROUTINE QTPCRH(PCRH)
0002      COMMON/TBL/QTBL(457)
0003      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0004      COMMON/SDTA/MPIT,IBETA,IQQL,IQQH,IDPL(4),IDPH(4)
0005      DIMENSION PCRH(1)

      C
      C      QUANTIZE PARCOR IN UPPER BAND
      C
0006      IQS=314
0007      IQI=IQS
0008      DO 210 I=1,4
0009      IBT=IBPH(I)
0010      CALL QTZ(IQI,IBT,PCRH(I),IDP)
0011      IDPH(I)=IDP
0012      IQS=IQS+15
0013      IF(IBPH(I).GE.4)IQS=IQS+16
0014      IQI=IQS
0015      210 CONTINUE
0016      RETURN
0017      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000202 65	RW,I,CON,LCL
SIDATA	000024 10	RW,D,CON,LCL
SVARS	000012 5	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003766 1019

NO FPP INSTRUCTIONS GENERATED

```

      C      QTZ.FTN
      C      SUBROUTINE  TO QUANTIZE SIDE INFORMATION OF SBAPC SYSTEM
      C
0001      SUBROUTINE QTZ(IQI,IBT,XX,ID)
0002      COMMON/TBL/QTBL(457)
0003      ID=0
0004      IF(IBT.LE.0)GO TO 20
0005      IQIT=2**IBT-1
0006      DO 10 J=1,IQIT
0007      ID=J-1
0008      IF(XX.LT.OTBL(IQI+1))GO TO 20
0009      IQI=IQI+2
0010      10  CONTINUE
0011      ID=ID+1
0012      20  XX=QTBL(IQI)
0013      RETURN
0014      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000154 54	RW,I,CON,LCL
SVARS	000004 2	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003624 970

```

      C      DEQTZ.FTN
      C
      C      DEQUANTIZE SBAPC PARAMETERS
0001      SUBROUTINE DEQTZ(IQI,ID,XX)
0002      COMMON/TBL/QTBL(457)
      C      IQI:INPUT TABLE POINTER
      C      ID=DECIMAL INPUT VALUE
      C      XX:DEQUANTIZED OUTPUT VALUE
0003      IQ=IQI+2*ID
0004      XX=QTBL(IQ)
0005      RETURN
0006      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
\$CODE1	000036 15	RW,I,CON,LCL
SVARS	000002 1	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003504 930

```

      C      ERSQTZ.FTN
      C      SUBROUTINE TO QUANTIZE ERROR SIGNALS
      C      DATE 7/31/80
0001      SUBROUTINE ERSQTZ(IQI,IBIT,XIN,XOUT,IDOT)
0002      COMMON/TBL/QTBL(457)
0003      IF(IBIT.GE.2)IQI=IQI+1
0004      IF(IBIT.GE.3)IQI=IQI+3
0005      IF(IBIT.GE.4)IQI=IQI+7
0006      XOUT=ABS(XIN)
0007      IBT=IBIT-1
0008      IMK=2**IBT
0009      CALL QTZ(IQI,IBT,XOUT,IDOT)
0010      IF(XIN.GE.0.0)RETURN
0011      XOUT=-XOUT
0012      IDOT=IDOT+IMK
0013      RETURN
0014      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000200 64	RW,I,CON,LCL
SIDATA	000012 5	RW,D,CON,LCL
SVARS	000004 2	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003662 985



```

C      DQTPCR.FTN
C      SUBROUTINE DEQUANTIZE PARCOR PARAMETERS
C
C      AUG. 4, 1980
C
0001      SUBROUTINE DQTPCR(IQIP,PCR)
0002      COMMON/TBL/QTBL(457)
0003      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0004      COMMON/SDTA/MPIT,IBETA,IQQL,IQQH,IDPL(4),IDPH(4)
0005      DIMENSION PCR(1)
0006      IQI=IQIP
0007      DO 10 I=1,4
0008      IF(IQIP.EQ.314)GO TO 11
0009      IDP=IDPL(I)
0010      CALL DEQTZ(IQI,IDP,PCR(I))
0011      IBIT=IBPL(I)
0012      GO TO 12
C      DEQUANTIZE FOR HIGH BAND
0013      11 CONTINUE
0014      IDP=IDPH(I)
0015      CALL DEQTZ(IQI,IDP,PCR(I))
0016      IBIT=IBPH(I)
0017      12 CONTINUE
0018      IQI=IQI+15
0019      IF(IBIT.GE.4)IQI=IQI+16
0020      IF(IBIT.GE.5)IQI=IQI+32
0021      10 CONTINUE
0022      RETURN
0023      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000304 98	RW,I,CON,LCL
SIDATA	000022 9	RW,D,CON,LCL
SVARS	000010 4	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
TBL	003444 914	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 004064 1050

NO FPP INSTRUCTIONS GENERATED

```

C      ERSDQT.FTN
C
C      ERROR SIGNALS DEQUANTIZER
C      AUG. 4, 1980
C
0001      SUBROUTINE ERSDQT(IBIL,EL,QQL,IBIH,EH,QQH)
0002      COMMON/MTAPE0/NIN(170),NOUT(170)
0003      COMMON/TBL/QTBL(457)
0004      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0005      COMMON/SDTA/MPIT,IBETA,IQQL,IQQH,IDPL(4),IDPH(4)
0006      DIMENSION EL(1),EH(1)
0007      DATA SQRT3,IRN,JRN/1.73201,0,0/
0008      IQL=406
0009      IF(IBIL.GE.2)IQL=IQL+1
0010      IF(IBIL.GE.3)IQL=IQL+3
0011      IF(IBIL.GE.4)IQL=IQL+7
0012      ISGL=2**(IBIL-1)
0013      IQH=432
0014      IF(IBIH.GE.2)IQH=IQH+1
0015      IF(IBIH.GE.3)IQH=IQH+3
0016      IF(IBIH.GE.4)IQH=IQH+7
0017      ISGH=2**(IBIH-1)
0018      DO 10 I=1,72

C
C      DEQUANTIZE FOR LOW BAND
0019      IDL=NIN(I)
0020      IF(IDL.GE.ISGL)IDL=IDL-ISGL
0021      IF(IBIL.EQ.0)GO TO 20
0022      CALL DEQTZ(IQL,IDL,EL(I))
0023      EL(I)=EL(I)*QQL
0024      IF(NIN(I).GE.ISGL)EL(I)=-EL(I)
0025      GO TO 30
0026      20  CONTINUE

C
C      ADD RANDOM NUMBER FOR ERROR SIGNALS
C
0027      CALL RANDU(IRN,JRN,YQR)
0028      YQR=(YQR+YQR-1.0)*SQRT3
0029      EL(I)=YQR*SQRT3
0030      30  CONTINUE
0031      IDH=NIN(I+72)
0032      IF(IDH.GE.ISGH)IDH=IDH-ISGH
0033      IF(IBIH.EQ.0)GO TO 40
0034      CALL DEQTZ(IQH,IDH,EH(I))
0035      EH(I)=EH(I)*QQH
0036      IF(NIN(I+72).GE.ISGH)EH(I)=-EH(I)
0037      GO TO 10
0038      40  CONTINUE
0039      CALL RANDU(IRN,JRN,YQR)
0040      YQR=(YQR+YQR-1.0)*SQRT3
0041      EH(I)=YQR*SQRT3
0042      10  CONTINUE
0043      RETURN
0044      END

```

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SBAPC.FTN /WR

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PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000744 242	RW,I,CON,LCL
SIDATA	000054 22	RW,D,CON,LCL
SVARS	000032 13	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL
MTAPE0	001250 340	RW,D,OVR,GBL
TBL	003444 914	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 006052 1557

SBAPC,LP:=SBAPC/NOTR

```

      C      TAPE2.FTN
0001      SUBROUTINE TAPE2(IQ)
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE0/NIN(170),NOUT(170)
0004      COMMON/MTAPE1/NSKIP,IST,NTOTI,NTUPS,NTOTO
0005      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0006      COMMON/MTAPE3/NBF(1324),NBUF(1324)
0007      COMMON/MTAPE4/LST,IBEG
0008      DIMENSION ICARD(64)
0009      GO TO (700,800,900,999,1000,1001,1002,1003),IQ

      C
      C      INPUT DATA
0010      700      IST=IST+NTUPS
0011              IF(1324.GE.IST) GO TO 200
0012      100      IST=IST-1024
0013              NSKIP=NSKIP+1
0014      200      KOVER=LST+NTOTI-1325
0015              IF(KOVER.GT.0) GO TO 305
0016              DO 5000 I=1,NTOTI
0017      5000      NIN(I)=NBF(LST+I-1)
0018              LST=LST+NTUPS
0019              RETURN
0020      305      IPEP=LST-1024
0021              DO 5001 I=1,300
0022      5001      NBF(IPEP+I-1)=NBF(LST+I-1)
0023              LST=IPEP
0024              IF(NINS.EQ.0) GO TO 2100

      C      DISK INPUT
0025      DO 5010 I=1,16
0026      READ(2,END=2001,ERR=6000)(ICARD(J),J=1,64)
0027      K=64*(I-1)+300
0028      DO 5010 J=1,64
0029      5010      NBF(K+J)=ICARD(J)
0030              IF(NERR.NE.0) GO TO 6000
0031              GO TO 200
0032      2001      NEND=1
0033              GO TO 200
0034      2100      CALL TIN(NBF(301),NEND,NERR)
0035              GO TO 200

      C
0036      800      CONTINUE

      C      OUTPUT DATA
0037      DO 5005 I=1,NTOTO
0038      5005      NBUF(IBEG+I-1)=NOUT(I)
0039              IBEG=IBEG+NTOTO
0040              KON=1025-IBEG
0041              IF(KON.GT.0) GO TO 90
0042              IF(NOUTS.EQ.0) GO TO 2002
0043              DO 6010 I=1,16
0044              K=64*(I-1)
0045              DO 6011 J=1,64
0046      6011      ICARD(J)=NBUF(K+J)
0047      6010      WRITE(3)(ICARD(J),J=1,64)
0048              GO TO 2003
0049      2002      CALL TOUT(NBUF,NERR)
0050      2003      LRESID=-KON

```

```

0051      DO 5006 I=1,LRESID
0052      5006      NBUF(I)=NBUF(1024+I)
0053      IBEG=LRESID+1
0054      90      RETURN
          C
          C      INITIALIZE
0055      900      IF((NINS+NOUTS).LE.1) CALL ATTACH
0056      IF(NINS.EQ.0) CALL RWND0
0057      IF(NOUTS.EQ.0) CALL RWND1
0058      IF(NFILE.EQ.0) GO TO 995
0059      IF(NINS.EQ.0) CALL FSRCH(NFILE,NFRR)
0060      IF(NERR.NE.0) GO TO 6000
0061      913      DO 912 J=1,NSKIP
0062      IF(NINS.EQ.0) GO TO 3000
          C      DISK INPUT
0063      DO 5011 I=1,16
0064      READ(2,END=3001,ERR=6000)(ICARD(JJ),JJ=1,64)
0065      K=64*(I-1)+300
0066      DO 5011 JJ=1,64
0067      5011      NBF(K+JJ)=ICARD(JJ)
0068      GO TO 912
0069      3001      NEND=1
0070      GO TO 912
0071      3000      CALL TIN(NBF(301),NEND,NERR)
0072      IF(NERR.NE.0) GO TO 6000
0073      912      CONTINUE
0074      GO TO 995
0075      999      CONTINUE
0076      IBEG=1
0077      CALL EOFSH(NERR)
0078      RETURN
0079      995      CONTINUE
0080      IBEG=1
0081      LST=IST+300
0082      IST=IST-NTUPS
0083      RETURN
          C      END OF FILE
0084      1000      IF(NOUTS.EQ.0) GO TO 2010
0085      CALL CLOSE(3)
0086      GO TO 2011
0087      2010      CALL EOFW(NERR)
0088      2011      IBEG=1
0089      RETURN
0090      1001      NEND=0
0091      IF(NINS.EQ.0) GO TO 4020
0092      REWIND 2
0093      GO TO 4011
0094      4020      CALL RWND0
0095      NERR=0
0096      CALL FSRCH(NFILE,NERR)
0097      IF(NERR.NE.0) GO TO 6000
0098      4011      DO 950 J=1,NSKIP
0099      IF(NINS.EQ.0) GO TO 4000
          C      DISK INPUT
0100      DO 5012 I=1,16
0101      READ(2,END=4001,ERR=6000)(ICARD(K),K=1,64)

```

```

0102      K=64*(I-1)+300
0103      DO 5012 JJ=1,64
0104      5012      NBF(K+JJ)=ICARD(JJ)
0105      GO TO 950
0106      4001      NEND=1
0107      GO TO 4002
0108      4000      CALL TIN(NBF(301),NEND,NERR)
0109      IF(NERR.NE.0) GO TO 6000
0110      4002      IF(NEND.NE.0) GO TO 2000
0111      950      CONTINUE
0112      LST=IST+300
0113      IST=IST-NTUPS
0114      RETURN
0115      2000      NERR=16384
0116      RETURN
0117      1002      IF(NINS.EQ.1)CALL CLOSE(2)
0118      NEND=0
0119      RETURN
0120      1003      CALL INFO
0121      RETURN
0122      6000      TYPE 6001
0123      6001      FORMAT(1X,'INPUT FILE ERROR'//)
0124      NERR=1
0125      RETURN
0126      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	002400 640	RW,I,CON,LCL
SPDATA	000032 13	RW,D,CON,LCL
SIDATA	000070 28	RW,D,CON,LCL
SVARS	000220 72	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL
MTAPE0	001250 340	RW,D,OVR,GBL
MTAPE1	000012 5	RW,D,OVR,GBL
MTAPE2	000012 5	RW,D,OVR,GBL
MTAPE3	012260 2648	RW,D,OVR,GBL
MTAPE4	000004 2	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 016526 3755

NO FPP INSTRUCTIONS GENERATED

```

C      PROGRAM FSIO.FTN TO MOVE MAG TAPES
C      AND WRITE SPEECH FOR REAL-TIME I/O USING QIO
C
0001      SUBROUTINE ATTACH
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0004      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0005      DATA IOATT,IOSUC,IEALN/0001400,1,-34/
0006      DATA IORWD,IOWLB,IEVER,IOSPF,IORLB/02400,0400,-4,02440,0100/
0007      DATA IOSPF,IEEOF,IOEOF/02440,-10,03000/
0008      DATA MASK/0377/
0009      DATA MT0/0,2048,0,0,0,0/
0010      DATA MT1/0,2048,0,0,0,0/
0011      IF(NINS.NE.0) GO TO 1
0012      CALL ASNLUN(2,'MT',0,DSW)
0013      IF(DSW.EQ.1)GO TO 10
0014      11      WRITE(5,100)
0015      100      FORMAT(1X,'MT0: ATTACH UNSUCCESSFUL'/)
0016      NERR=1
0017      RETURN
0018      10      CALL WTOIO(IOATT,2,1,0,ISW,0,DSW)
0019      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0020      IF(IAND(IEALN,MASK).NE.IAND(MASK,ISW(1)))GO TO 11
0021      1      IF(NOUTS.NE.0) GO TO 2
0022      CALL ASNLUN(3,'MT',1,DSW)
0023      IF(DSW.EQ.1) GO TO 20
0024      12      WRITE(5,101)
0025      101      FORMAT(1X,'MT1: ATTACH UNSUCCESSFUL'/)
0026      NERR=1
0027      RETURN
0028      20      CALL WTOIO(IOATT,3,1,0,ISW,0,DSW)
0029      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 2
0030      IF(IAND(IEALN,MASK).NE.IAND(MASK,ISW(1)))GO TO 12
0031      2      RETURN
0032      END

```

# PROGRAM SECTIONS

NAME	SIZE		ATTRIBUTES
SCODE1	000262	89	RW,I,CON,LCL
SPDATA	000024	10	RW,D,CON,LCL
SIDATA	000160	56	RW,D,CON,LCL
MTAPE2	000012	5	RW,D,OVR,GBL
MTAPE5	000064	26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 000564 186

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE RWND0
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0004      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0005      CALL WTQIO(IORWD,2,1,0,ISW,0,DSW)
0006      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0007      WRITE(5,902)
0008      902      FORMAT(1X,'MT0: BUSY'//)
0009      NERR=1
0010      1      RETURN
0011      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000062 25	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000036 15	RW,D,CON,LCL
MTAPE2	000012 5	RW,D,OVR,GBL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 000232 77

NO FPP INSTRUCTIONS GENERATED



```

      C
0001      SUBROUTINE RWND1
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0004      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1  IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0005      CALL WTQIO(IORWD,3,1,0,ISW,0,DSW)
0006      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0007      WRITE(5,902)
0008      NERR=1
0009      902  FORMAT(1X,'MT1: BUSY'//)
0010      1    RETURN
0011      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000062 25	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000036 15	RW,D,CON,LCL
MTAPE2	000012 5	RW,D,OVR,GBL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 000232 77

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE TIN(BUF,NEND,NERR)
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MTO(6),MT1(6),DSW
0004      NEND=0
0005      NERR=0
0006      CALL GETADR(MTO,BUF)
0007      CALL WTQIO(IORLB,2,1,0,ISW,MTO,DSW)
0008      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0009      IF(IAND(IEEOF,MASK).EQ.IAND(MASK,ISW(1)))NEND=1
0010      IF(IAND(IEVER,MASK).EQ.IAND(MASK,ISW(1)))NERR=1
0011      1      RETURN
0012      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000156 55	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000026 11	RW,D,CON,LCL
MTAPE5	000064 26	RW,D,OV,GBL

TOTAL SPACE ALLOCATED = 000304 98

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE TOUT(NBUF,NERR)
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0004      NERR=0
0005      CALL GETADR(MT1,NBUF)
0006      CALL WTQIO(IOWLB,3,1,0,ISW,MT1,DSW)
0007      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0008      IF(IAND(IEVER,MASK).EQ.IAND(MASK,ISW(1)))NERR=1
0009      1      RETURN
0010      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000110 36	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000026 11	RW,D,CON,LCL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 000236 79

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE FSRCH(NFILE,NERR)
0002      IMPLICIT INTEGER (A-Z)
0003      COMMON/MTAPE3/NBF(1324),NBUF(1324)
0004      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1  IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0005      NERR=0
0006      FILE=NFILE-1
0007      IF(FILE.LE.0) RETURN
0008      DO 1 I=1,FILE
0009      CALL GETADR(MT0,NBF(301))
0010      CALL WTQIO(IORLB,2,1,0,ISW,MT0,DSW)
0011      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GOTO 2
0012      WRITE(5,100)NFILE
0013      100  FORMAT(1X,'FILE',I4, ' NOT FOUND'//)
0014      NERR=1
0015      RETURN
0016      2    MT0(1)=1
0017      1    CALL WTQIO(IOSPF,2,1,0,ISW,MT0,DSW)
0018      RETURN
0019      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000202 65	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000076 31	RW,D,CON,LCL
SVARS	000004 2	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
MTAPE3	012260 2648	RW,D,OVR,GBL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 012666 2779

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE EOFSH(NERR)
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE3/NBF(1324),NBUF(1324)
0004      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0005      NERR=0
0006      1      CALL GETADR(MT1(1),NBUF(1))
0007      CALL WTQIO(IORLB,3,1,0,ISW,MT1,DSW)
0008      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0009      IF(IAND(IEEOF,MASK).EQ.IAND(MASK,ISW(1)))GO TO 2
0010      NERR=1
0011      WRITE(5,1000)ISW(1)
0012      1000  FORMAT(1X,'FILE SEARCH ERROR' 09/)
0013      RETURN
0014      2      CALL GETADR(MT1(1),NBUF(1))
0015      CALL WTQIO(IORLB,3,1,0,ISW,MT1,DSW)
0016      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 1
0017      IF(IAND(IEEOF,MASK).EQ.IAND(MASK,ISW(1))) GO TO 3
0018      NERR=1
0019      RETURN
0020      3      MT1(1)=-1
0021      CALL WTQIO(IOSPF,3,1,0,ISW,MT1,DSW)
0022      RETURN
0023      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODF1	000254 86	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000076 31	RW,D,CON,LCL
MTAPE3	012260 2648	RW,D,OVR,GBL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 012732 2797

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE EOFW(NERR)
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE5/MASK,ISW(2),IOATT,IOSUC,IEALN,IORWD,
      1      IOWLB,IEVER,IOSPF,IEEOF,IOEOF,IORLB,MT0(6),MT1(6),DSW
0004      NERR=0
0005      DO 1 I=1,2
0006      1      CALL WTQIO(IOEOF,3,1,0,ISW(1))
0007      IF(IOSUC.EQ.IAND(MASK,ISW(1)))GO TO 2
0008      NERR=1
0009      RETURN
0010      2      MT1(1)=-1
0011      CALL WTQIO(IOSPF,3,1,0,ISW,MT1,DSW)
0012      IF(IOSUC.EQ.IAND(MASK,ISW(1)))RETURN
0013      NERR=1
0014      RETURN
0015      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000152 53	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000034 14	RW,D,CON,LCL
SVARS	000002 1	RW,D,CON,LCL
MTAPE5	000064 26	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 000310 100

NO FPP INSTRUCTIONS GENERATED

AD-A092 010

GTE PRODUCTS CORP NEEDHAM HEIGHTS MA COMMUNICATION S--ETC F/G 9/4  
SPEECH ALGORITHM OPTIMIZATION AT 16 KBPS.(U)  
SEP 80 R S CHEUNG, S Y KWON, A J GOLDBERG

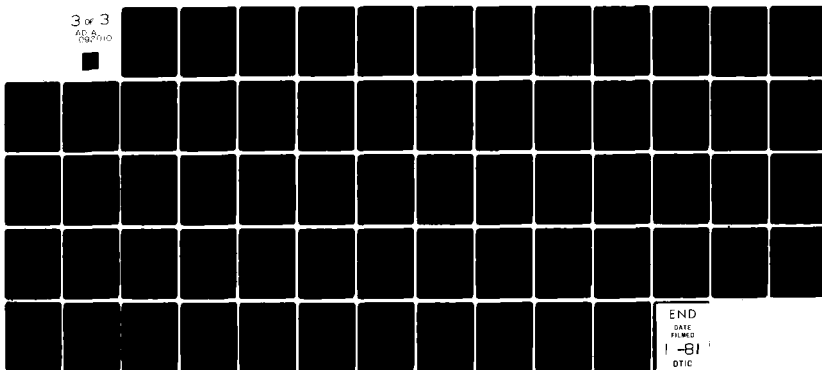
DCA100-79-C-0038

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```

      C      SUBROUTINE INFO.FTN
      C
0001      SUBROUTINE INFO
0002      IMPLICIT INTEGER(A-Z)
0003      COMMON/MTAPE0/NIN(256),NOUT(256)
0004      COMMON/MTAPE1/NSKIP,IST,NTOTI,NTUPS,NTOTO
0005      COMMON/MTAPE2/NEND,NERR,NFILE,NINS,NOUTS
0006      COMMON/MTAPE3/NBF(1324),NBUF(1324)
0007      LOGICAL*1 Y,ANS
0008      LOGICAL*1 EXTIN,EXTOUT,APPEND
0009      DIMENSION EXTIN(3),EXTOUT(3)
0010      DATA EXTIN/'I','N','P'/
0011      DATA EXTOUT/'O','U','T'/
0012      DATA Y/'Y'/
0013      DATA NEND,NERR,NFILE/0,0,0/
0014      DATA NSKIP,IST/1,1/

      C
      C      GET I/O INFORMATION FOR SPEECH HANDLER
      C
0015      APPEND=.FALSE.
0016      TYPE 1
0017      1      FORMAT(1H$,'IS THE INPUT ON MAG. TAPE? ')
0018      READ(5,2)ANS
0019      2      FORMAT(A1)
0020      IF(ANS.NE.Y)NINS=1
0021      TYPE 3
0022      3      FORMAT(1H$,'IS THE OUTPUT GOING TO MAG TAPE? ')
0023      READ (5,2) ANS
0024      IF(ANS.NE.Y) NOUTS=1
0025      IF(NOUTS.NE.0) GO TO 5
0026      TYPE 4
0027      4      FORMAT(1H$,'APPEND DATA? ')
0028      READ (5,2) ANS
0029      IF(ANS.EQ.Y) APPEND=.TRUE.
0030      IF(NOUTS.EQ.0) GO TO 151
0031      C      RSX11 SUPPORTED FILE
0032      TYPE 150
0033      150     FORMAT(1H$,'OUTPUT FILE NAME= ')
0034      CALL FILEN(3,EXTOUT)

      C
      C      BEGINNING OF INPUT
      C
0034      151     IF(NINS.NE.0) GO TO 155
0035      TYPE 100
0036      100     FORMAT(1H$,'MT FILE NO.=(I3) ')
0037      READ(5,101)NFILE
0038      101     FORMAT(I3)
0039      GO TO 14
0040      155     TYPE 13
0041      13      FORMAT(1H$,'INPUT FILE NAME= ')
0042      CALL FILEN(2,EXTIN)
0043      NFILE=1
0044      14      CALL TAPE2(3)
0045      IF(NERR.NE.0) RETURN
0046      IF(APPEND)CALL TAPE2(4)
0047      RETURN

```



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TAPE2.FTN /WR

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END

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000470 156	RW,I,CON,LCL
SPDATA	000014 6	RW,D,CON,LCL
SIDATA	000270 92	RW,D,CON,LCL
SVARS	000012 5	RW,D,CON,LCL
MTAPE0	002000 512	RW,D,OVR,GBL
MTAPE1	000012 5	RW,D,OVR,GBL
MTAPE2	000012 5	RW,D,OVR,GBL
MTAPE3	012260 2648	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 015312 3429

NO FPP INSTRUCTIONS GENERATED

```

0001      C      SUBROUTINE FILEN(UNIT,EXT)
          C
          C      THIS SUBROUTINE ACCEPTS THE NAME OF THE INPUT OR OUTPUT FILE
          C      FORM THE TTY DEVICE 5
          C      DEFAULT DEVICE
          C      UNLESS SPECIFIED IN INPUT STRING
          C      UNIT=UNIT NUMBER
          C      EXT = LOGICAL*1 BUFFER OF EXTENSION
          C
0002      IMPLICIT INTEGER(A-Z)
0003      LOGICAL*1 INSTR,DOT,BLNK,EXT
0004      DIMENSION INSTR(40)
0005      DIMENSION EXT(3)
0006      DATA BLNK,DOT/' ','.'/

          C
          C      INPUT FILE
0007      152      READ (5,99)(INSTR(I),I=1,40)
0008      99       FORMAT(40A1)
          C      CHECK FOR END OF LINE
0009      DO 1600 I=40,1,-1
0010      J=I
0011      1600    IF(INSTR(I).NE.BLNK)GO TO 1601
0012      TYPE 151
0013      151     FORMAT(1H$,'>')
0014      GO TO 152
0015      1601    DO 1602 I=1,J
0016      IF(INSTR(I).NE.BLNK) GO TO 1602

          C
          C
          C      BLANK DISCOVERED-COLLAPSE LINE BY ONE AND DECREASE CHARACTER COU
          C
0017      DO 1603 K=I,J-1
0018      1603    INSTR(K)=INSTR(K+1)
0019      INSTR(J)=BLNK
0020      J=J-1
0021      GO TO 1601
0022      1602    CONTINUE
0023      DO 103 I=1,J
0024      103     IF(INSTR(I).EQ.DOT) GO TO 25
0025      INSTR(J+1)=DOT
0026      INSTR(J+2)=EXT(1)
0027      INSTR(J+3)=EXT(2)
0028      INSTR(J+4)=EXT(3)
0029      J=J+4
0030      25      CALL SCAN(INSTR,J)
0031      CALL ASSIGN(UNIT,INSTR,J)
0032      RETURN
0033      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000444 146	RW,I,CON,LCL

FORTTRAN IV-PLUS V02-51E  
TAPE2.FTN /WR

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SIDATA 000042 17  
SVARS 000060 24  
STEMPS 000004 2

RW,D,CON,LCL  
RW,D,CON,LCL  
RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000572 189

NO FPP INSTRUCTIONS GENERATED

```

      C
0001      SUBROUTINE SCAN(BUF,LTH)
0002      IMPLICIT INTEGER(A-Z)
0003      LOGICAL*1 BUF,DEVICE
0004      DIMENSION BUF(1),DEVICE(4)
0005      DATA DEVICE/'S','Y','O','I'/'
0006      DO 1 I=1,LTH
0007      1 IF(BUF(I).EQ.DEVICE(4))RETURN
0008      LTH=LTH+4
0009      DO 2 I=LTH,5,-1
0010      2 BUF(I)=BUF(I-4)
0011      DO 3 I=1,4
0012      3 BUF(I)=DEVICE(I)
0013      RETURN
0014      END
  
```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000172 61	RW,I,CON,LCL
\$IDATA	000012 5	RW,D,CON,LCL
SVARS	000006 3	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000214 70

NO FPP INSTRUCTIONS GENERATED

TAPE2,LP:=TAPE2/NOTR

```

C      FFTRR8.FTN
C      JAN.,30, 1979
C      EQU. ROUTINE OF (100,117)FFTRR8
0001      SUBROUTINE FFTRR8(XR,XI,M,IS)
0002      DIMENSION XR(1),XI(1)
0003      N=2**M
0004      NV2=N/2
0005      NM1=N-1
0006      J=1
0007      DO 7 I=1,NM1
0008      IF(I.GE.J)GO TO 5
0009      T=XR(J)
0010      XR(J)=XR(I)
0011      XR(I)=T
0012      T=XI(J)
0013      XI(J)=XI(I)
0014      XI(I)=T
0015      5      K=NV2
0016      6      IF(K.GE.J)GO TO 7
0017      J=J-K
0018      K=K/2
0019      GO TO 6
0020      7      J=J+K
0021      PI=3.1415927
0022      DO 20 L=1,M
0023      LE=2**L
0024      LE1=LE/2
0025      UR=1.0
0026      UI=0.0
0027      WR=COS(PI/LE1)
0028      WI=SIN(PI/LE1)
0029      IF(IS.LT.0)WI=-WI
0030      DO 20 J=1,LE1
0031      DO 10 I=J,N,LE
0032      IP=I+LE1
0033      TR=XR(IP)*UR-XI(IP)*UI
0034      TI=XR(IP)*UI+XI(IP)*UR
0035      XR(IP)=XR(I)-TR
0036      XI(IP)=XI(I)-TI
0037      XI(I)=XI(I)+TI
0038      10      XR(I)=XR(I)+TR
0039      URR=UR*WR-UI*WI
0040      UI=UR*WI+WR*UI
0041      20      UR=URR
0042      IF(IS.EQ.-1)GO TO 40
0043      DO 30 I=1,N
0044      XR(I)=XR(I)/FLOAT(N)
0045      XI(I)=XI(I)/FLOAT(N)
0046      30      CONTINUE
0047      40      RETURN
0048      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
------	------	------------

FORTTRAN IV-PLUS V02-51E  
FFTRR8.FTN /WR

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\$CODE1 001154 310  
SPDATA 000004 2  
SIDATA 000024 10  
\$VARS 000070 28  
STEMPS 000012 5

RW,I,CON,LCL  
RW,D,CON,LCL  
RW,D,CON,LCL  
RW,D,CON,LCL  
RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 001306 355

FFTRR8,LP:=FFTRR8/NOTR

```

C      SER.FTN
C      SERIALIZE TRANSMISSION PARAMETERS INTO BINARY DATA
C
C      AUG.4, 1980
C
0001      SUBROUTINE SER(INBA,INB,IBIL)
0002      COMMON/MTAPE0/NIN(170),NOUT(170)
0003      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0004      COMMON/SDTA/MPIT,IBETA,IQOL,IQOH,IDPL(4),IDPH(4)
0005      DIMENSION INBA(1),INB(1)
C
C      INI. THE TRANSMITER DATA
C
0006      DO 100 I=1,360
0007      INBA(I)=0
C
C      SERIALIZE MPIT
0008      CALL DBCONV(MPIT,IBPT,INB)
0009      IQI=0
0010      DO 220 I=1,IBPT
0011      IQI=IQI+1
0012      INBA(IQI)=INB(I)
C
C      SERIALIZE FOR BETA
0013      CALL DBCONV(IBETA,IBBT,INB)
0014      DO 230 I=1,IBBT
0015      IQI=IQI+1
0016      INBA(IQI)=INB(I)
C
C      SERIALE FOR QOL
0017      CALL DBCONV(IQOL,IBQL,INB)
0018      DO 200 I=1,IBQL
0019      IQI=IQI+1
0020      INBA(IQI)=INB(I)
C
C      SERIALIOZE FOR QOH
0021      CALL DBCONV(IQOH,IBQH,INB)
0022      DO 210 I=1,IBQH
0023      IQI=IQI+1
0024      INBA(IQI)=INB(I)
C
C      SERIALIZE FOR LOW BAND PARCOR
C
0025      DO 240 J=1,4
0026      IBT=IBPL(J)
0027      CALL DBCONV(IDPL(J),IBT,INB)
0028      DO 250 I=1,IBT
0029      IQI=IQI+1
0030      INBA(IQI)=INB(I)
0031      CONTINUE
C
C      SERIALIZE FOR HIGH BAND PARCOR
C
0032      DO 260 J=1,4
0033      IBT=IBPH(J)
0034      CALL DBCONV(IDPH(J),IBT,INB)

```

```

0035      DO 270 I=1,IBT
0036      IQI=IQI+1
0037      270  INBA(IQI)=INB(I)
0038      260  CONTINUE
           C
           C      IQI WILL BE 50
0039      IQS=50
           C
           C      PROTECT 56 BITS OF IMPORTANT BAND
           C
0040      IBIH=3-IBIL
0041      IF(IBIL.LE.1)GO TO 300
           C
           C      IBIL=2 OR 3
0042      IES=0
0043      IEF=72
0044      IBL=IBIL
0045      IBS=IBIH
0046      GO TO 400
0047      300  CONTINUE
0048      IES=72
0049      IEF=0
0050      IBL=IBIH
0051      IBS=IBIL
0052      400  CONTINUE
0053      IF(IBL.EQ.3)GO TO 600
           C
           C      IBL=2
           C
           C      SERIALIZE HIGHER ENERGY ERROR SIGNALS
0054      DO 520 I=1,72
0055      IJ=I+IES
0056      CALL DBCONV(NIN(IJ),IBL,INB)
0057      DO 530 J=1,IBL
0058      IQS=IQS+1
0059      530  INBA(IQS)=INB(J)
0060      520  CONTINUE
           C
           C      SERIALIZE LOW ENERGY BAND ERROR SIGNALS
           C
0061      DO 540 I=1,72
0062      IJ=I+IEF
0063      IQS=IQS+1
0064      550  INBA(IQS)=NIN(IJ)
0065      540  CONTINUE
0066      RETURN
0067      600  CONTINUE
           C
           C      IBL=3
           C      IBS=0
0068      DO 610 I=1,31
0069      IJ=I+IES
0070      CALL DBCONV(NIN(IJ),IBL,INB)
0071      DO 620 J=1,IBL
0072      IQS=IQS+1
0073      620  INBA(IQS)=INB(J)

```



```

0074      610      CONTINUE
           C
0075      DO 630 I=32,72
0076      IJ=I+IES
0077      CALL DBCONV(NIN(IJ),IBL,INB)
0078      DO 640 J=1,2
0079      IQS=IQS+1
0080      640      INBA(IQS)=INB(J)
           C      STORE THE THIRD BITS OUT OF PROTECTION GROUP
0081      INBA(194+I)=INB(3)
0082      630      CONTINUE
0083      RETURN
0084      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	001716 487	RW,I,CON,LCL
SIDATA	000104 34	RW,D,CON,LCL
SVARS	000026 11	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL
MTAPEU	001250 340	RW,D,OVR,GBL
SRTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003404 898

NO FPP INSTRUCTIONS GENERATED

SER,LP:=SER/NOTR

```

      C      ENCBCH.FTN
      C      MARCH 16, 1979
      C      ENCODING OF A(63,45)BCH CODE
0001      SUBROUTINE ENCBCH(INBA,INA,INC,KT)
0002      DIMENSION INBA(1),INA(1),INC(1),ING(19)
0003      DATA ING/1,1,1,1,0,0,0,0,0,1,0,1,1,0,0,1,1,1,1/
      C      CALCULATE PARITY BITS
0004      DO 10 I=1,63
0005      KTI=(KT-1)*63+I
0006      INA(I)=INBA(KTI)
0007      IF(I.GT.45)INA(I)=0
0008      10  CONTINUE
0009      CALL GF2DIV(INA,63,ING,19,INC,NC)
      C      SHIFT 18 BITS FOR PARITY BITS
      C
0010      KTF=270+18*KT
0011      KTI=KTF-63*KT
0012      DO 30 I=1,KTI
0013      INBA(KTF+1-I)=INBA(KTF-17-I)
0014      30  CONTINUE
      C
      C      STORE PARITY BITS
0015      DO 20 I=1,NC
0016      KTI=(KT-1)*63+I+45
0017      20  INBA(KTI)=INC(I)
0018      RETURN
0019      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000412 133	RW,I,CON,LCL
SPDATA	000010 4	RW,D,CON,LCL
SIDATA	000054 22	RW,D,CON,LCL
SVARS	000056 23	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000556 183

NO FPP INSTRUCTIONS GENERATED

```

      C      CEIR.FTN
      C      MARCH 16, 1979
      C      CHANNEL ERROR SIMULATION ROUTINE
0001      SUBROUTINE CEIR(INBA,NBRPF,PROB,IRN,JRN,NERB,NEPB)
0002      COMMON/SW/ICOUNT,IPRSW
0003      DIMENSION INBA(1),NERB(1)
0004      NEPB1=NEPB+1
0005      DO 50 I=1,NEPB1
0006      50  NERB(I)=0
      C      XMIT INPUT BINARY VECTOR
0007      IF(NEPB.LE.0)GO TO 40
0008      DO 30 J=1,NEPB
0009      DO 10 I=1,63
0010      ISV1=NERB(J)
0011      IP=I+63*(J-1)
0012      CALL RANERR(INBA(IP),PROB,IRN,JRN,NERB(J))
0013      IF(ISV1.NE.NERB(J).AND.IPRSW.EQ.1)WRITE(4,100)ICOUNT,IP
0014      10  CONTINUE
0015      30  CONTINUE
0016      40  CONTINUE
0017      ISTP=NEPB*63+1
0018      DO 20 I=ISTP,NBRPF
0019      ISV1=NERB(NEPB1)
0020      CALL RANERR(INBA(I),PROB,IRN,JRN,NERB(NEPB1))
0021      IF(ISV1.NE.NERB(NEPB1).AND.IPRSW.EQ.1)WRITE(4,100)ICOUNT,I
0022      20  CONTINUE
0023      100  FORMAT(1X,'FR=',I4,2X,'ERR LC=',I3)
0024      RETURN
0025      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000664 218	RW,I,CON,LCL
SIDATA	000066 27	RW,D,CON,LCL
SVARS	000014 6	RW,D,CON,LCL
STEMPS	000010 4	RW,D,CON,LCL
SW	000004 2	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 001002 257

NO FPP INSTRUCTIONS GENERATED

```
      C      RANERR.FTN
0001      SUBROUTINE RANERR(IX,PROB,IRN,JRN,NER)
0002      CALL RANDU(IRN,JRN,YQR)
0003      IF(YQR.GE.PROB)RETURN
0004      IX=IEOR(IX,1)
0005      NER=NER+1
0006      RETURN
0007      END
```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000066 27	RW,I,CON,LCL
SIDATA	000010 4	RW,D,CON,LCL
SVARS	000004 2	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000102 33

```

C      DECBCH.FTN
C      DECODING OF BCH CODE
C      EXAMPLE OF A(63,45) BCH CODE WHICH CORRECT 3 ERRORS
C      G(X)=(X**6+X+1)(X**6+X**4+X**2+X+1)(X**6+X**5+X**2+X+1)
0001      SUBROUTINE DECBCH(INBA,INA,KT,NES)
0002      COMMON/SW/ICOUNT,IPRSW
0003      DIMENSION ISD1(7),ISD3(7),ISD5(7),INA(1),INB(63),INC(7),IM1(7)
0004      DIMENSION INBA(1),NERL(3)
0005      DATA IM1/1,0,0,0,0,1,1/
C      READ INPUT VECTOR INA
0006      DO 10 I=1,63
0007      KTI=(KT-1)*45+I
0008      INA(I)=INBA(KTI)
C      START DECODING
C
C      DECODING ROUTINE
C
C      *****
C      CALCULATE POWER SUMS
0009      CALL GF2DIV(INA,63,IM1,7,ISD1,NC)
C      CALCULATE R(X**3)
DO 18 I=1,63
0010      INB(I)=0
0011      DO 19 I=1,63
0012      I3=(63-I)*3
0013      IR=I3-(I3/63)*63
0014      IT=63-IR
0015      IX=INA(I)
0016      INB(IT)=IEOR(IX,INB(IT))
0017      CALL GF2DIV(INB,63,IM1,7,ISD3,NC)
0018      CALCULATE R(X**5)
DO 28 I=1,63
0019      INB(I)=0
0020      DO 29 I=1,63
0021      I5=(63-I)*5
0022      IR=I5-(I5/63)*63
0023      IT=63-IR
0024      IX=INA(I)
0025      INB(IT)=IEOR(IX,INB(IT))
0026      CALL GF2DIV(INB,63,IM1,7,ISD5,NC)
0027      FORMAT(1X,'S1=',18I1)
0028      FORMAT(1X,'S3=',18I1)
0029      FORMAT(1X,'S5=',18I1)
0030      CHECK ERROR RANGE
0031      DO 40 I=1,6
0032      IF(ISD1(I).EQ.1)GO TO 50
0033      IF(ISD3(I).EQ.1)GO TO 50
0034      IF(ISD5(I).EQ.1)GO TO 50
0035      CONTINUE
C      NO CHANNEL ERROR
0036      GO TO 998
0037      CONTINUE
C      CORRECT CHANNEL ERROR
C
C      CALCULATE SIGMA(I),I=1,3
C      CALCULATE DET(3),I.E.,S1**3+S3

```

```

0038      CALL GF2MUL(ISD1,6,ISD1,6,INC,ND,IM1,7)
0039      CALL GF2MUL(ISD1,6,INC,6,INA,ND,IM1,7)
0040      CALL GF2ADD(INA,6,ISD3,6,INB,ND)
          CC      IF(ISW0.EQ.2)WRITE(5,303)(INB(I),I=1,ND)
0041      NES=3
0042      DO 60 I=1,6
0043      IF(INB(I).EQ.1)GO TO 70
0044      60      CONTINUE
0045      NES=1
          C      ONLY ONE ERROR OCCUR
0046      GO TO 80
0047      70      CONTINUE
          C      CALCULATE SIGMA(2) AND SIGMA(3)
          C      STORE INB(I),I=1,6
0048      DO 90 I=1,6
0049      90      INA(I)=INB(I)
          C      CALCULATE SIGMA(2)
          C      CALCULATE S1**2*S3+S5
0050      CALL GF2MUL(INC,6,ISD3,6,INB,NC,IM1,7)
0051      CALL GF2ADD(INB,6,ISD5,6,INC,NC)
          CC      IF(ISW0.EQ.2)WRITE(5,303)(INC(I),I=1,6)
0052      DO 789 I=1,6
0053      IF(INC(I).EQ.1)GO TO 444
0054      789      CONTINUE
          C      INC=0
0055      GO TO 85
0056      444      CONTINUE
          C      FIND THE ORDER OF INC=S1**2*S3+S5
          C      FIND THE ORDER OF INA=S1**3+S3
          C      INI INB
0057      DO 39 I=1,63
0058      39      INB(I)=0
0059      IORA=0
0060      IORC=0
0061      DO 49 I=2,63
0062      INB(64-I)=1
0063      INB(65-I)=0
0064      CALL GF2DIV(INB,63,IM1,7,ISD3,NC)
          CC      IF(ISW0.EQ.2.AND.ISW1.EQ.1)WRITE(5,404)I,(ISD3(J),J=1,6)
0065      404      FORMAT(1X,'N=',I3,3X,8I1)
          C      CHECK THE ORDER
0066      DO 59 J=1,6
0067      IF(ISD3(J).NE.INA(J))GO TO 69
0068      59      CONTINUE
0069      IORA=I-1
0070      69      DO 79 J=1,6
0071      IF(ISD3(J).NE.INC(J))GO TO 89
0072      79      CONTINUE
0073      IORC=I-1
0074      89      IF(IORA.NE.0.AND.IORC.NE.0)GO TO 109
0075      49      CONTINUE
0076      109      IOR3=IORC-IORA
0077      IF(IOR3.LT.0)IOR3=IOR3+63
0078      IOR3=63-IOR3
0079      DO 119 I=1,63
0080      IT=0

```

```

0081      IF(I.EQ.IOR3)IT=1
0082      119      INB(I)=IT
           C      CALCULATE SIGMA(2)
0083      CALL GF2DIV(INB,63,IM1,7,ISD3,NC)
           C
           CC     IF(ISW0.EQ.2)WRITE(5,202)(ISD3(I),I=1,6)
           C      CALCULATE SIGMA(3)
0084      CALL GF2MUL(ISD1,6,ISD3,6,INC,NC,IM1,7)
0085      CALL GF2ADD(INA,6,INC,6,ISD5,NC)
           CC     IF(ISW0.EQ.2)WRITE(5,303)(ISD5(I),I=1,6)
           C      IF ISD5=0, THEN NES=2
0086      DO 71 I=1,6
0087      IF(ISD5(I).NE.0)GO TO 80
0088      71      CONTINUE
0089      NES=2
0090      GO TO 80
0091      85      CONTINUE
0092      DO 87 I=1,6
0093      ISD3(I)=0
0094      ISD5(I)=INA(I)
0095      87      CONTINUE
0096      80      CONTINUE
           C      CORRECT NES ERROR BY CHIEN'S SEARCH METHOD
           C
0097      NEST=0
0098      DO 11 II=1,63
0099      III=II-1
0100      IF(III.EQ.0)III=63
           C      INI VECTOR C
0101      DO 22 I=1,6
0102      22      INB(I)=0
0103      CALL GF2ADD(ISD1,6,INB,6,INC,NC)
0104      IF(NES.EQ.1)GO TO 33
0105      CALL GF2ADD(ISD3,6,INC,6,INB,NB)
0106      CALL GF2ADD(INB,6,ISD5,6,INC,NC)
0107      33      CONTINUE
           CC     IF(ISW0.EQ.2.AND.ISW1.EQ.1)WRITE(5,303)(INC(I),I=1,6)
0108      IF(INC(6).EQ.0)GO TO 44
0109      DO 55 I=1,5
0110      IF(INC(I).EQ.1)GO TO 44
0111      55      CONTINUE
           C      CORRECT ERROR
0112      KTT=(KT-1)*63+III
0113      NEST=NEST+1
0114      NERL(NEST)=KTT
0115      44      CONTINUE
           C      SHIFT ISV1,ISV3,ISV5
0116      INB(1)=1
0117      INB(2)=0
0118      DO 88 I=1,6
0119      88      INA(I)=ISD1(I)
0120      CALL GF2MUL(INA,6,INB,2,ISD1,NC,IM1,7)
0121      IF(NES.EQ.1)GO TO 11
0122      INB(1)=1
0123      INB(2)=0
0124      INB(3)=0

```

```

0125      DO 775 I=1,6
0126      775      INA(I)=ISD3(I)
0127      CALL GF2MUL(INA,6,INB,3,ISD3,NC,IM1,7)
0128      INB(1)=1
0129      INB(2)=0
0130      INB(3)=0
0131      INB(4)=0
0132      DO 665 I=1,6
0133      665      INA(I)=ISD5(I)
0134      CALL GF2MUL(INA,6,INB,4,ISD5,NC,IM1,7)
0135      11      CONTINUE
          C      CHECK ERROR STATUS
0136      IF(NES.EQ.NEST)GO TO 888
0137      NES=4
0138      GO TO 998
          C      CORRECT ERRORS
0139      888      CONTINUE
0140      DO 72 I=1,NES
0141      KTT=NERL(I)
0142      IF(IPRSW.EQ.1)WRITE(4,707)ICOUNT,KTT
0143      707      FORMAT(1X,'FR=',I6,2X,'EC LC=',I3)
0144      KTR=KTT-(KT-1)*18
0145      INBA(KTR)=IEOR(INBA(KTR),1)
0146      72      CONTINUE
0147      998      CONTINUE
          C
          C      COMPRESS 18 PARITY BITS FOR DESERIALIZATION ROUTINE
          C
0148      KTI=45*KT+1
0149      KTF=360-18*KT
0150      DO 900 I=KTI,KTF
0151      900      INBA(I)=INBA(I+18)
0152      RETURN
0153      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	002706 739	RW,I,CON,LCL
SPDATA	000030 12	RW,D,CON,LCL
SIDATA	000430 140	RW,D,CON,LCL
SVARS	000362 121	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
Sw	000004 2	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003756 1015

NO FPP INSTRUCTIONS GENERATED

CESR,LP:=CESR/NOTR



```

C      MRNSA.FTN
C
C      JUNE 6, 1980
C
C
C      *****
C
C      NOISE SUPPRESION ROUTINE BY R.J. MCAULAY
C
C      R.J. MCAULAY,"SPEECH ENHANCEMENT USING A SOFT-DECISION NOISE
C      SUPPRESION FILTER,"IEEE TRANS. ASSP APRIL 1980.
C
C      *****
C
0001      SUBROUTINE MRNSA(XR,XI,NTOTI,NSF)
0002      COMMON/MTAPE0/NIN(170),NOUT(170)
0003      COMMON/NSTBL/FNSTBL(50)
0004      DIMENSION XR(1),XI(1)
0005      DIMENSION STCS(129),DIST(128)
0006      DATA STCS/129*1.0/
0007      DATA DIST/10*0.0,117*200.,0.0/
0008      DATA AGNO,AGNL/2*1.0/
C      TAKE DFT OF NOISY INPUT SPEECH SIGNAL
C
C      CALCULATE ENERGY FOR V/N/S DECISION
C
0009      EN0=0.0
0010      DO 8010 I=1,256
0011      XI(I)=0.0
0012      XR(I)=0.0
0013      IF(I.GT,NTOTI)GO TO 8010
0014      XR(I)=FLOAT(NIN(I))
0015      8010 EN0=EN0+XR(I)**2
0016      EN0=EN0/128.0
C
C
C      PERFORM DFT
C
0017      CALL FFTRR8(XR,XI,8,-1)
C
C      CLASSIFY SIGNAL STATE
C      USE ROBERT'S MODIFIED NOISE DETECTION ALGORITHM
C
0018      CALL MRNDA(EN0,DIST,NTH0,THL,ENN,FMU)
C
C
C      SUPPRESS NOISE IN FREQUENCY DOMAIN
C
C      USE MCAULAY'S APPROACH
C
C      START SUPPRESION

```

```

      C
0019      AGN=0.0
0020      DO 8030 J=1,256
0021      JX=J
0022      IF(J.GE.129)JX=258-J
      C      SIGNAL POWER SPECTRUM ASPW
0023      ASPW=XR(J)**2+XI(J)**2
0024      GN=ASPW-STCS(JX)
0025      IF(GN.GE.1.E-6)GN=GN/ASPW
0026      IF(GN.LE.1.E-6)GN=1.E-6
      C
      C      UPDATE NOISE SATTISTICS IF SPEECH NOT PRESENT
      C
0027      IF(J.GT.129)GO TO 8033
0028      IF(NTH0.EQ.2)GO TO 8033
      C
      C      UPDATE NOISE STATISTICS
      C
0029      TT=STCS(J)-ASPW
0030      IF(TT.LT.0.0)TT=TT*0.7788
0031      IF(TT.GE.0.0)TT=TT*0.875
0032      STCS(J)=ASPW+TT
0033      8033      CONTINUE
      C      CALCULATE SUPPRESION FACTOR
      C
      C
0034      IGN=INT(GN*50.0)+1
0035      IF(IGN.GE.50)IGN=50
0036      GN=FNSTBL(IGN)
0037      AGN=AGN+GN
      C      INSERT SMOOTHING GAIN PROGRAM IN LATER VERSION
      C
0038      8037      XR(J)=XR(J)*GN
0039      XI(J)=XI(J)*GN
0040      8030      CONTINUE
      C
      C      NOISE SUPPRESSION IS DONE IN FREQUENCY DOMAIN
      C
      C      PERFORM INVERSE DFT
0041      CALL FFTRR8(XR,XI,8,1)
      C
      C      STORE NOISE SUPPRESSED OUTPUT TIME DOMAIN FOR SBAPC
      C
      C
0042      AGN=AGN/256.0
      C
      C      CALCULATE LONG TERM AGN AND USE IT TO ADJUST THE NOISE SUPPRESSION
      C      FACTOR ADAPTIVELY IN LATER VERSION
0043      AGNL=AGNL*127./128.0+AGN/128.0
      C
      C      CALCULATE SHORT TERM AGN
      C
0044      AGNO=AGNO*0.75+AGN*0.25
0045      FMUL=AGNO/AGNL
0046      FMUL=SQRT(FMUL)
      C

```

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```
      C
0047      DO 8040 I=1,NTOTI
0048      XR(I)=FMUL*XR(I)
0049      8040 CONTINUE
      C
0050      RETURN
0051      END
```

#### PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	001070 284	RW,I,CON,LCL
SPDATA	000024 10	RW,D,CON,LCL
SI DATA	000066 27	RW,D,CON,LCL
SVAKS	002072 541	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL
MTAPE0	001250 340	RW,D,OVR,GBL
NSTBL	000310 100	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 005056 1303

```

C      MRNDA.FTN
C
C      MAY 15, 1980
C
C      MODIFIED ROBERT'S NOISE DETCTION ALGORITHM(ASSP 144, APRIL 1980)
C
0001      SUBROUTINE MRNDA(ENO,DIST,NTH,THL,FJMX,FMU)
0002      DIMENSION DIST(1)
0003      DATA THMXT,THMX,THOL,THOMN/2*32768.0,16384.0,1024./
0004      DATA FMUL/1.0/

C
C      CHECK INPUT ENERGY
C
C      NTH=0:SILENCE
C      NTH=1:NOISE PRESENT
C      NTH=2:SPEECH PRESENT
C
C      SLOW DEGRADATION OF MAX ENERGY VALUE

0005      THMX=THMX*0.995
C      CALCULATE AVERAGE FRAME ENERGY
0006      THMXT=THMXT*0.75+ENO*0.25
0007      IF(THMXT.GE.THMX)THMX=THMXT
C      FIND MAX DIST. POINT
0008      JMX=1
0009      DIMX=DIST(1)
0010      DO 100 I=2,128
0011      IF(DIST(I).LE.DIMX)GO TO 100
0012      JMX=I
0013      DIMX=DIST(I)
0014      100 CONTINUE

C
C      FIND AVERAGE VALUE OF THMX AND JMX EQUIVALENT
C
0015      FJMX=256.0*FLOAT(JMX+1)/FMUL
C
C      DECREASE FMUL IF MORE THAN 100 FRAMES ARE SPEECH'S
0016      IF(NTH.NE.2)ICT=0
0017      IF(NTH.EQ.2)ICT=ICT+1
0018      IF(ICT.LE.50)GO TO 333
0019      FMUL=FMUL/2.0
0020      GO TO 222
0021      333 IF(JMX.NE.1)GO TO 222
C
C      INCREASE FMUL
0022      FMUL=FMUL*2.0
0023      222 CONTINUE
0024      AVENN=SQRT(FJMX*THMX)
0025      FMULT=32768.0/AVENN
C      SLOW CHANGE OF FMUL TIME CONST 1 SEC
C
0026      FMUL=FMULT+0.875*(FMUL-FMULT)
0027      FMU=FMUL
0028      NTH=2
C      TEST FOR NOISE PRESENSE

```

```

      C
      C      DECAY HISTOGRAM BY 4-SEC TIME CONSTATNT
      C      FS=6400, FRAME SIZE=22.5 MS(144 SAMPLES)
      C
0029      FNORM=0.0
0030      DO 10 I=1,128
0031      DIST(I)=DIST(I)*0.9944
0032      FNORM=FNORM+DIST(I)
0033      10  CONTINUE
      C
      C      NORMAIZE ENERGY SUCH THAT THOL=16384.
      CC     FMUL=1.0
0034      EN=EN0*FMUL
0035      IF(EN.GE.32768.)RETURN
      C      CALCULATE PRESENT FRAME ENERGY BIN
      C
0036      JBIN=INT(EN/256.)
0037      NTH=0
0038      DECAY=0.60653
0039      THNW=0.0
0040      IF(JBIN.EQ.0)GO TO 30
0041      DIST(JBIN)=DIST(JBIN)+144.
0042      FNORM=FNORM+144.
      C
      C      SEARCH FOR SILENCE AND SET NEW THRESHOLD
      C
0043      THSL=FNORM/4.0
0044      THNC=FNORM*0.8
0045      THMV=0.0
0046      DO 20 J=1,10
0047      20  THMV=THMV+DIST(J)
0048      IF(THMV.GE.THSL)GO TO 30
      C
      C      NOISE PRESENT
      C
0049      NTH=1
      C
0050      DO 40 J=11,128
0051      THMV=THMV+DIST(J)
0052      IF(THMV.GE.THNC)GO TO 50
0053      40  CONTINUE
0054      50  CONTINUE
0055      THNW=256.*FLOAT(J)
0056      IF(EN.GE.THOL)NTH=2
0057      IF(THNW.LT.THOL)GO TO 30
0058      DECAY=0.945
0059      30  CONTINUE
0060      THOL=THNW+DECAY*(THOL-THNW)
      CC     THOL=THOL+DECAY*(THNW-THOL)
0061      IF(THOL.LE.THOMN)THOL=THOMN
0062      IF(NTH.EQ.0.AND.THOL.LE.EN)THOL=EN
0063      THL=THOL/FMUL
0064      RETURN
0065      END

```

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BNSR.FTN /WR

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PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	001232 333	RW,I,CON,LCL
SPDATA	000024 10	RW,D,CON,LCL
SIDATA	000012 5	RW,D,CON,LCL
SVARS	000106 35	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 001376 383

BNSR,LP:=BNSR/NOTR

```

      C      DSER.FTN
      C      DESERIALIZE BINARY DATA
      C      AUG 4 ,1980
0001      SUBROUTINE DSER(INBA,INB,QQL,QQH,IBIL,IBIH,ILMX,ILMN)
0002      COMMON/MTAPE0/NIN(170),NOUT(170)
0003      COMMON/SBTA/IBPT,IBBT,IBQL,IBQH,IBPL(4),IBPH(4)
0004      COMMON/SDTA/MPIT,IBETA,IQQL,IQQH,IDPL(4),IDPH(4)
0005      DIMENSION INBA(1),INB(1)

      C
      C      DESERIALIZE PITCH
      C
0006      IQI=0
0007      DO 220 I=1,IBPT
0008      IQI=IQI+1
0009      220  INB(I)=INBA(IQI)
0010      CALL BDCONV(INB,IBPT,MPIT)

      C
      C      DESERIALIZE FOR BETA
0011      DO 230 I=1,IBBT
0012      IQI=IQI+1
0013      230  INB(I)=INBA(IQI)
0014      CALL BDCONV(INB,IBBT,IBETA)

      C
      C      DESERIALIZE FOR QQL
0015      DO 200 I=1,IBQL
0016      IQI=IQI+1
0017      200  INB(I)=INBA(IQI)
0018      CALL BDCONV(INB,IBQL,IQQL)

      C
      C      DEQUANTIZE FOR QQL
0019      IQD=32
0020      CALL DEQTZ(IQD,IQQL,QQL)
0021      IQD=IQD+2**((IBQL+1)-1)

      C
      C      DESERIALIZE FOR IQQH
0022      DO 210 I=1,IBQH
0023      IQI=IQI+1
0024      210  INB(I)=INBA(IQI)
0025      CALL BDCONV(INB,IBQH,IQQH)

      C
      C      DEQUANTIZE FOR QQH
0026      CALL DEQTZ(IQD,IQQH,QQH)

      C
      C      FIND THE BITS ASSIGNMENTS FOR LOW BAND AND HIGH BAND
      C
      C      ASSUME THE AVERAGE BITS=1.5
      C
0027      QQL IS LOG QQL OF BASE 2
0028      FIBIL=1.5*(QQL-QQH)/2.0
0029      IBIL=FIBIL+0.5
0030      IF (IBIL.GE.ILMX) IBIL=ILMX
0031      IF (IBIL.LE.ILMN) IBIL=ILMN
0032      IBIH=3-IBIL
0033      QQL=2.0**QQL
      QQH=2.0**QQH

```

```

      C
      C      DESERIALIZE FOR PARCOR OF LOW BAND
      C
0034      DO 240 J=1,4
0035      IBT=IBPL(J)
0036      DO 250 I=1,IBT
0037      IQI=IQI+1
0038      250  INB(I)=INBA(IQI)
0039      CALL BDCONV(INB,IBT,IDPL(J))
0040      240  CONTINUE
      C
      C      DESERIALIZE FOR PARCOR OF HIGH BAND
      C
0041      DO 260 J=1,4
0042      IBT=IBPH(J)
0043      DO 270 I=1,IBT
0044      IQI=IQI+1
0045      270  INB(I)=INBA(IQI)
0046      CALL BDCONV(INB,IBT,IDPH(J))
0047      260  CONTINUE
      C
      C      DESERIALIZE FOR ERROR SIGNALS
0048      IF(IBIL.LE.1)GO TO 300
      C      IBIL=2 OR 3
      C
0049      IES=0
0050      IEF=72
0051      IBL=IBIL
0052      IBS=IBIH
0053      GO TO 400
0054      300  CONTINUE
0055      IES=72
0056      IEF=0
0057      IBL=IBIH
0058      IBS=IBIL
0059      400  CONTINUE
      C
      C
0060      IQS=50
      C
0061      IF(IBL.EQ.3)GO TO 600
      C
      C      IBL=2
      C      DESERIALIZE FOR HIGHER ENERGY BAND
      C
      C
0062      DO 520 I=1,72
0063      IJ=I+IES
0064      DO 530 J=1,IBL
0065      IQS=IQS+1
0066      530  INB(J)=INBA(IQS)
0067      CALL BDCONV(INB,IBL,NIN(IJ))
0068      520  CONTINUE
      C
      C      DESERIALIZE LESS IMPORTANT BAND
      C

```



```

0069      DO 540 I=1,72
0070      IJ=I+IEF
0071      IQS=IQS+1
0072      NIN(IJ)=INBA(IQS)
0073      540 CONTINUE
0074      RETURN
0075      600 CONTINUE
          C
          C      IBL=3
          C
0076      DO 610 I=1,31
0077      IJ=I+IES
0078      DO 620 J=1,IBL
0079      IQS=IQS+1
0080      620 INB(J)=INBA(IQS)
0081      CALL BDCONV(INB,IBL,NIN(IJ))
0082      610 CONTINUE
          C
0083      DO 630 I=32,72
0084      IJ=I+IES
0085      DO 640 J=1,2
0086      IQS=IQS+1
0087      640 INB(J)=INBA(IQS)
0088      INB(3)=INBA(194+I)
0089      CALL BDCONV(INB,IBL,NIN(IJ))
0090      630 CONTINUE
          C
          C      END OF DESERIALIZATION
0091      RETURN
0092      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	002162 569	RW,I,CON,LCL
SIDATA	000124 42	RW,D,CON,LCL
SVARS	000032 13	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL
MTAPE0	001250 340	RW,D,OVR,GBL
SBTA	000030 12	RW,D,OVR,GBL
SDTA	000030 12	RW,D,OVR,GBL

TOTAL SPACE ALLOCATED = 003674 990

DSER,LP:=DSER/NOTR

```

      C      GF2ADD.FTN
      C      ADDITION OVER GF(2)
      C      POLINOMIAL A(X) MUST BE ORDERED IN DESCENDING POWER SERIES
0001      SUBROUTINE GF2ADD(INA,NA,INB,NB,INC,NC)
0002      DIMENSION INA(1),INB(1),INC(1)
0003      NC=NA
0004      IF(NB.GT.NA)NC=NB
0005      DO 10 I=1,NC
0006      IC=NC+1-I
0007      IRA=NA+1-I
0008      IRB=NB+1-I
0009      ITA=0
0010      ITB=0
0011      IF(IRA.GT.0)ITA=INA(IRA)
0012      IF(IRB.GT.0)ITB=INB(IRB)
0013      INC(IC)=IEOR(ITA,ITB)
0014      10  CONTINUE
0015      RETURN
0016      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000272 93	RW,I,CON,LCL
SIDATA	000036 15	RW,D,CON,LCL
SVARS	000014 6	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000346 115

NO FPP INSTRUCTIONS GENERATED

```

      C      GF2MUL.FTN
      C      MULTIPLICATION OVER GF(2)
      C      NA<NF,NB<NF
0001      SUBROUTINE GF2MUL(INA,NA,INB,NB,INC,NC,INF,NF)
0002      DIMENSION IAT(17),INA(1),INB(1),INC(1),INF(1)
0003      NCC=NA+NB-1
      C      INI VECTOR C
0004      DO 10 I=1,NCC
0005      10  IAT(I)=0
      C      MULTIPLY A AND B
0006      DO 20 I=1,NA
0007      DO 30 J=1,NB
0008      IC=I+J-1
0009      IT=IAND(INA(I),INB(J))
0010      IAT(IC)=IEOR(IAT(IC),IT)
0011      30  CONTINUE
0012      20  CONTINUE
0013      CALL GF2DIV(IAT,NCC,INF,NF,INC,NC)
0014      RETURN
0015      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000344 114	RW,I,CON,LCL
SIDATA	000066 27	RW,D,CON,LCL
SVARS	000054 22	RW,D,CON,LCL
STEMPS	000004 2	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000512 165

NO FPP INSTRUCTIONS GENERATED

```

      C      GF2DIV.FTN
      C      FINITE FIELD DIVISION
      C      DEVISOR VECTOR B IS DESTROYED IN COMPUTATION IF NOT NORMALIZWD
0001      SUBROUTINE GF2DIV(INA,NA,INB,NB,INC,NC)
0002      DIMENSION INA(1),INB(1),INC(1)
      C      NORMALIZE VECTOR B
0003      NC=NB-1
0004      NBP=NB
0005      DO 11 I=1,NB
0006      IF(INB(1).EQ.1)GO TO 22
0007      NBP=NBP-1
0008      IF(NBP.LE.0)GO TO 11
0009      DO 33 J=1,NBP
0010      33  INB(J)=INB(J+1)
0011      11  CONTINUE
      C      VECTOR B=0
0012      WRITE(5,100)
0013      100  FORMAT(1X,'DIVISOR=0')
0014      RETURN
0015      22  CONTINUE
0016      IF(NA.GE.NBP)GO TO 10
      C      INA(I) IS THE ANSWER
0017      DO 20 I=1,NC
0018      IR=NC+1-I
0019      INC(IR)=0
0020      IF(I.GT.NA)GO TO 20
0021      ITA=NA+1-I
0022      INC(IR)=INA(ITA)
0023      20  CONTINUE
0024      RETURN
0025      10  CONTINUE
      C      INI VECTOR C
      C      ACTUAL NA MAY BE SMALLER THAN NBP
0026      DO 30 I=1,NBP
0027      30  INC(I)=INA(I)
0028      NAP=NBP
0029      111  CONTINUE
      C      CHECK C(1)=1
0030      IF(INC(1).EQ.0)GO TO 222
      C      START DIVISION
0031      DO 50 I=1,NBP
0032      50  INC(I)=IEOR(INC(I),INB(I))
0033      222  CONTINUE
0034      NAP=NAP+1
0035      IF(NAP.GT.NA)GO TO 333
      C      SHIFT ONE BIT LEFT
0036      DO 60 I=1,NBP-1
0037      60  INC(I)=INC(I+1)
0038      INC(NBP)=INA(NAP)
0039      GO TO 111
0040      333  CONTINUE
      C      INSERT 0 IF NBP NOT EQUAL TO NB
0041      IF(NBP.NE.NB)GO TO 777
0042      DO 555 I=1,NC
0043      555  INC(I)=INC(I+1)
0044      RETURN

```

FORTRAN IV-PLUS V02-51E  
GF2AMD.FTN /WR

16:45:14

06-OCT-80

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```
0045      777      CONTINUE
0046                      DO 773 I=1,NC
0047                      IT=0
0048                      IR=NC+1-I
0049                      IBC=NBP+1-I
0050                      IF(I.GT.NBP)GO TO 773
0051                      IT=INC(IBC)
0052      773      INC(IR)=IT
0053                      RETURN
0054                      END
```

#### PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	001004 258	RW,I,CON,LCL
SIDATA	000054 22	RW,D,CON,LCL
\$VARS	000020 8	RW,D,CON,LCL
STEMPS	000010 4	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 001110 292

NO FPP INSTRUCTIONS GENERATED

GF2AMD,LP:=GF2AMD/NOTR

```

C      DBCONV.FTN
C      MARCH 13, 1979
C      DECIMAL TO BINARY CONVERSION ROUTINE
C      SUBROUTINE DBCONV(IX,LIB,INB)
C      IX;INPUT INTERGER
C      LIB;LENGTH OF OUTPUT VECTOR
C      IX=INB(LIB)+INB(LIB-1)*2+ . . .
0001      SUBROUTINE DBCONV(IX,LIB,INB)
0002      DIMENSION INB(1)
0003      IY=IX
0004      DO 10 I=1,LIB
0005      IR=LIB+1-I
0006      INB(IR)=MOD(IY,2)
0007      10  IY=IY/2
0008      RETURN
0009      END

```

# PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000136 47	RW,I,CON,LCL
SIDATA	000012 5	RW,D,CON,LCL
SVARS	000006 3	RW,D,CON,LCL
STEMPS	000002 1	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000160 56

NO FPP INSTRUCTIONS GENERATED

```

      C      BD CONV.FTN
      C      MARCH 13, 1979
      C      BINARY TO DECIMAL CONVERSION ROUTINE
      C      SUBROUTINE BD CONV(INB,LIB,IY)
      C      IY;OUTPUT INTEGER
      C      LIB;LENGTH OF INPUT VECTOR
      C      IY=INB(LIB)+INB(LIB-1)*2+ . . .
0001      SUBROUTINE BD CONV(INB,LIB,IY)
0002      DIMENSION INB(1)
0003      IY=0
0004      IF(LIB.LE.0)RETURN
0005      DO 10 I=1,LIB
0006      IT=2*(I-1)
0007      IY=IY+INB(LIB+1-I)*IT
0008      RETURN
0009      END

```

PROGRAM SECTIONS

NAME	SIZE	ATTRIBUTES
SCODE1	000144 50	RW,I,CON,LCL
SIDATA	000012 5	RW,D,CON,LCL
SVARS	000004 2	RW,D,CON,LCL
SIEMPS	000002 1	RW,D,CON,LCL

TOTAL SPACE ALLOCATED = 000164 58

NO FPP INSTRUCTIONS GENERATED

CONV,LP:=CONV/NOTR

01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 00
01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 1100
01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 1100

PPPPPPPP		AAAAAA		RRRRRRRR		AAAAAA		MM		MM	
PPPPPPPP		AAAAAA		RRRRRRRR		AAAAAA		MM		MM	
PP	PP	AA	AA	RR	RR	AA	AA	MMMM		MMMM	
PP	PP	AA	AA	RR	RR	AA	AA	MMMM		MMMM	
PP	PP	AA	AA	RR	RR	AA	AA	MM	MM	MM	
PP	PP	AA	AA	RR	RR	AA	AA	MM	MM	MM	
PPPPPPPP		AA	AA	RRRRRRRR		AA	AA	MM		MM	
PPPPPPPP		AA	AA	RRRRRRRR		AA	AA	MM		MM	
PP		AAAAAAAAAA		RR RR		AAAAAAAAAA		MM		MM	
PP		AAAAAAAAAA		RR RR		AAAAAAAAAA		MM		MM	
PP		AA	AA	RR	RR	AA	AA	MM		MM	
PP		AA	AA	RR	RR	AA	AA	MM		MM	....
PP		AA	AA	RR	RR	AA	AA	MM		MM	....
PP		AA	AA	RR	RR	AA	AA	MM		MM	....
PP		AA	AA	RR	RR	AA	AA	MM		MM	....

DDDDDDDD		AAAAAA		TTTTTTTTTT		????		222222	
DDDDDDDD		AAAAAA		TTTTTTTTTT		????		222222	
DD	DD	AA	AA	TT		????	22	22	
DD	DD	AA	AA	TT		????	22	22	
DD	DD	AA	AA	TT				22	
DD	DD	AA	AA	TT		????		22	
DD	DD	AA	AA	TT		????		22	
DD	DD	AAAAAAAAAA		TT		????	22		
DD	DD	AAAAAAAAAA		TT		????	22		
DD	DD	AA	AA	TT		??	22		
DD	DD	AA	AA	TT		??	22		
DDDDDDDD		AA	AA	TT		??	2222222222		
DDDDDDDD		AA	AA	TT		??	2222222222		

01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 1100
01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 1100
01234567890123456789	** RSX-11M V3.2 **	6-OCT-80	16:47:32	DR0: 1100



+0.69105790E-03  
 -0.14037930E-02  
 -0.12683030E-02  
 +0.42341950E-02  
 +0.14142460E-02  
 -0.94583180E-02  
 -0.13038590E-03  
 +0.17981450E-01  
 -0.41874830E-02  
 -0.31238620E-01  
 +0.14568440E-01  
 +0.52947450E-01  
 -0.39348780E-01  
 -0.99802430E-01  
 +0.12855790E+00  
 +0.4664053E+00  
 +0.4664053E+00  
 +0.12855790E+00  
 -0.99802430E-01  
 -0.39348780E-01  
 +0.52947450E-01  
 +0.14568440E-01  
 -0.31238620E-01  
 -0.41874830E-02  
 +0.17981450E-01  
 -0.13038590E-03  
 -0.94583180E-02  
 +0.14142460E-02  
 +0.42341950E-02  
 -0.12683030E-02  
 -0.14037930E-02  
 +0.69105790E-03

:SBAPC.TBL  
 :32 TAP QMF FILTER COEFFICIENT(6400 HZ)

0.11955E+00 :BETA QUANTIZER WITH 4 BITS  
 0.17501E+00  
 0.23046E+00  
 0.27991E+00  
 0.32937E+00  
 0.37689E+00  
 0.42441E+00  
 0.47350E+00  
 0.52259E+00  
 0.56728E+00  
 0.61196E+00  
 0.64927E+00  
 0.68657E+00  
 0.72049E+00  
 0.75441E+00  
 0.78538E+00  
 0.81635E+00  
 0.84285E+00  
 0.86935E+00  
 0.89298E+00  
 0.91660E+00  
 0.93881E+00  
 0.96102E+00  
 0.98399E+00  
 0.10070E+01  
 0.10454E+01  
 0.10838E+01  
 0.11432E+01  
 0.12027E+01  
 0.12882E+01  
 0.13737E+01

0.17426E+01 TQQL QUANTIZER WITH 5 BITS

0.18480E+01  
0.19535E+01  
0.20564E+01  
0.21593E+01  
0.22642E+01  
0.23691E+01  
0.24743E+01  
0.25795E+01  
0.26861E+01  
0.27928E+01  
0.28983E+01  
0.30039E+01  
0.31081E+01  
0.32122E+01  
0.33168E+01  
0.34214E+01  
0.35233E+01  
0.36252E+01  
0.37236E+01  
0.38220E+01  
0.39192E+01  
0.40164E+01  
0.41137E+01  
0.42110E+01  
0.43064E+01  
0.44018E+01  
0.44962E+01  
0.45906E+01  
0.46848E+01  
0.47790E+01  
0.48703E+01  
0.49616E+01  
0.50512E+01  
0.51408E+01  
0.52307E+01  
0.53205E+01  
0.54095E+01  
0.54985E+01  
0.55902E+01  
0.56818E+01  
0.57713E+01  
0.58607E+01  
0.59518E+01  
0.60428E+01  
0.61351E+01  
0.62275E+01  
0.63214E+01  
0.64154E+01  
0.65122E+01  
0.66090E+01  
0.67081E+01  
0.68073E+01  
0.69119E+01  
0.70166E+01  
0.71304E+01  
0.72442E+01  
0.73728E+01  
0.75014E+01  
0.76496E+01  
0.77979E+01  
0.80013E+01  
0.82047E+01  
0.19064E+00  
0.32683E+00  
0.46302E+00

:QQH QUANTIZER WITH 5 BITS  
E-74

0.58423E+00  
 0.70543E+00  
 0.82849E+00  
 0.95154E+00  
 0.10760E+01  
 0.12004E+01  
 0.13188E+01  
 0.14372E+01  
 0.15488E+01  
 0.16605E+01  
 0.17730E+01  
 0.18856E+01  
 0.19939E+01  
 0.21022E+01  
 0.22105E+01  
 0.23188E+01  
 0.24193E+01  
 0.25198E+01  
 0.26204E+01  
 0.27210E+01  
 0.28168E+01  
 0.29127E+01  
 0.30101E+01  
 0.31075E+01  
 0.32044E+01  
 0.33013E+01  
 0.33961E+01  
 0.34910E+01  
 0.35889E+01  
 0.36868E+01  
 0.37795E+01  
 0.38722E+01  
 0.39655E+01  
 0.40588E+01  
 0.41555E+01  
 0.42522E+01  
 0.43483E+01  
 0.44444E+01  
 0.45438E+01  
 0.46432E+01  
 0.47414E+01  
 0.48396E+01  
 0.49364E+01  
 0.50332E+01  
 0.51330E+01  
 0.52329E+01  
 0.53378E+01  
 0.54426E+01  
 0.55504E+01  
 0.56582E+01  
 0.57699E+01  
 0.58816E+01  
 0.59983E+01  
 0.61151E+01  
 0.62371E+01  
 0.63591E+01  
 0.64892E+01  
 0.66194E+01  
 0.67673E+01  
 0.69153E+01  
 -0.87994E+00  
 -0.77363E+00  
 -0.66732E+00  
 -0.59522E+00  
 -0.52312E+00  
 -0.46606E+00

:PCRL(1) QUANTIZER WITH 5 BITS

-0.40900E+00  
-0.36045E+00  
-0.31190E+00  
-0.26812E+00  
-0.22434E+00  
-0.18392E+00  
-0.14350E+00  
-0.10522E+00  
-0.66935E-01  
-0.30230E-01  
0.64762E-02  
0.42000E-01  
0.77525E-01  
0.11224E+00  
0.14696E+00  
0.18073E+00  
0.21450E+00  
0.24746E+00  
0.28042E+00  
0.31248E+00  
0.34454E+00  
0.37567E+00  
0.40680E+00  
0.43687E+00  
0.46695E+00  
0.49566E+00  
0.52438E+00  
0.55127E+00  
0.57817E+00  
0.60282E+00  
0.62748E+00  
0.64976E+00  
0.67205E+00  
0.69215E+00  
0.71226E+00  
0.73047E+00  
0.74869E+00  
0.76526E+00  
0.78184E+00  
0.79701E+00  
0.81219E+00  
0.82618E+00  
0.84018E+00  
0.85317E+00  
0.86617E+00  
0.87832E+00  
0.89048E+00  
0.90190E+00  
0.91333E+00  
0.92401E+00  
0.93470E+00  
0.94457E+00  
0.95445E+00  
0.96344E+00  
0.97244E+00  
0.98054E+00  
0.98865E+00  
-0.96267E+00  
-0.91995E+00  
-0.87723E+00  
-0.84365E+00  
-0.81007E+00  
-0.78072E+00  
-0.75137E+00  
-0.72398E+00  
-0.69659E+00

:PCRL(2) QUANTIZER WITH 5 BITS

-0.67018E+00  
-0.64377E+00  
-0.61763E+00  
-0.59149E+00  
-0.56532E+00  
-0.53915E+00  
-0.51275E+00  
-0.48635E+00  
-0.45957E+00  
-0.43279E+00  
-0.40556E+00  
-0.37833E+00  
-0.35062E+00  
-0.32291E+00  
-0.29523E+00  
-0.26755E+00  
-0.24122E+00  
-0.21489E+00  
-0.19155E+00  
-0.16821E+00  
-0.14803E+00  
-0.12785E+00  
-0.10934E+00  
-0.90829E-01  
-0.73840E-01  
-0.56850E-01  
-0.40620E-01  
-0.24389E-01  
-0.83896E-02  
0.76100E-02  
0.23901E-01  
0.40191E-01  
0.57370E-01  
0.74550E-01  
0.92820E-01  
0.11109E+00  
0.13205E+00  
0.15301E+00  
0.17825E+00  
0.20349E+00  
0.23324E+00  
0.26299E+00  
0.29826E+00  
0.33353E+00  
0.37267E+00  
0.41181E+00  
0.45435E+00  
0.49689E+00  
0.54353E+00  
0.59017E+00  
0.64602E+00  
0.70187E+00  
0.77762E+00  
0.85337E+00  
-0.72278E+00  
-0.59179E+00  
-0.46080E+00  
-0.35662E+00  
-0.25244E+00  
-0.18333E+00  
-0.11422E+00  
-0.56879E-01  
0.46074E-03  
0.60810E-01  
0.12116E+00  
0.20370E+00

:PCRL(3) QUANTIZER WITH 3 BITS

```

0.28624E+00
0.41861E+00
0.55098E+00
-0.75740E+00      :PCRL(4) QUANTIZER WITH 3 BITS
-0.60863E+00
-0.45986E+00
-0.36269E+00
-0.26552E+00
-0.19364E+00
-0.12176E+00
-0.57760E-01
0.62395E-02
0.72040E-01
0.13784E+00
0.21700E+00
0.29616E+00
0.41644E+00
0.53672E+00
-0.94739E+00      :PCRH(1) QUANTIZER WITH 4 BITS
-0.89316E+00
-0.83893E+00
-0.78660E+00
-0.73427E+00
-0.68057E+00
-0.62687E+00
-0.56998E+00
-0.51309E+00
-0.45476E+00
-0.39643E+00
-0.34116E+00
-0.28589E+00
-0.23492E+00
-0.18395E+00
-0.13749E+00
-0.91032E-01
-0.46850E-01
-0.26668E-02
0.41811E-01
0.86288E-01
0.13477E+00
0.18325E+00
0.23942E+00
0.29559E+00
0.35880E+00
0.42201E+00
0.49611E+00
0.57021E+00
0.66087E+00
0.75153E+00
-0.94890E+00      :PCRH(2) QUANTIZER WITH 4 BITS
-0.87898E+00
-0.80906E+00
-0.75051E+00
-0.69196E+00
-0.63959E+00
-0.58722E+00
-0.53818E+00
-0.48914E+00
-0.44235E+00
-0.39556E+00
-0.35059E+00
-0.30562E+00
-0.26238E+00
-0.21914E+00
-0.17735E+00
-0.13556E+00

```

-0.94420E-01  
 -0.53281E-01  
 -0.11620E-01  
 0.30041E-01  
 0.73880E-01  
 0.11772E+00  
 0.16644E+00  
 0.21516E+00  
 0.27301E+00  
 0.33086E+00  
 0.40702E+00  
 0.48318E+00  
 0.59736E+00  
 0.71154E+00  
 -0.78903E+00 :PCRH(3) QUANTIZER WITH 3 BITS  
 -0.66820E+00  
 -0.54737E+00  
 -0.45189E+00  
 -0.35641E+00  
 -0.27235E+00  
 -0.18829E+00  
 -0.11008E+00  
 -0.31868E-01  
 0.47160E-01  
 0.12619E+00  
 0.21560E+00  
 0.30501E+00  
 0.42609E+00  
 0.54717E+00  
 -0.77081E+00 :PCRH(4) QUANTIZER WITH 3 BITS  
 -0.64754E+00  
 -0.52427E+00  
 -0.43351E+00  
 -0.34275E+00  
 -0.26413E+00  
 -0.18551E+00  
 -0.11102E+00  
 -0.36528E-01  
 0.40490E-01  
 0.11751E+00  
 0.20637E+00  
 0.29523E+00  
 0.41846E+00  
 0.54169E+00  
 0.57160E+00 :LOW BAND(LB)ERROR SIGNAL QUANTIZER WITH 1-BIT  
 0.37732E+00 :LOW BAND ERROR SIGNAL QUANTIZER= 2 BITS  
 0.10100E+01  
 0.16427E+01  
 0.20766E+00 :LB ERROR SIGNAL QUANTIZER=3 BITS  
 0.44375E+00  
 0.67984E+00  
 0.10428E+01  
 0.14057E+01  
 0.20966E+01  
 0.27874E+01  
 0.12400E+00 :LB ERROR SIG. QUANTIZER WITH 4 BITS  
 0.26440E+00  
 0.40480E+00  
 0.56670E+00  
 0.72870E+00  
 0.91980E+00  
 0.11110E+01  
 0.13444E+01  
 0.15778E+01  
 0.18776E+01  
 0.21773E+01

0.25971E+01	
0.30169E+01	
0.37240E+01	
0.44311E+01	
0.65376E+00	:HIGH BAND(HB) ERROR SIGNAL QUANTIZER WITH 1 BIT
0.38877E+00	:HB ERROR SIGNAL QUANTIZER=2 BITS
0.11427E+01	
0.18966E+01	
0.20196E+00	:HB ERROR SIGNAL QUANTIZER=3 BITS
0.48833E+00	
0.77469E+00	
0.11967E+01	
0.16188E+01	
0.23432E+01	
0.30676E+01	
0.12400E+00	:LB ERROR SIG. QUANTIZER WITH 4 BITS
0.26440E+00	
0.40480E+00	
0.56670E+00	
0.72870E+00	
0.91980E+00	
0.11110E+01	
0.13444E+01	
0.15778E+01	
0.18776E+01	
0.21773E+01	
0.25971E+01	
0.30169E+01	
0.37240E+01	
0.44311E+01	
0.25182E+00	: TABLE FOR MCAULEY NOISE SUPPRESSION FACTOR NSF=1
0.27069E+00	
0.28459E+00	
0.29657E+00	
0.30749E+00	
0.31776E+00	
0.32761E+00	
0.33718E+00	
0.34659E+00	
0.35590E+00	
0.36518E+00	
0.37447E+00	
0.38383E+00	
0.39329E+00	
0.40289E+00	
0.41266E+00	
0.42263E+00	
0.43285E+00	
0.44333E+00	
0.45413E+00	
0.46527E+00	
0.47679E+00	
0.48873E+00	
0.50113E+00	
0.51404E+00	
0.52750E+00	
0.54157E+00	
0.55630E+00	
0.57173E+00	
0.58794E+00	
0.60498E+00	
0.62291E+00	
0.64179E+00	
0.66168E+00	
0.68263E+00	
0.70468E+00	



0.72785E+00  
0.75212E+00  
0.77742E+00  
0.80364E+00  
0.83053E+00  
0.85774E+00  
0.88474E+00  
0.91079E+00  
0.93493E+00  
0.95600E+00  
0.97285E+00  
0.98476E+00  
0.99222E+00  
0.99749E+00  
0.20235E+00  
0.21901E+00  
0.23188E+00  
0.24336E+00  
0.25417E+00  
0.26462E+00  
0.27490E+00  
0.28514E+00  
0.29542E+00  
0.30581E+00  
0.31638E+00  
0.32716E+00  
0.33822E+00  
0.34959E+00  
0.36131E+00  
0.37342E+00  
0.38597E+00  
0.39899E+00  
0.41253E+00  
0.42662E+00  
0.44133E+00  
0.45667E+00  
0.47271E+00  
0.48949E+00  
0.50704E+00  
0.52541E+00  
0.54464E+00  
0.56476E+00  
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0.70465E+00  
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0.68105E+00  
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0.98204E+00  
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0.96019E-01  
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0.36507E+00  
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0.93352E+00  
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0.96125E+00  
0.96987E+00  
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0.98211E+00  
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0.99749E+00  
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0.70454E-01  
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0.20692E+00  
0.22826E+00  
0.25237E+00  
0.27958E+00  
0.31024E+00  
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0.38318E+00  
0.42588E+00  
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0.52342E+00  
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0.68929E+00  
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0.96191E+00  
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0.25374E-01  
0.27430E-01  
0.29629E-01  
0.32000E-01  
0.34574E-01  
0.37384E-01  
0.40465E-01  
0.43861E-01  
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0.51792E-01  
0.56448E-01  
0.61662E-01  
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0.81641E-01  
0.90174E-01  
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0.13881E+00  
0.15601E+00  
0.17600E+00  
0.19925E+00  
0.22632E+00  
0.25782E+00  
0.29437E+00  
0.33653E+00  
0.38473E+00  
0.43907E+00  
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0.56392E+00  
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0.81935E+00  
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0.15898E-01  
0.17269E-01  
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0.84844E+00  
0.89488E+00  
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0.99244E+00  
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0.92164E+00  
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0.99244E+00  
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0.32029E-02  
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0.38547E-02  
0.42250E-02  
0.46332E-02  
0.50862E-02  
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0.61595E-02  
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0.75262E-02  
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0.31414E-02  
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0.43260E-02  
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0.90013E+00  
0.93985E+00  
0.96009E+00  
0.97037E+00  
0.97680E+00  
0.98217E+00  
0.98734E+00  
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0.69974E-03  
0.77592E-03  
0.85786E-03  
0.94745E-03  
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0.55762E-02  
0.65194E-02  
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0.91239E-02  
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0.20094E-01  
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:NSF=13

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0.28486E+00  
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0.73501E+00  
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0.92493E+00  
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0.98217E+00  
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:NSF=14

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0.25538E-02  
0.32605E-02  
0.42303E-02  
0.55886E-02  
0.75336E-02  
0.10388E-01  
0.14695E-01  
0.21387E-01  
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0.37403E+00  
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0.76772E+00  
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## APPENDIX F

### THE 16 Kbps ADAPTIVE TRANSFORM CODER

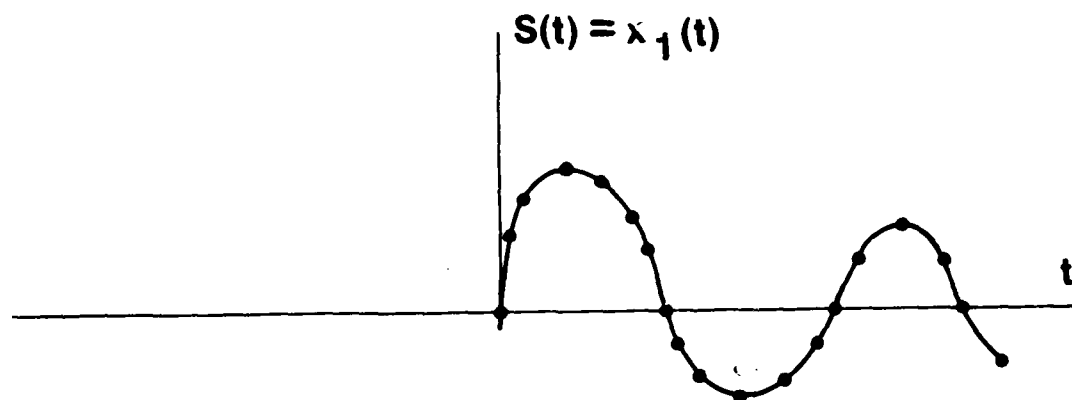
Adaptive Transform Coding (ATC), as proposed by Zelinsky and Noll [1] is an effective block-coding technique for speech encoding in the 8.0 to 16.0 kb/s range.

In its basic form, ATC consists of sending the largest cosine transform coefficients of a segment of data with each coefficient quantized according to an algorithm that gives the larger coefficients more bits than the smaller coefficients. This ATC algorithm departs from earlier algorithms that not only had to send the amplitudes of the coefficients, but also had to send considerable information about which coefficients were quantized and how many bits were associated with each. This extra information could consume as much data capacity as the coefficient amplitudes themselves. Attempts at sending only specific coefficients or the use of a fixed-bit assignment generally reduced voice quality by creating waveform discontinuities at the frame boundaries and by spectrally distorting the signal between boundaries.

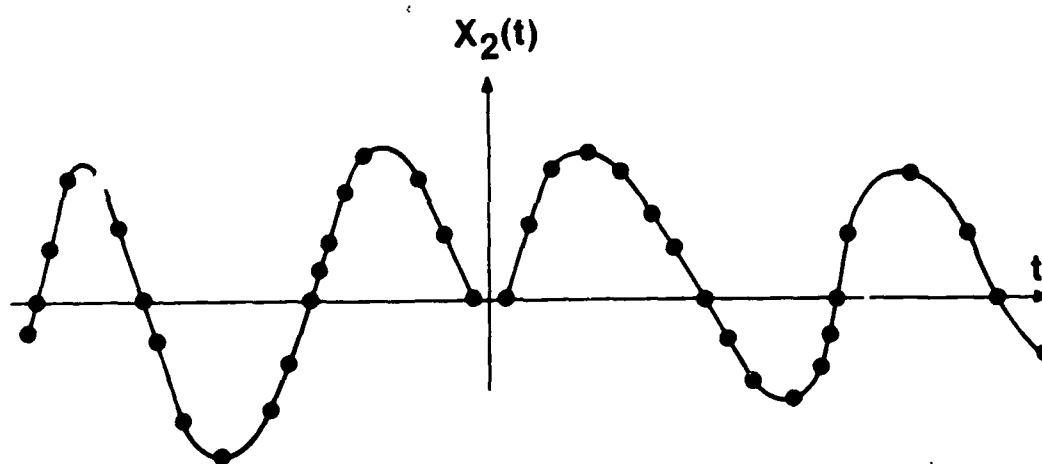
In ATC, however, information about which amplitude is sent and how many bits are allocated to each is contained in the basis spectrum, which requires only 2000 to 2400 b/s. This basis spectrum generally is information about the envelope of the transform coefficients being quantized. Its calculation can be performed by the smoothing of transform coefficients or by separate estimates involving least-square analysis [2].

To understand ATC, consider a sampled waveform segment shown in Figure C-1(a). If this waveform is multiplied by 1/2, delayed by half the sampling interval  $T$ , and reflected about  $t=0$ , it yields  $x_2(t)$  whose Fourier transform is given by:

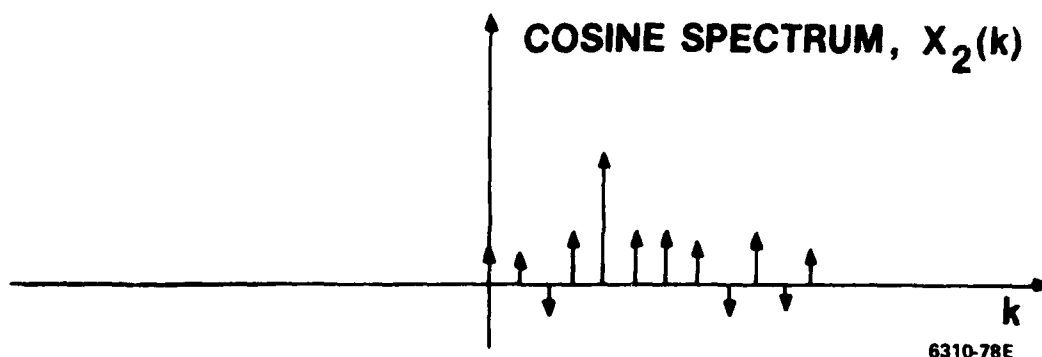
$$X_2(f) = \sum_{n = -(N-1)}^{N-1} x_2(nT) \exp(-j2\pi f(n+1/2)T) \quad (F-1)$$



(a) Original Waveform



(b) Reflected Waveform



(c) DFT Output

Figure F-1. Discrete Cosine Transform Operation

If we sample the Fourier transform of  $X_2(f)$  at frequencies  $\frac{m}{2NT}$ , the discrete Fourier transform (DFT) becomes

$$X_2\left(\frac{m}{2NT}\right) = X_2(m) = \sum_{N=-(N-1)}^{N-1} X_2(nT) \exp\left(-j\frac{\pi}{N}(n+1/2)m\right) \quad (F-2)$$

Using symmetry properties of  $X_2(nT)$ ,  $X_2(m)$  shown in Figure F-1(b) is real only and is given by

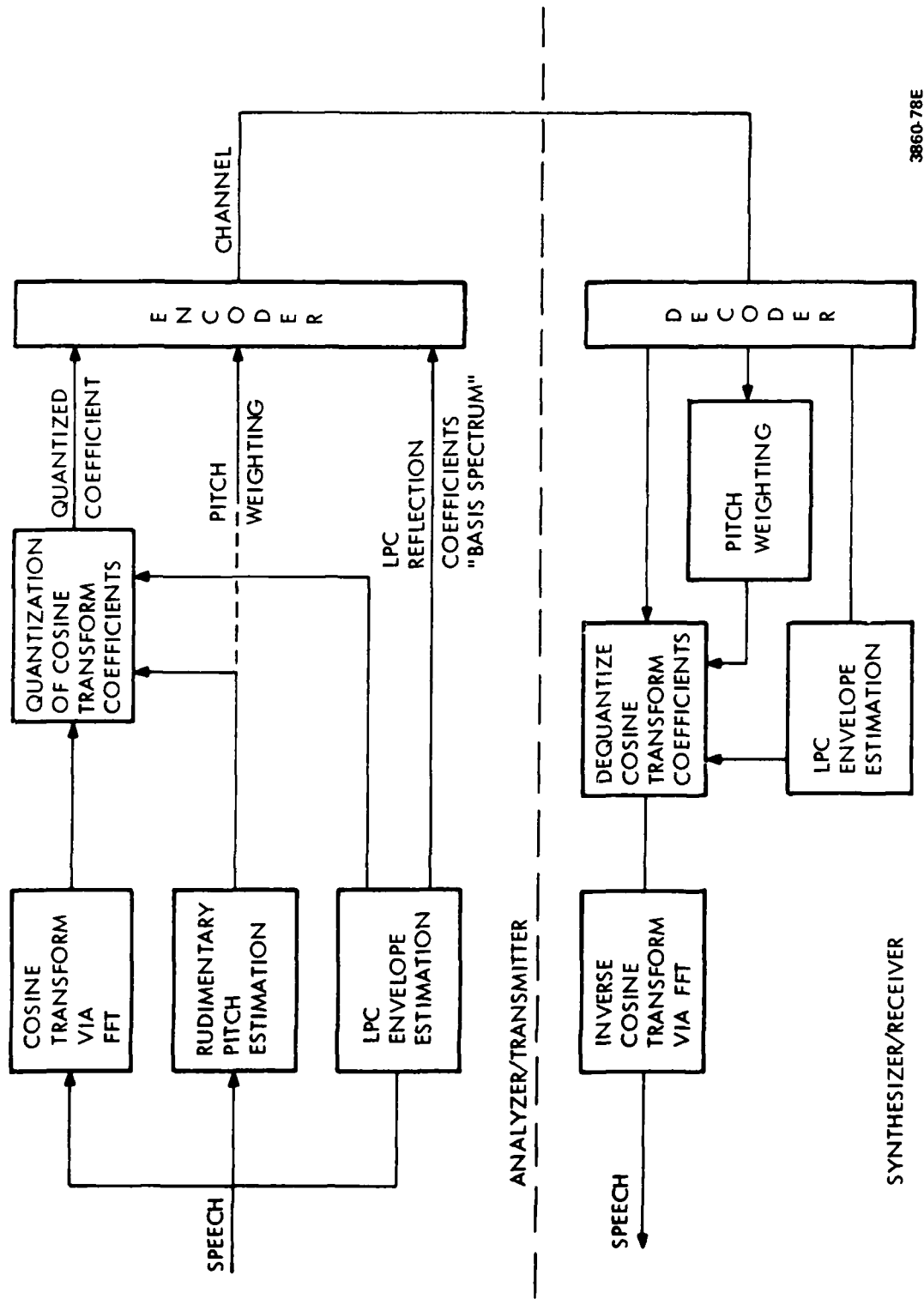
$$X_2(m) = \sum_{n=0}^{N-1} X_1(nT) \cos\left(\frac{\pi m}{2N}(2n+1)\right) \quad 0 \leq m \leq N-1 \quad (F-3)$$

Equation (F-3) is the cosine transform. This derivation shows that the Fast Fourier Transform (FFT) can be used to implement the cosine transform by delaying and reflecting the original waveform and then taking the FFT on a waveform twice as long as the original.

The most expensive implementation costs with the ATC algorithm are associated with the Discrete Cosine Transform (DCT) and Discrete Fourier Transform (DFT). Although the DCT cannot be employed directly, methods elaborated by Ahmed et al [3] and Cooley et al [4] use the DFT to compute the desired transform. These algorithms and their interrelationships are shown in Appendix G for clarification. Our FORTRAN simulations are now using the Cooley method for DCT calculation and a special FFT algorithm to lower simulation costs.

After calculation of the ATC coefficients, the basis spectrum (envelope of the cosine transform) can be estimated by making all the cosine transform coefficients positive and smoothing between peaks to efficiently send the envelope. We can quantize the amplitudes of every  $m$ th ( $m$  is typically 8) envelope sample and send those as the coefficients of the basis spectrum.

However, this original ATC algorithm, as proposed by Zelinski and Noll, suffers from a "burbling" characteristic at lower data rates. To reduce this distortion, Tribolet [2] uses side transmission of pitch and spectral parameters obtained by Linear Predictive Coding (LPC) analysis. The side transmission of the LPC and pitch parameters does in fact remove the "burbling" sound and improve the overall signal-to-noise ratio. Figure F-2 describes the operation of this ATC digitizer.



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Figure F-2. Adaptive Transform Coder

The innovative solution to the basis spectrum calculation is formed from a least-square analysis of  $x_2(t)$ , that is, finding those predictor coefficients which minimize.

$$E = \sum_{n=0}^{N-1} \left[ x_2(n) - \sum_{i=1}^P a_i x_2(n-i) \right]^2 \quad (F-4)$$

These predictor coefficients, or alternately reflection coefficients, carry information about the envelope since:

$$y(f) = \text{FFT}(a_i) \quad (F-5)$$

and the envelope is then  $Y^{-1}(f)$ .

In addition to linear predictive modeling of the ATC spectrum, the Tribolet approach uses a pitch excitation source. This accounts for the fine structure in the short-time spectrum, which is consistent with the known mechanisms of speech production. This scheme forces the assignment of transform bits to many pitch strictions that otherwise would not be transmitted at all.

With reference to Figure F-3, the ATC analysis is described as follows:

1. The input speech (Figure F-3(a)) is Fourier transformed to yield a DCT spectrum (Figure F-3(b)). This spectrum is squared, windowed, and inverse Fourier transformed to yield an autocorrelation function (i.e., pseudo-ACF) of the reflected speech waveform. The first  $P+1$  values of this function are used to define a correlation matrix in the usual normal equation formulation sense. The solution of these equations (i.e., Levinson recursion) yields a prediction filter of order  $P$ . The inverse spectrum of this filter yields a smoothed estimate of the DCT (Figure F-3(c)) spectral levels to be used in the adaptation of the quantizers.
2. A rudimentary estimate of the pitch value,  $M$ , is found in the pseudo-ACF after the second zero crossing beyond the  $P+1$  ACF value. A corresponding gain factor,  $G$ , is also computed as the ratio of  $\text{ACF}(M)/\text{ACF}(0)$ . With these two parameters, a pitch pattern is generated in the frequency domain (Figure F-3(d)) and applied congruently with the LPC spectrum. This combination, yielding a linear prediction spectral fit to the DCT of the input speech, is called the basis spectrum (Figure F-3(e)).
3. The computation to determine the number of bits to allocate for each transform then proceeds as follows:



Let  $\sigma_i$  be the amplitude of the  $i$ th term of the envelope of the basis spectrum. The  $B_i$ , the number of bits allocated to the  $i$  cosine transform coefficient, is given by:

$$B_i = \left[ B_f/N - (1/2N) \sum_{j=1}^N \log_2 \sigma_j^2 \right] + 1/2 \log_2 \sigma_i^2 \quad (F-6)$$

where

$B_f$  = the total number of bits allocated to send the cosine transform coefficients per frame

$N$  = the total number of cosine transform coefficients calculated per frame.

Note that the term in brackets is calculated once per frame. Fairly simple algorithms ensure that  $B_i$  is an integer value and that the sum of the integer  $B_i$  adds to  $B_f$ .

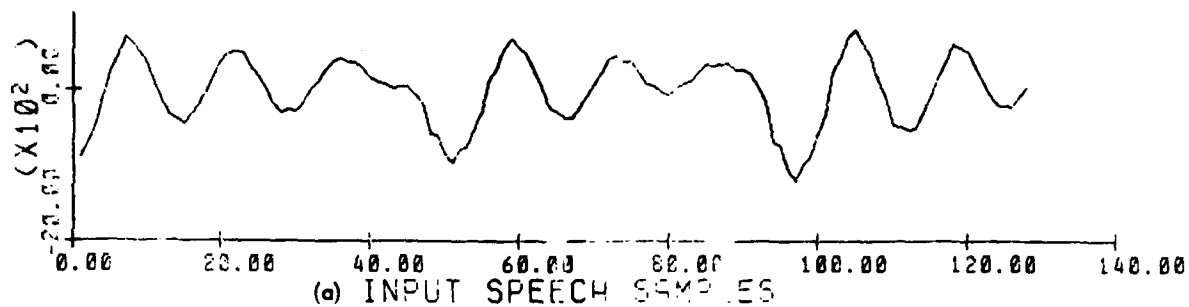
The cosine transform coefficients approximate a Gaussian probability density function. Optimum Gaussian quantizers derived by Max can be used to encode each transform coefficient with  $B_i$  bits. Since many of the  $B_i$ 's will be zero, only larger coefficients are sent. However, GTE has shown that optimal quantizers can be developed that more closely match the transform distribution.

4. The receiver uses the basis spectrum information (LPC, M, G) to regenerate the DCT envelope, to generate the bit allocations using Equation (F-6), to decode the cosine transform coefficients (Figure F-3 (f)), and then to take the inverse cosine transform using the FFT. Frame boundary problems exist at all data rates since quantization of the transform coefficients causes the regenerated waveform to be slightly different than the original. By overlapping the frames slightly and by interpolating across frame boundaries, these discontinuities can be smoothed.

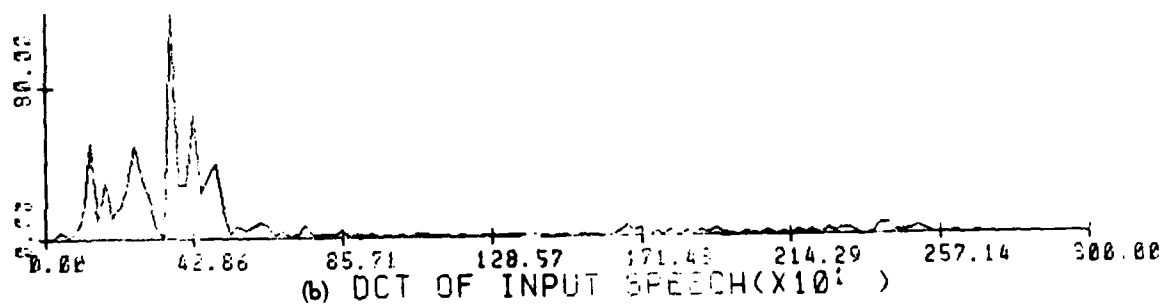
The overall quality of this approach can be surmised from Figure F-3(g), which shows the error waveform defined as:

$$e(n) = s(n) - \hat{s}(n) \quad (F-7)$$

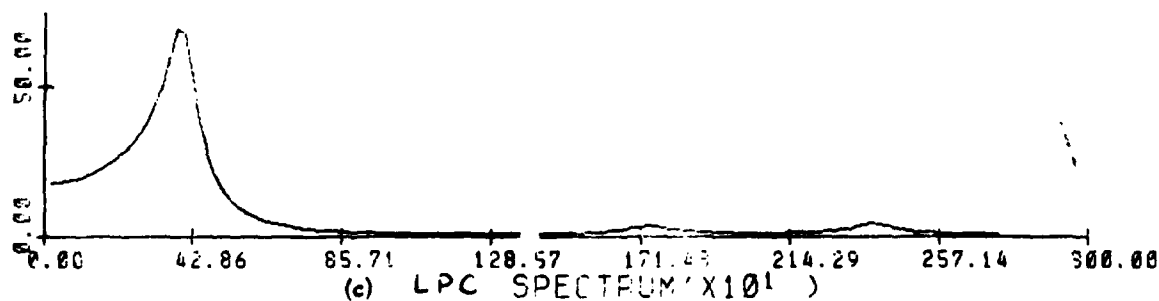
The received waveform,  $\hat{s}(n)$ , has a high signal-to-noise ratio ( $\sim 20$  dB) for some speakers, even for erroneous pitch estimations made in the analyzer. In fact, GTE has found that an eighth-order LPC predictor ( $P = 8$ ), coupled with the rudimentary pitch extractor (and voiced/unvoiced logic), yields high quality speech. In summary, the specifications of the 16 Kb/s ATC is shown in Table F-1.



(a) Input Speech Samples

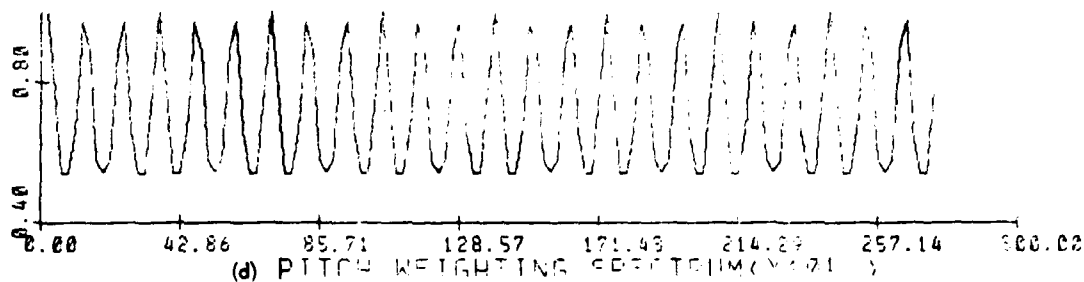


(b) DCT of Input Speech(X10<sup>1</sup>)

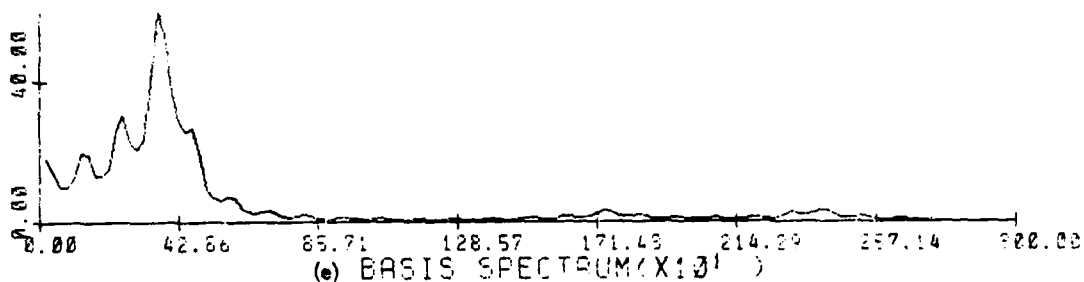


(c) LPC Spectrum(X10<sup>1</sup>)

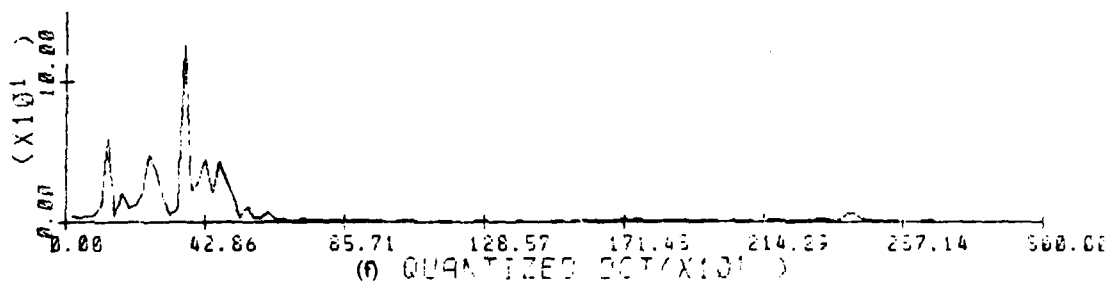
Figure F-3. Graphical Description of Vocoder Strategy for ATC



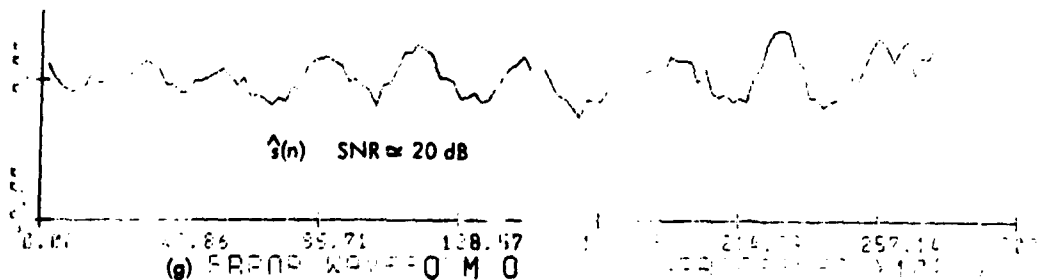
(d) Pitch-Weighting Spectrum(X10<sup>1</sup>)



(e) Basic Spectrum(X10<sup>1</sup>)



(f) Quantized DCT(X10<sup>1</sup>)



(g) Error Waveform-Original-Processed(X10<sup>1</sup>)

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Figure F-3. Graphical Description of Vocoder Strategy for ATC (Cont.)

<u>PARAMETER</u>	<u>SPECIFICATION</u>
Input Bandwidth	0-3200 Hz
Sampling Rate	6400 Hz
Frame Rate	26.016/sec.
Number of Samples/Frame	246
Number of Samples Overlapped/Frame	10
Bits/Frame	615
Pitch	{ 6 if voiced 0 if unvoiced
Pitch Gain	{ 2 if voiced 0 if unvoiced
Voiced/Unvoiced	1
RMS Energy	5
DC BIAS	5
PARCOR 1	5
PARCOR 2	5
PARCOR 3	4
PARCOR 4	4
PARCOR 5	3
PARCOR 6	3
PARCOR 7	2
PARCOR 8	2
Parity Bits (Error Correction)	54
SYNC	1
DCT Coefficients	{ 513 voiced 521 unvoiced
Number of Error Control Blocks/Frame	3
Error Control Technique	(63,45) BCH

TABLE F-1: 16 KBPS ATC SYSTEM SPECIFICATION

REFERENCES for APPENDIX F

- [1] R. Zelinski and P. Noll, "Adaptive Transform Coding of Speech Signals," IEEE Trans. Acoustics, Speech and Signal Processing, Vol. ASSP-25, No. 4, August 1977.
- [2] J. Tribolet and R. Crochiere, "A Vocoder-Driven Adaptation Strategy for Low-Bit Rate Adaptive Transform Coding of Speech," 1978 International Conference on Digital Signal Processing, Florence, Italy, August 30 to September 2, 1978.
- [3] N. Ahmed, T. Nataragan, and K. Rao, "Discrete Cosine Transform," IEEE Trans. Computers, Vol. C-23, 1974, pp. 90-93.
- [4] J. Cooley, P. Lewis, and P. Welch, "The Fast Fouries Transform Algorithm: Programming Considerations in the Calculation of Sine, Cosine, and Laplace Transforms," Jour. of Sound Vib., Vol. 12, July 1970, pp. 315-337.

## APPENDIX G

### INTERRELATIONSHIPS BETWEEN DCT AND DFT ALGORITHMS

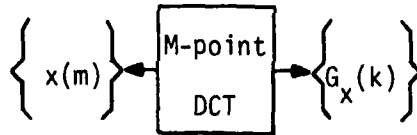
Problem Statement: Given a sequence  $x(m)$   $m=0,1,\dots,M-1$   
formulate the DCT of  $x$  as  $G_x(k)$   $k=0,1,\dots,M-1$

Solutions:

#### 1. Direct DCT Method

$$G_x(0) = \frac{\sqrt{2}}{M} \sum_{m=0}^{M-1} x(m)$$

$$G_x(k) = \frac{2}{M} \sum_{m=0}^{M-1} x(m) \cos \frac{\pi k(2m+1)}{2M}, \quad k=1,2,\dots,M-1$$



#### 2. Ahmed DFT Method

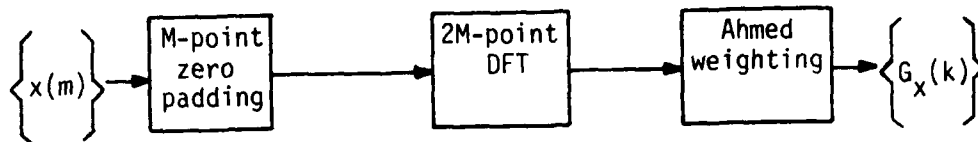
$$G_x(0) = \frac{\sqrt{2}}{M} \bar{X}(0)$$

$$G_x(k) = \frac{2}{M} \operatorname{Re} \left\{ \exp \left( -j \frac{\pi k}{2M} \right) \bar{X}(k) \right\}, \quad k=1,2,\dots,M-1$$

where

$$\bar{X}(k) = \text{DFT}(\hat{x}) = \sum_{m=0}^{2M-1} \hat{x}(m) \exp \left( -j \frac{2\pi km}{2M} \right), \quad k=0,1,\dots,2M-1$$

$$\text{and } \hat{x}(m) = \begin{cases} x(m) & \text{for } m=0,1,\dots,M-1 \\ 0 & \text{for } m=M,M+1,\dots,2M-1 \end{cases}$$



(3) Cooley DFT Method

$$G_x(0) = \frac{\sqrt{2}}{M} \bar{\bar{X}}(0)$$

$$G_x(k) = \frac{1}{M} \operatorname{Re} \left\{ \exp \left( -\frac{j\pi(M-1)k}{2M} \right) \bar{\bar{X}}(k) \right\}, \quad k=1, 2, \dots, M-1$$

$$\text{where } \bar{\bar{X}}(k) = \text{DFT}(\hat{x}) = \sum_{m=0}^{2M-1} \hat{x}(m) \exp \left( -\frac{j2\pi km}{2M} \right)$$

$$\text{and } \hat{x}(m) = x(M-1-m) + x(m-M)$$

